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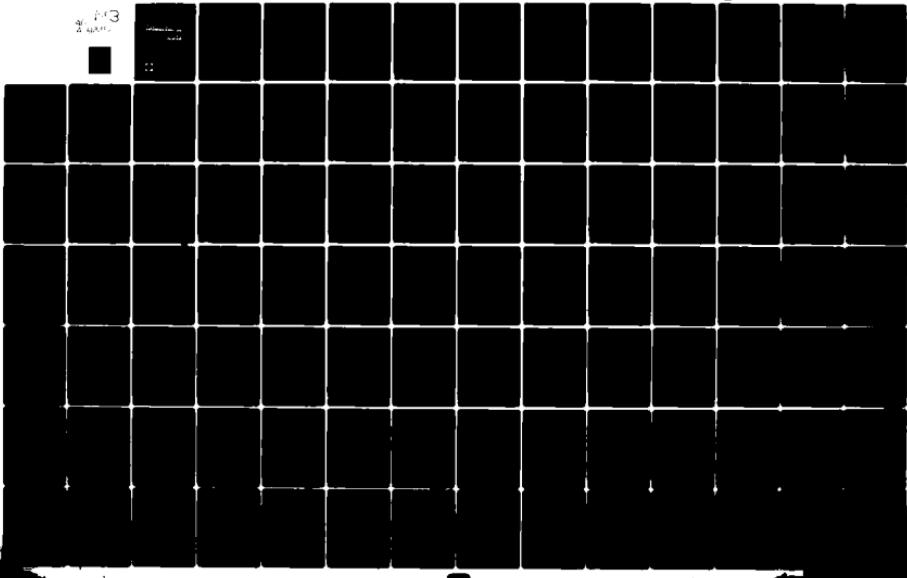
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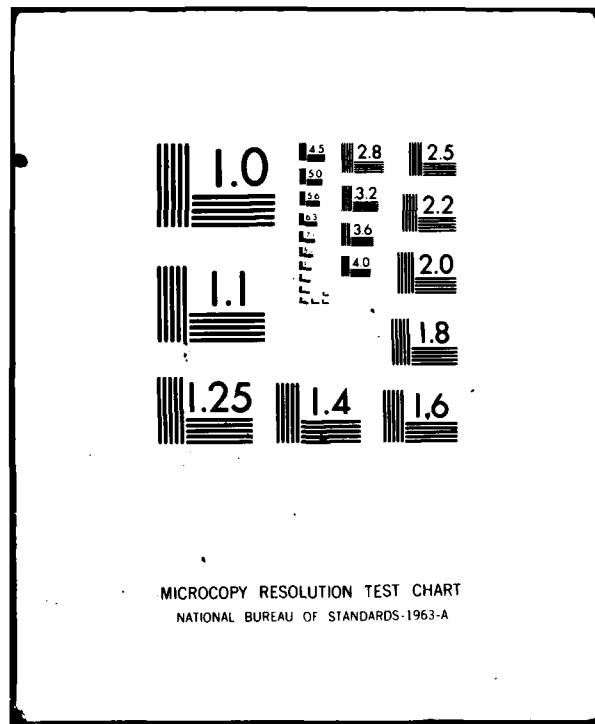
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# Technical Note

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**title:** DECELL USERS MANUAL-A FORTRAN IV PROGRAM FOR  
COMPUTING THE STATIC DEFLECTIONS OF STRUCTURAL  
CABLE ARRAYS

**author:** S. Sergev

**date:** August 1980

**sponsor:** Naval Facilities Engineering Command

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## CIVIL ENGINEERING LABORATORY

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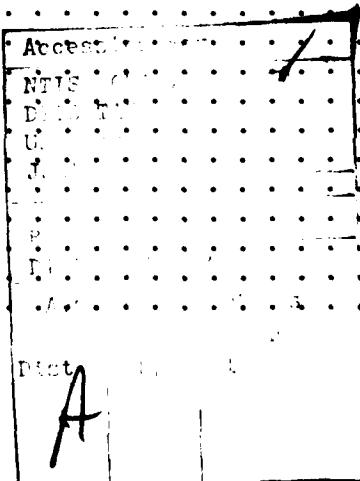
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## PREFACE

The Civil Engineering Laboratory (CEL), under sponsorship of the Naval Facilities Engineering Command, is engaged in a program of developing numerical tools for analyzing cable systems. As part of this work the NRL-written DESADE program has been used. In the course of using DESADE several improvements and additions have been made. The modifications are for the most part minor and serve to increase the accuracy of the mathematical modeling and to add user conveniences.

This report documents these modifications in the form of a revised users manual. (Much of the text of the original manual is used without modification.) To distinguish the updated program from the original NRL version, the program has been renamed DECELL for DESADE, CEL version one.

CEL's modifications were in five general areas:

1. Force calculations
2. Current field definition
3. Plotting options
4. Miscellaneous user conveniences
5. Iteration control

### Force Calculations

Drag force and weight of cable sections covered by in-line devices have been deleted. (This assumes an in-line device that terminates the cable at each end of the device; floats that are in-line and envelope the cable must have their buoyancy adjusted by the weight of the enveloped cable segment.) This addition has a relatively minor effect except when in-line devices envelope a significant portion of a cable.

Calculation of tangential drag has been added to both cables and in-line devices.

### Current Field Definition

The capability to accept a current field defined by 2, 3 or 4 current meter strings of up to 25 meters each has been added. Since much current meter data is referenced to magnetic north, the cable structure can be referenced to the current field by specifying the angle between the structure's X-axis and magnetic north.

The specification of current direction has been changed to be consistent with oceanographic terminology: a 90° current flows due east.

An option has been added to specify the input current velocity units; all velocities within an NDAT case must be the same units.

### Plotting Options

Options have been added to plot the current field defined by two or more current meter strings and to plot the cable structure in either its deformed or undeformed configuration. Perspective or plan or elevation views can be depicted.

### Miscellaneous User Conveniences

Required title cards have been added for the cable structure source deck and for each parametric case.

The specification of indexed and unindexed devices has been simplified. User selected devices now are automatically indexed, in order, by their location along a cable.

The changes allowed in a parametric study deck are such that the physical appearance of the array could be altered in the parametric case so much that referencing displacements to the original no-current case is illogical. An option has been added to declare any parametric case as the new no-current reference case. Displacements are printed referenced to both the original no-current case and to the present parametric reference case. The reference parametric case can be redefined any number of times since the original no current case is retained for the duration of the problem.

The error detection and display scheme has been altered. Errors that are detected by DECELL cause the entire input deck to be listed. Then, the cards with errors are flagged with a coded error number. The coded error message text is printed below the input card listing. All cards are scanned for errors; however, only the first error on a particular card is detected. The error messages are identical to those in the original DESADE manual except that only the portion of the message applicable to the card type is printed.

In some cases it is desirable to be able to punch on cards the locations of particular devices for input to other programs. An option has been added to select, based on device weight, the devices whose location is to be punched.

### Iteration Control

Under some circumstances that have not been well defined, DECELL may either fail to converge or converge very slowly. To protect the user from high execution costs, iteration limits have been imposed. Iterative techniques are used to satisfy the imaginary reaction displacement constraints and to obtain the structure shape. Both iteration processes have had limits imposed because both have been the cause of excessively high execution costs.

These modifications have added to the capabilities of DECELL and have made it a more useful tool for the cable structure analyst.

## INTRODUCTION

DECELL is a Fortran IV program for computing the ocean current-induced static deflections of undersea structural cable arrays. The solution algorithm is the Method of Imaginary Reactions (Refs 1,2)

combined with the method of successive approximations for treating position and configuration dependent forces (Refs 3,4).

As dimensioned, the program can handle arbitrarily configured arrays of up to 22 cables. The cables can be electromechanical, wire rope, or synthetic. Any number of discrete devices (buoyancy elements, current meters, tensiometers, etc.) may be incorporated in the array.

Certain limitations are placed on the structural characteristics of the arrays which can be analyzed by this program. These limitations are as follows:

1. No cables or cable segments may lie on the ocean floor. (No surface or bottom interaction is modeled, thus a cable may hang below the lowest anchor point.)
2. The dimensions of each discrete device must be small compared to overall array dimensions. Thus, for example, the application of this program to the analysis of an anchorage for a submerged submarine is not valid.
3. All parts of the array must be submerged. Thus, an array containing a surface buoy cannot be validly analyzed using this program. (The reason for this is that a surface buoy generates only one geometric constraint on its location.) An exception occurs when all three coordinates of a device on the surface can be specified - for example, the coordinates of a ship handling a crown line.

Also, certain hydromechanical assumptions are incorporated in the program as written. These are as follows:

1. The only hydrodynamic force considered to be acting on the discrete devices is a drag force. For in-line devices a normal drag coefficient and a tangential drag coefficient can be specified. For a free device, only the normal drag coefficient is to be specified. Lift forces are neglected as being small compared to the weight, buoyancy, and drag forces on these devices.
2. The only hydrodynamic force considered to be acting on the cable is a drag force. This drag force consists of both normal and tangential components and consequently two drag coefficients (normal and tangential) are to be specified for each cable.
3. The current option 1 is depth dependent in magnitude, unidirectional and horizontal. The current option 2 permits direction and magnitude variation as a function of depth. The current option 3 also permits magnitude and direction variation as a function of depth. This option requires two, three or four "strings" of depth dependent velocity data (where the strings are located at arbitrary points). These velocity data are used within the code via interpolation or extrapolation to obtain the velocity at any arbitrary point in space. In all cases the vertical component of velocity is assumed to be zero.

An option for parametric studies (changes in weights, diameters, cable lengths, anchor locations, etc.) is included in the program. DECELL also contains a series of error checks which insure that all input data are properly formulated.

Perspective plotting package SSP has been incorporated into DECELL to plot the deformed and/or undeformed configuration of the array.

The program uses the internally generated nodal points of the cables as the points to be plotted.

Scratch files 3, 4 and 10 must be available for use in the plotting package SSP.

#### Computer Requirements

As written, DECELL should be compilable on most Fortran IV compilers with Boolean algebra capabilities. Memory requirements for the program are approximately 206,000 (octal) words in single precision. Access to one, two, or three magnetic tape units, depending on the I/O options chosen, is required by the program.

#### Program Operation

The overall operation of the program DECELL is shown in the flow diagram in Figure 1. Numerical examples in Appendix A and the source language listing of the program is given in Appendix B.

#### Array Description

Typical cable arrays which can be analyzed using DECELL are shown in Figures 2a-2d. The figures also show the numbering and coordinate system conventions required for transmitting the array geometry to DECELL. These conventions are as follows:

1. The cables comprising the array must be numbered consecutively from one to the total number of cables in the array (C1, C2, ... in Figure 2). Each cable so designated must have uniform properties (weight, drag coefficients, diameter, and constitutive relation) along its length. A change in property also requires a change in cable number as illustrated in Figure 2a.
2. The termination points of the cables in the array are called junctions. A junction may designate an anchor, the intersection point of two or more cables, or the free end of a cable such as illustrated by junction J9 in Figure 2c. The junctions must also be numbered consecutively from one to the total number of junctions in the array (J1, J2, ... in Figure 2).
3. A fixed, right-handed (X, Y, Z) Cartesian coordinate system must be chosen to describe the configuration of the array in space. This coordinate system is called the array-referenced coordinate system. The origin of the coordinate system can be arbitrarily located. The Z axis must be defined parallel to the direction of gravity and increasing upward. All distances are measured in feet.

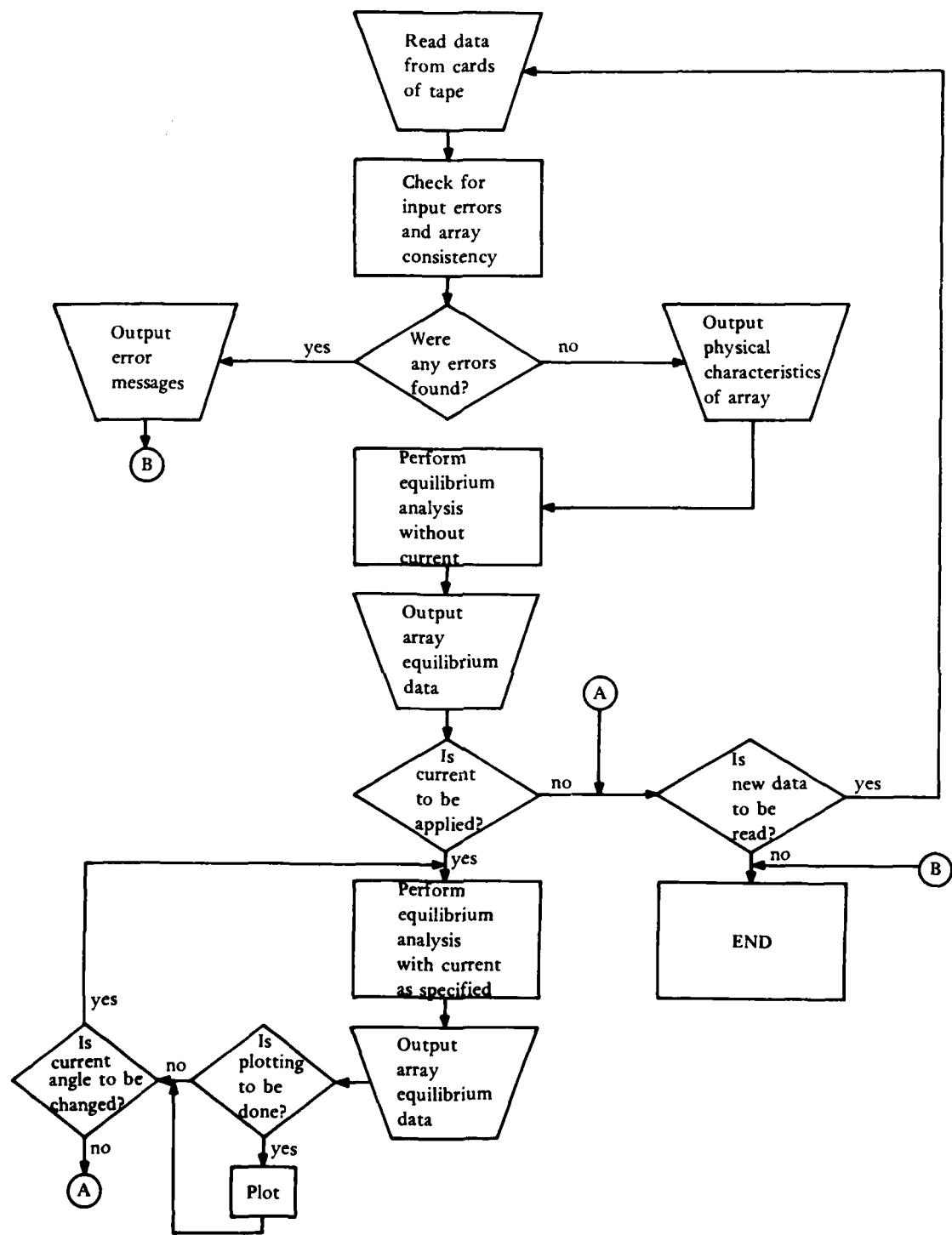


Figure 1. Generalized flow diagram of DECEL1 operation.

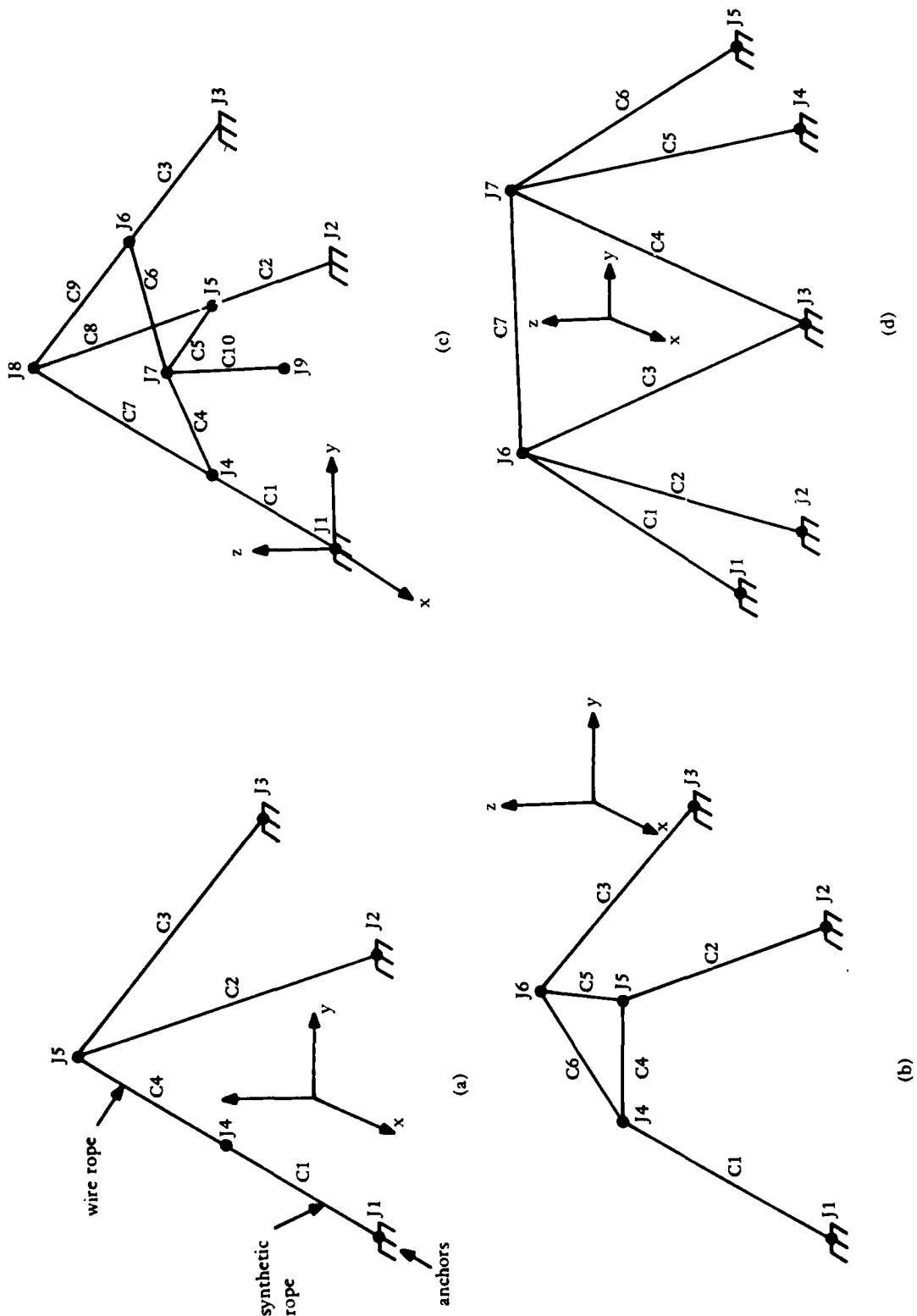


Figure 2. Typical cable arrays which can be analyzed using DECEL1.

- The junction numbers corresponding to anchors and the coordinate of the anchors must be tabulated according to the scheme illustrated in Table 1.

Table 1. Anchor Tabulation

<u>Column 1</u>	<u>Column 2</u>	<u>Column 3</u>	<u>Column 4</u>
Junction number of Anchor	X coordinate (ft)	Y coordinate (ft)	Z coordinate (ft)

Anchors are defined to be any fixed end point of a cable; thus an "anchor" can be placed on the bottom or at the surface or anywhere within the water column.

#### Reduction to a Statically Determinate Array

Before an arbitrary cable array can be analyzed by DECELL, a sufficient number of cuts must be made in the array to reduce it to a statically determinate structure. The effects of the constraints removed by these cuts are replaced by imaginary and equilibrating reactions (Refs 1,2).

The number of cuts required to reduce a cable array to a statically determinate structure is determined uniquely from the relation

$$\begin{aligned} \text{number of cuts} &= \text{number of cables} + \text{number of anchors} \\ &\quad - \text{number of junctions} \end{aligned} \tag{1}$$

Certain rules must be adhered to as the required cuts are made. These rules are as follows:

- All required cuts must be made at points directly adjacent to array junctions - that is at end points of the cables comprising the array.
- The first group of cuts must be made so as to release all but one cable from an anchor.
- The remaining cuts (if required) are made within the array structure and must be located so as not to break the array into two (or more) parts.
- As cuts are made, each new cut must be assigned a consecutive junction number, continuing from the last-used junction number. Also, the junction number (in the original array) at which the cut is made must be tabulated.

In effect, applying rules 1-3 reduces the array to the equivalent of a topological tree. As the name implies, this is a continuous structure containing only one fixed point and for which a unique (nonduplicative) path exists from any point to any other point.

Examples of proper reductions to statically determinate structures for the arrays illustrated in Figures 2a-2d are shown in Figures 3a-3d, respectively. In each of these figures, the left-hand schematic shows the reduced array while the right-hand schematic depicts the topological tree representation of the reduced array. The information required by rule 4, which represents geometric constraints on the reduced array, is tabulated below the left-hand schematic in each figure.

Finally, it is necessary to define directions of increasing arc length along the cables comprising the array. The tree representation of the reduced array is used primarily for this purpose. These directions, indicated by the arrowheads in the right-hand schematic of each figure, are identified by starting from the base of the tree and climbing "up" the tree.

Let the measure of arc length along a cable be denoted by  $s$  which increases from zero to the total length of the cable  $L$ . Then, the required information on increasing directions of arc length can be summarized in terms of array junctions as shown in the table below the right-hand schematic in each figure.

Once an array has been reduced to the state represented by Figure 3, it is amenable to analysis by the program DECEL1.

#### Coordinate Systems

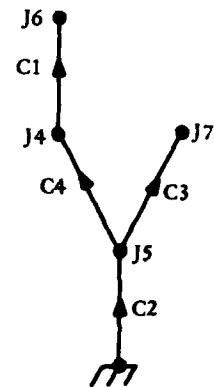
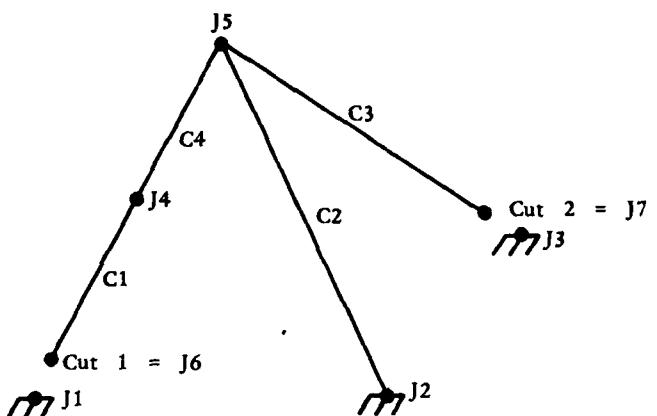
There are two coordinate systems used for inputting the data to DECEL1. They are the magnetically aligned reference coordinate system ( $N$ ,  $W$ ,  $Z$ ) and the array or laboratory reference coordinate system ( $X$ ,  $Y$ ,  $Z$ ). The two coordinate systems share the same origin and the same  $Z$ -axis;  $Z$  is positive upward. Consequently, the two coordinate systems can differ from one another by an arbitrary angular rotation in the horizontal plane which is denoted by  $\phi$ . For arbitrary locations on the earth, the magnetic axes N-S and E-W are preestablished. Consequently, the angular rotation of the array-referenced coordinate system is referenced to the magnetic axes. In particular,  $\phi$  is the angle between the  $N$ -axis and the positive  $X$ -axis. A positive rotation of the  $X$ -axis with respect to the  $N$ -axis is in the clockwise sense. Figure 4 illustrates the two coordinate systems.

The direction of positive rotation is in the clockwise sense in the magnetically aligned coordinate system. The zero degree reference is taken as the  $N$ -axis.

All current data to be input into the program are to be referenced with respect to the magnetic coordinate system. For example, a current having an inclination of  $0^\circ$  is flowing due north; a current with  $270^\circ$  inclination is flowing due west.

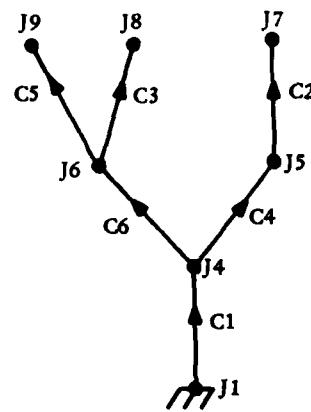
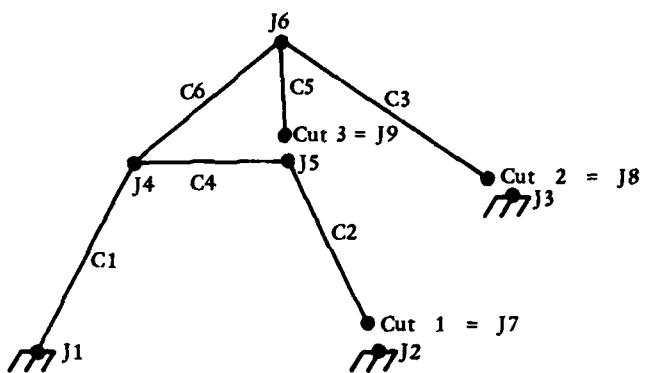
When current field input option 3 is selected, it is necessary to specify the locations on the ocean surface (horizontal plane) of the stations where current data have been gathered (relative to the  $N,W,Z$  coordinate origin). Typical examples of locations of such stations might be:

100 ft N by 3000 ft W = ( 100, 3000)  
700 ft S by 1500 ft E = (-700, -1500)  
0 ft N by 800 ft E = ( 0, -800)  
400 ft N by 450 ft W = ( 400, 450)



<u>Cut No.</u>	<u>Junction No. Assigned To Cut</u>	<u>Junction No. At Which Cut Made</u>	<u>Cable No.</u>	<u>Junction No. At s = 0</u>	<u>Junction No. At s = L</u>
1	6	1	1	4	6
2	7	3	2 3 4	2 5 5	5 7 4

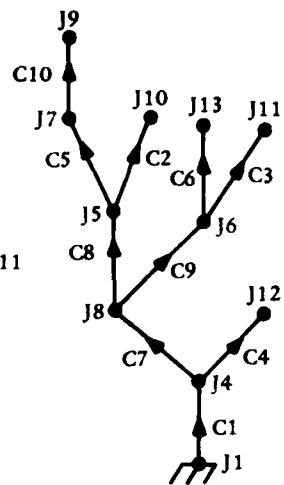
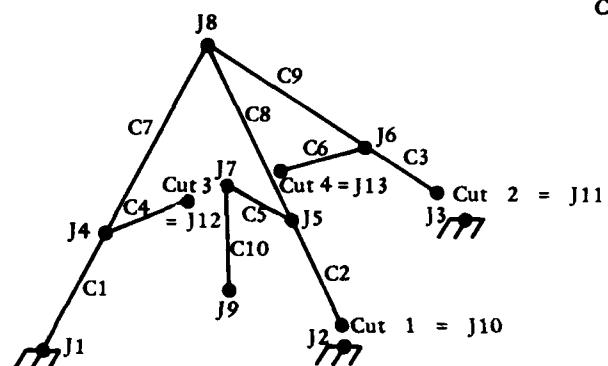
(a)



<u>Cut No.</u>	<u>Junction No. Assigned To Cut</u>	<u>Junction No. At Which Cut Made</u>	<u>Cable No.</u>	<u>Junction No. At s = 0</u>	<u>Junction No. At s = L</u>
1	7	2	1	1	4
2	8	3	2	5	7
3	9	5	3 4 5 6 6	6 4 6 9 4	8 5 9 6

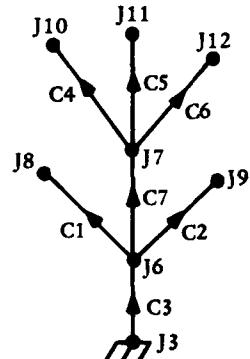
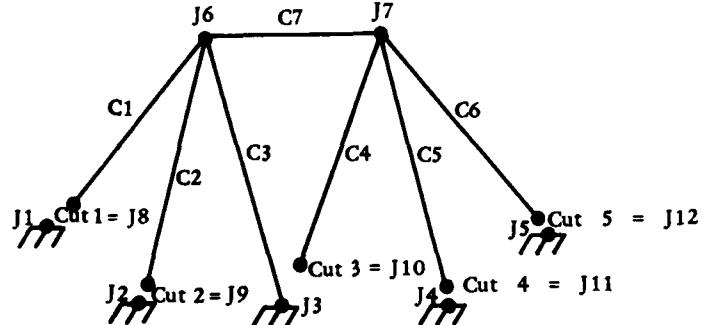
(b)

Figure 3. Examples of proper reductions to statically determinate structures for the arrays shown in Figures 2a and 2b.



<u>Cut No.</u>	<u>Junction No. Assigned To Cut</u>	<u>Junction No. At Which Cut Made</u>	<u>Cable No.</u>	<u>Junction No. At s = 0</u>	<u>Junction No. At s = L</u>
1	10	2	1	1	4
2	11	3	2	5	10
3	12	7	3	6	11
4	13	7	4	4	12
			5	5	7
			6	6	13
			7	4	8
			8	8	5
			9	8	6
			10	7	9

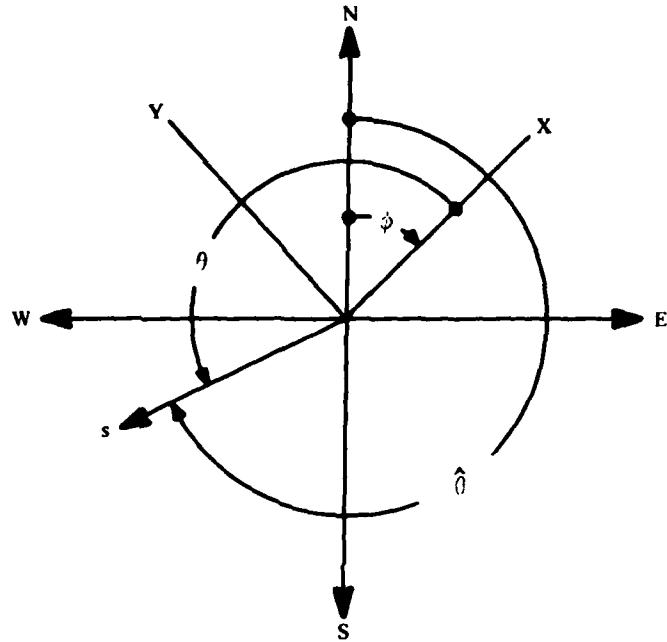
(c)



<u>Cut No.</u>	<u>Junction No. Assigned To Cut</u>	<u>Junction No. At Which Cut Made</u>	<u>Cable No.</u>	<u>Junction No. At s = 0</u>	<u>Junction No. At s = L</u>
1	8	1	1	6	8
2	9	2	2	6	9
3	10	3	3	3	6
4	11	4	4	7	10
5	12	5	5	7	11
			6	7	12
			7	6	7

(d)

Figure 3. Examples of proper reductions to statically determinate structures for the arrays shown in Figures 2c and 2d.



$$s = \sqrt{N^2 + W^2}$$

$$X = s \cos \theta$$

$$\theta = 360 + \beta - \hat{\theta}$$

$$Y = s \sin \theta$$

In the magnetic coordinate system the N,W axes are positive. (N,W) form a coordinate pair of a right handed coordinate system. The positive direction of rotation  $\hat{\theta}$  in the (N,W) coordinate system is clockwise with the zero degree reference being the N - axis. The array coordinate system (X,Y) system. The relationship between the two systems is given above.

Figure 4. Description and relationship between the magnetic and array referenced coordinate systems.

Above (on the right), is an example of how such locations should be interpreted for input preparation as coordinate pairs. Note that the north-west quadrant is the first quadrant of a right-handed coordinate system. Consequently, north and west are positive axes while south and east are the negative axes. When current field input option 3 is selected, the current data are printed out in both the magnetic and array-referenced coordinate systems.

The specification of the anchor locations is accomplished with respect to the array-referenced (X, Y, Z) coordinate system. All internal calculations within DECELL are performed with respect to the array-referenced coordinate system. The (X, Y, Z) coordinate system is also right-handed. In the horizontal plane in this frame of reference the direction of positive rotation is counter-clockwise with the positive X-axis being the zero degree reference.

#### Directions of Positive Rotation

<u>Reference System</u>	<u>0° Reference</u>	<u>Positive Rotation</u>
Magnetic	N-axis	clockwise
Array	X-axis	counter-clockwise

#### Current Field - Input Option 0

There is an input option for determining the static deflections of a cable system immersed in a currentless environment. This is current field input option 0. This option is automatically processed when any of the subsequently described current field input options are exercised. It can be exercised independently.

#### Current Field - Input Option 1

The current field option 1 is taken to be unidirectional and horizontal, though depth dependent in magnitude. The direction of the current is specified from the magnetic north axis by using the ANG card. [Within the code, the current is referenced to the array coordinate system for calculation purposes. Thus, if the direction of the flow with respect to the X-axis is denoted by  $\theta$ , the current field is expressed by:

$$V_1 = V(Z)(\underline{e}_1 \cos \theta + \underline{e}_2 \sin \theta)$$

Here,  $\underline{e}_1$ ,  $\underline{e}_2$  are unit base vectors with respect to the X- and Y- axes, respectively.]  $V(Z)$  specifies the magnitude of the current as a function of depth, Z. This functional relationship must be tabulated as in Table 2.

Table 2. Current Tabulation - Option 1

<u>Column 1</u>	<u>Column 2</u>
Z coordinate (ft)	V(Z) knots

Up to 25 rows are permitted in Table 2. At least one of the Z-coordinates in Table 2 must be less than or equal to the Z-coordinate of the lowest anchor. A sorting scheme is invoked within the program that arranges Table 2 data according to ascending values of Z. Such sorting is necessary within the program for the determination of the current of an arbitrary depth. This is accomplished via a linear interpolation of the currents using the data at the two depths encompassing the depth of interest.

Figure 5 illustrates the magnetic-referenced coordinate system and the linear interpolation of the velocity between given data points.

For current field input option 1, the directionality of the current is a constant for the entire velocity field. Also, for any point (X, Y) on the plane (Z = constant), the value of velocity is invariant.

#### Current Field - Input Option 2

Current field input option 2 is a slight generalization of the current field input option 1. The generalization involves allowing the current direction  $\theta$  to vary with depth. The input specification for this option requires depth Z, current magnitude and current direction from the magnetic north axis. The positive direction of rotation is clockwise in the magnetically-aligned reference coordinate system and a zero degree current flows due north. The current specification for option 2 requires a tabulation as in Table 3.

Table 3. Current Tabulation - Option 2

<u>Column 1</u>	<u>Column 2</u>	<u>Column 3</u>
Z-coordinate	V(Z) magnitude, knots	$\theta(Z)$ direction, degrees from magnetic N-axis, positive in clockwise sense

Up to 25 rows are permitted in Table 3. The velocity sorting scheme is invoked by the program. One entry for this data must correspond to a depth less than or equal to the Z-coordinate of the lowest anchor. The above current magnitude and direction data are used to generate velocity components along the (X, Y) axes. To obtain the velocity at an arbitrary depth, linear interpolation is performed using the (X, Y) velocity components above and below the depth of interest; the angular direction of the current is also found by interpolation.

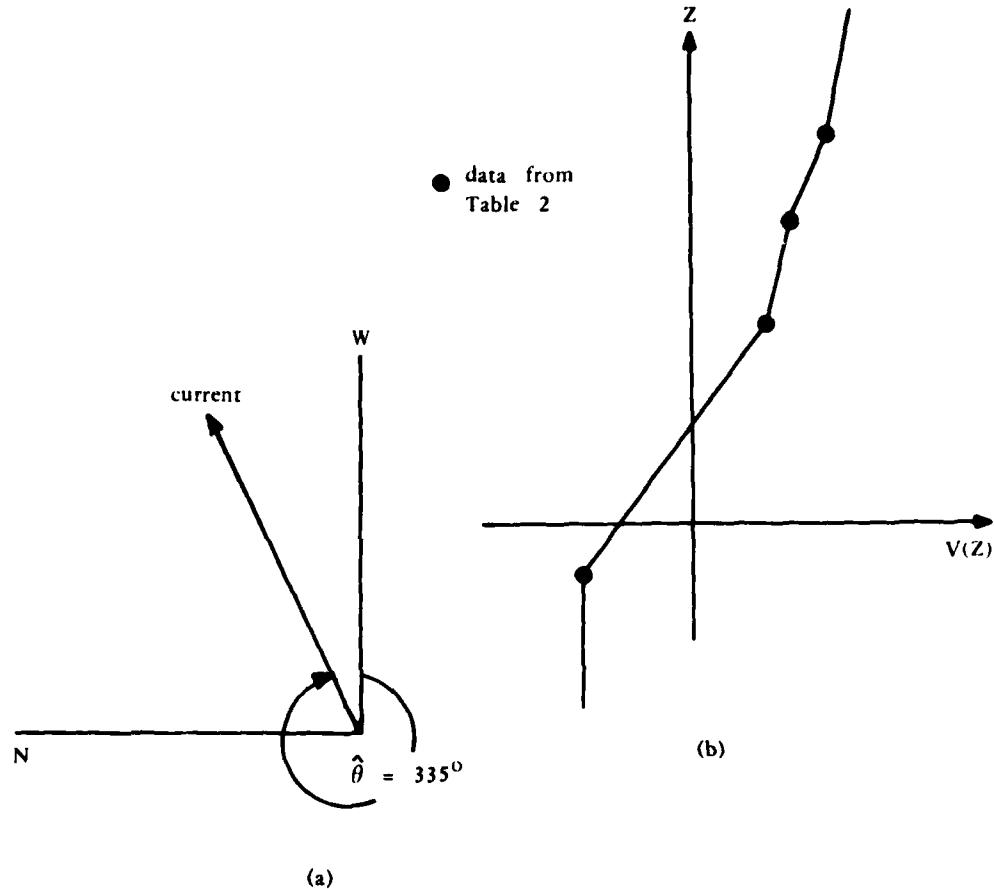


Figure 5. Current field option 1 used in DECEL1 (a) Current angle,  $\theta$ , (b) Current profile,  $V(Z)$ .

For current option 2, the value of velocity at any ( $X$ ,  $Y$ ) point on the plane  $Z = \text{constant}$  is invariant.

An ANG card can be used to rotate the entire current profile in the same manner that a unidirectional current profile is rotated.

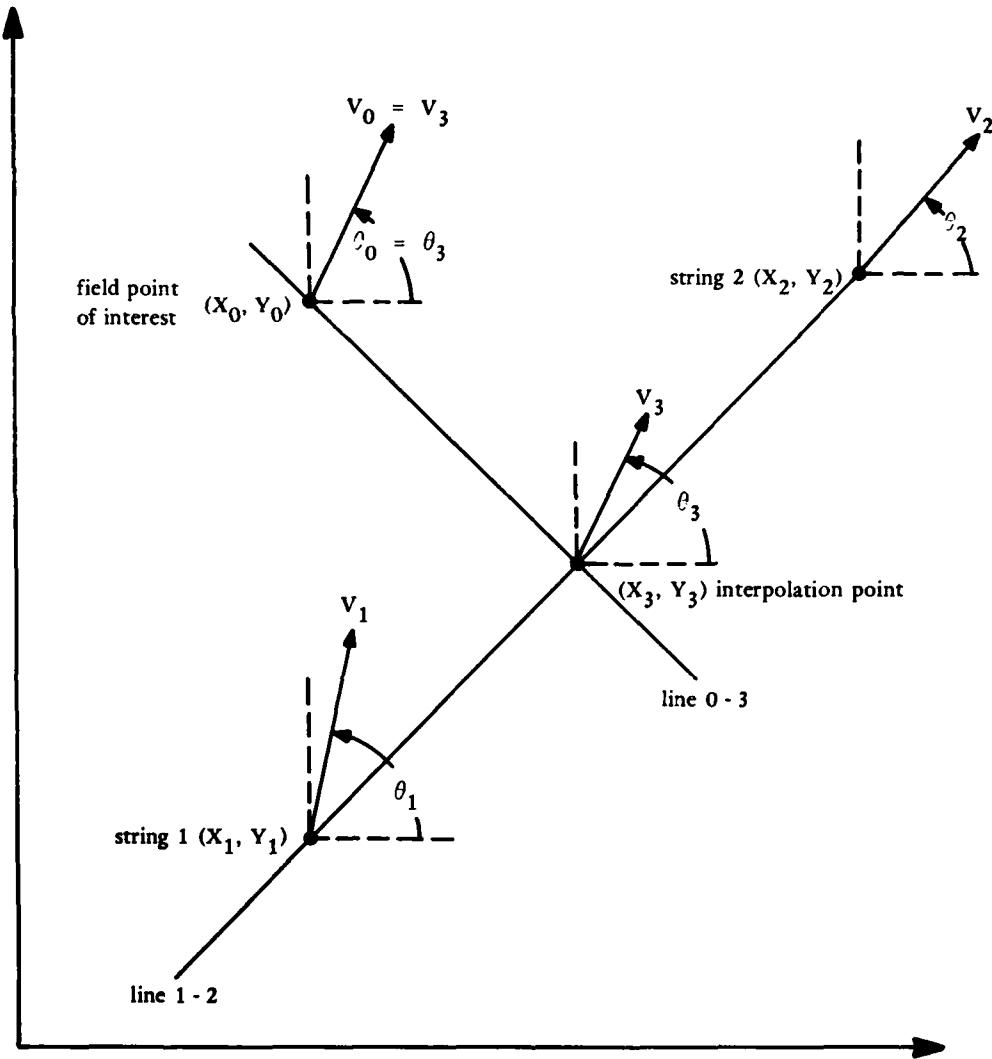
#### Current Field - Input Option 3

The current field input option 3 employs a linear interpolation/extrapolation scheme on current (magnitude and direction) data to give velocity variation in horizontal planes. When this option is invoked the program expects current data from 2, 3 or 4 current meter strings. Up to 25 measurements of current data can be contained on each string. For each string the first data entry must be at a depth equal to or less than the lowest anchor. The depth dependent data on the various strings do not have to correspond one to the other. That is, if on one string current data are obtained at  $Z_1$ ,  $Z_2$ ,  $Z_3$ , ...  $Z_p$ , then on the other strings data can be collected at completely different depths. This current field input option has been designed to treat mildly varying current fields. It does not provide acceptable results for eddy currents or reverse shear flows. The interpolation/extrapolation scheme to obtain the velocity at an arbitrary point in the field works as follows:

Case of 2 Strings. The field point  $(X_o, Y_o, Z_o)$  is determined where the velocity is to be found. On the plane  $Z=Z_o$  there are three points of interest. They are  $(X_1, Y_1, Z_1)$ ,  $(X_1, Y_1, Z_o)$  and  $(X_2, Y_2, Z_o)$  where the last two points denote the location on the plane  $Z=Z_o$  at the meter strings. At each of these locations current magnitude and direction data are determined by a straight line interpolation of the data values given directly above and below the  $Z_o$  elevation. Figure 6 illustrates the situation after this linear interpolation. There,  $(V_1, \theta_1)$  and  $(V_2, \theta_2)$  are obtained from the vertical interpolation just mentioned.

A line normal to the line connecting  $(X_1, Y_1)$  and  $(X_2, Y_2)$  through the field point  $(X_o, Y_o)$  is constructed to locate the interpolation point  $(X_3, Y_3)$ . The point  $(X_3, Y_3)$  lies on the line joining  $(X_1, Y_1)$  and  $(X_2, Y_2)$ . Linear interpolations are now performed to find  $V_3$  and  $\theta_3$  from the corresponding values at  $(X_1, Y_1)$  and  $(X_2, Y_2)$ . The current  $(V_3, \theta_3)$  are assumed to prevail at all points along the normal line. Hence,  $(V_3, \theta_3)$  provide the description of the current at the field point  $(X_o, Y_o)$ .

Case of 3 Strings. Suppose the field point is  $(X_o, Y_o, Z_o)$ . The current magnitude and direction are determined by linear vertical interpolation at the three string locations  $(X_1, Y_1, Z_1)$ ,  $(X_2, Y_2, Z_2)$  and  $(X_3, Y_3, Z_3)$ . The corresponding velocity data obtained at these locations are  $(V_1, \theta_1)$ ,  $(V_2, \theta_2)$  and  $(V_3, \theta_3)$ . At the string location on the horizontal plane ( $Z=Z_o$ )  $V_1$ ,  $V_2$  and  $V_3$  are amplitudes through which a velocity plane can be passed. (A unique plane can be passed through any three non-collinear points.) The velocity  $V_o$  at the field point  $(X_o, Y_o, Z_o)$  then can be obtained by determining the amplitude on the velocity plane corresponding to the position  $(X_o, Y_o, Z_o)$ . The procedure is exactly the same for the determination of the current direction  $\theta_o$ . For this quantity a direction plane has to be established using the direction amplitudes  $\theta_1$ ,  $\theta_2$  and  $\theta_3$ .



Line 0 - 3 is orthogonal to line 1 - 2. The velocities  $(V_1, \theta_1)$  and  $(V_2, \theta_2)$  are obtained by linearly interpolating string 1 and string 2 data, respectively. The velocity of any point along line 1 - 2 can be obtained by linear interpolation/extrapolation of the velocities  $(V_1, \theta_1)$ ,  $(V_2, \theta_2)$ . The assumption is made that the velocity  $(V_3, \theta_3)$  of an arbitrary point  $(X_3, Y_3)$  on line 1 - 2 is propagated along the orthogonal trajectory to that line at that point.

Figure 6. Interpolation/extrapolation in the case of 2-string data.

Case of 4 Strings. The field point is  $(X, Y, Z)$ . The string points are  $(X_1, Y_1, Z_1)$ ,  $(X_2, Y_2, Z_2)$ ,  $(X_3, Y_3, Z_3)$  and  $(X_4, Y_4, Z_4)$ . Through any three of the string points the procedure used in the preceding case can be repeated exactly. There are four independent ways that three points can be selected from four points, namely:  $(1, 2, 3)$ ;  $(1, 3, 4)$ ;  $(1, 2, 4)$ ;  $(2, 3, 4)$ . The current is determined at the field point by averaging the results obtained by applying the case of three strings four times to the four combinations of points just indicated.

#### TANGENTIAL DRAG

The tangential drag computation on the cable is straightforward and is based on the expression

$$\Delta F_{TD} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix} = \frac{1}{2} \rho [\pi D(1+\epsilon)] C_{DT} V_{TM} V_T \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$$

where  $\Delta F_{TD} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$  = tangential drag force component per unit length in the direction X, Y or Z

$V_T \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$  = tangential velocity component along X, Y or Z axis

$V_{TM}$  =  $\sqrt{V_T^2(X) + V_T^2(Y) + V_T^2(Z)}$ , magnitude of tangential velocity

$C_{DT}$  = tangential drag coefficient

$\rho$  = density of fluid

D = cable diameter

$\epsilon$  = strain developed by cable tension

The above calculation forms a part of the hydrodynamic cable drag force. The hydrodynamic force is comprised of a normal drag and a tangential drag.

#### CABLE DEVICES

In FUNCTION EFORCE (I, M, N) the tangential drag contribution to in-line devices is included in the drag calculation. It is required therefore to supply a tangential drag coefficient for each in-line device as input.

For in-line cable devices the weight of the cable and the hydrodynamic drag over a portion of the cable covered by an in-line device is deleted. Cable devices are referred to as in-line or free devices (two types). All cable devices are numbered automatically within the program. The numbering is accomplished sequentially with respect to cable number

and location of the device away from its  $s=0$  end. That is, if on cable 1 there are three cable devices located at  $s=s_1$ ,  $s=s_2$ , and  $s=s_3$  with a  $s_3 > s_2 > s_1$ , then cable device indices 1, 2, 3 refer to devices located on cable 1 at  $s=s_1, s_2, s_3$ , respectively.

#### REFERENCE CONFIGURATION

An option exists to specify a particular parametric study case as a new no current reference configuration. Displacements with respect to the new no current reference configuration as well as the displacement from the original no current reference configuration are part of the output.

#### ITERATION CONTROL AND EXECUTION ERROR MESSAGES

To protect the user from excessively high execution costs coupled with the risk of not receiving any output, iteration limits have been added to DECELL. Two separate iteration processes are involved: one attempts to satisfy the displacement constraints, where the cuts are made, imposed by the COMP card; where the other determines the structure's shape. Both iteration processes have been observed on rare occasions to converge very slowly, if at all.

The first iteration process deals with the imaginary reactions. The associated displacement errors have been observed to be large and to change slowly in some slowly convergent problems. An arbitrary definition of slow convergence coupled with a maximum iteration limit is used to terminate execution of a particular parametric case. Slow convergence has been defined to occur when, after half of the iteration limit is achieved, the displacement error is large (100 times the COMP value) and the error is changing by less than the COMP value per iteration. Iteration is terminated due to slow convergence with the message: SLOW CONVERGENCE AFTER XXX ITERATIONS. The previous and present displacement error values are printed to aid in determining how closely the solution has converged. If only one of the slow convergence criteria is satisfied iteration will continue until convergence occurs or the iteration limit is reached. Iteration is terminated due to reaching the iteration limit with the message: NO CONVERGENCE IN XXX ITERATIONS and the present and previous displacement error values are printed.

The second iteration process to determine the structure's shape occurs after the imaginary reaction iteration has been successful. This process has been observed on some occasions to oscillate about the correct solution. The normal iteration process is allowed to continue until half of the nodal position iteration limit is reached. At this point, the solution is arbitrarily assumed to be oscillating and a half-step iteration scheme is imposed (the iteration process is unchanged except that each node is allowed to move only half as far as calculated). This half-step technique continues until the iteration limit is reached or convergence occurs. Execution of the parametric case is terminated with the message: PROGRAM DID NOT CONVERGE AFTER XXX ITERATIONS, PARAMETRIC CASE TERMINATED. The displacement error is printed and the full output for the case is printed preceded by the message: APPROXIMATE RESULTS PRINTED. The user must judge if an adequate displacement error has been achieved for the results to be meaningful.

### What To Do If . . .

When execution has been terminated by reaching the imaginary reaction iteration limit, several options are still available. The iteration limit (field 4 of the COMP card) can be increased; however, this probably will have to be done in conjunction with an increase in the COMP value. The COMP value should still be kept in a range that will be judged to produce usable results. The error values printed upon execution termination will give an idea of how much the COMP value will have to be increased.

In some cases, the desired current is too strong to apply in one step; strong currents have caused the imaginary reaction iteration limit to be reached. To handle this and other sensitive cases, an option has been added to apply the current in increments (field 11 of the NDAT card). Using this option, the program iterates to a solution for the first current increment as if this were the total current to be applied. Then the current is incremented and the process is repeated. An option exists to print the solution for each increment of the current (see field 11 of the NDAT card). This technique has been highly effective in obtaining solutions in high currents up to 10 knots.

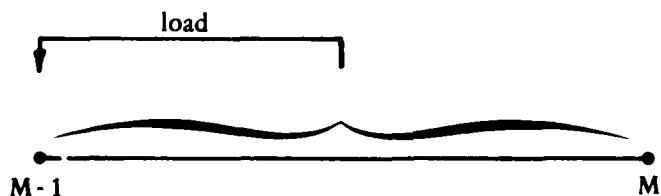
### DECELL USER EXPERIENCE

In the course of using DECELL a wide variety of structures in various current profiles have been analyzed. Some results have been compared with experimental data with close agreement (Ref 7). Other cases have been cross-checked against other computer models again with good agreement. The program is easy to use to the point that a user with a general engineering background can use the manual to formulate the required input and expect to receive back usable results once obvious input errors are corrected. The ease of use is an exceptional attribute of the program.

In the course of making modifications to the program a great deal of insight has been gained regarding the mathematical modeling. Many of the details are of no importance to the user. However there are several characteristics that the user should be aware of; these deal with the internal distribution of loads, non-convergent problems, and the convergence parameter.

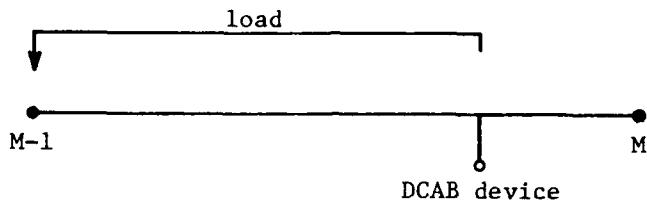
### Load Distribution

Loads (weight and drag) are generated from three sources: cables, cable devices, and junction devices. Cable forces due to drag and weight are calculated for the cable length between two nodes [length = (total cable length)/(no. of elements in the cable)]. (See CAB card.) The forces are assigned to the M-1 node as shown below:



Clearly, the smaller the distance between the nodes, the more accurate the mathematical representation.

Loads due to devices on the cable (DCAB card) are modeled in a similar way except that the device is physically located at a specific point along the cable between the two nodes. The DCAB loads are modeled as shown below:



This is a good representation when the device is actually near node (M-1). However, when the device is near node M and the distance between the nodes is large, this may be a poor representation. This is not to say the computer results will be grossly in error; this depends upon the size and number of DCAB devices. If the devices are few and/or small such that the system is cable-load dominated, the results should be acceptable.

Probably the most serious error will arise when there are few elements and the DCAB devices produce large static or drag loads. In this case large loads may be assigned to locations quite distant from their actual point of application.

Loads due to DJNC devices are most accurately modeled. The loads are assigned exactly where the device is located.

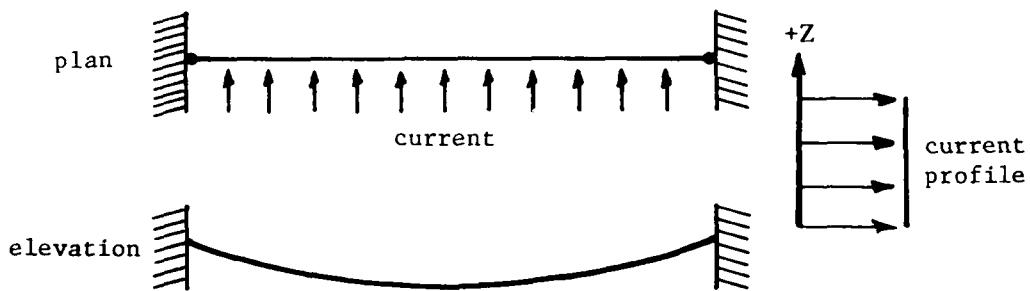
It may appear that a better modeling of cable and DCAB loads could be achieved by proportioning the loads between the appropriate adjacent nodes. However, this single change is not consistent with other internal force accounting schemes. To implement force proportioning, a major re-write of the program would be required; this has not been done.

As the program stands, the majority of problems can be analyzed with wholly satisfactory results even ignoring the way loads are distributed. Where the load distribution scheme is judged by the user to pose a problem in obtaining a satisfactory model, the following suggestions are presented.

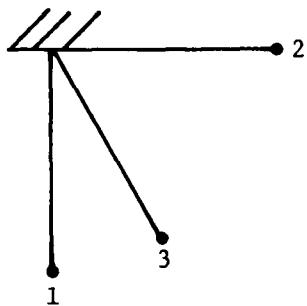
1. Model all cables with as many elements as possible (50). This will make the distance between nodes least so that DCAB loads will be assigned as close to the actual device location as possible.
2. Model large bodies as DJNC devices - loads will be assigned exactly where the device is located.
3. Model long cables as a series of shorter series-connected cables. This will aid in making elements short.

### Non-Convergent Problems

DECCELL treats statically determinate and statically indeterminate problems differently. The indeterminate problems are solved using the imaginary reaction technique (Ref 1). This is a powerful method and usually converges rapidly to a solution. (Reference 1 shows that the method is unconditionally convergent.) However, at least one case has been encountered where the method is at best very slowly convergent. The case involves a nearly neutrally buoyant cable hung in a catenary between two fixed points with a strong current acting perpendicular to the plane of the catenary:

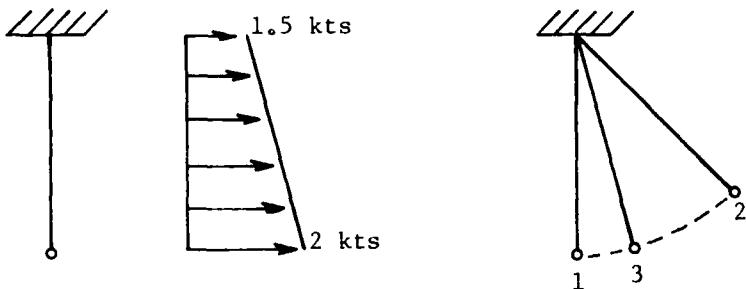


The positions attained by the cable during the iteration procedure are sketched below.



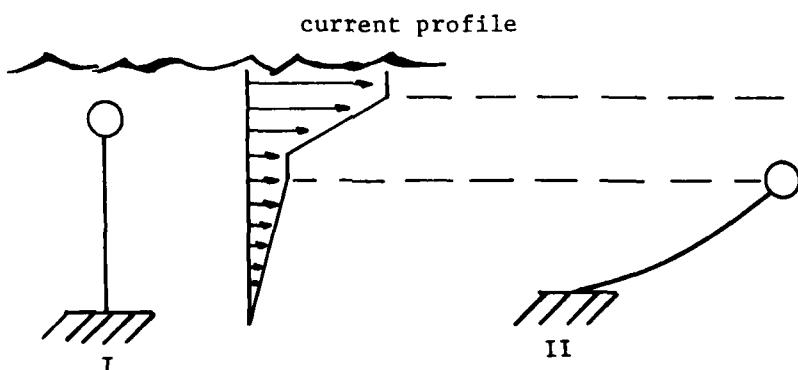
The cable is initially driven from the no-current position (1) to a nearly horizontal position (2). Here there is low- or no-normal drag to support the cable so in the next iteration it falls to position (3) (which may be coincident with position (1)). Internally, the iterations appear to oscillate between positions (2) and (3), and the solution fails to converge. Convergence can be achieved by reducing the current or by increasing the weight of the cable.

Statically determinate cases bypass the imaginary reaction routine, thus convergence is not as certain. There are combinations of current and geometry that interact in such a way as to appear to be unstable. An example is a lightweight anchor suspended from the surface in a current that increases with depth.



From the no-current position (1), the first iteration is to position (2) where the normal drag force is reduced both because of the orientation change (toward horizontal) and the reduced current in the new position. The reduced loading causes the system to attain position (3). The solution then oscillates between positions (2) and (3). Whether another case using this configuration will converge or not depends on both the magnitude of the current and the system weight. The particular case in question probably would converge in a more uniform current field or if the system weight were to be increased.

Another non-convergent case involved a sharp change in the velocity profile.



The subsurface buoy was initially in a high current zone (sketch I); in the first iteration it moved to a lower current region (sketch II). Here the high current was no longer acting on the system so on the next iteration the buoy was moved back into the high current regime. This case failed to converge primarily because the current shear was very near the initial depth of the buoy. Thus the buoy moved in and out of the high current on subsequent iterations. If the current shear had been much below the buoy and always acted only on the cable the solution most likely would have converged.

The above cases are presented simply to illustrate non-convergent problems. They by no means represent all non-convergent cases; however, they serve to illustrate what kinds of situations can be difficult to solve. If a user encounters a case that does not converge, the discussion of the examples here will help guide his reasoning in determining why non-convergence occurs.

In an attempt to improve the iteration technique, a half-step iteration technique has been introduced. The process is implemented only after 100 standard iterations have occurred. (The 100 iteration number has been relatively arbitrarily judged to be an indicator of oscillation during iteration.) After the first 100 iterations have occurred the next 100 iteration steps are calculated in the same way but the allowed displacement is reduced by one-half. This approach has not yet (as of this writing) been user tested; however, initial tests indicate that formerly oscillating cases will converge to a solution. As part of the half-step technique, an informative printout has been added that states the number of iterations required to achieve convergence. After 200 total iterations have occurred, iteration will be stopped, a message printed and the next parametric case will be analyzed. (The 200 iteration limit is arbitrarily taken as an indicator that the solution is not converging.)

#### Convergence Parameters

The variable on the COMP card is used as the convergence test parameter. The discussion of the COMP card defines a lower limit for the parameter that can be quite small. Iteration continues until two consecutive calculated positions for each node on the structure differ by less than the convergence parameter. Very small values of the convergence parameter can cause certain "sensitive" cases (such as some of those discussed above) to appear to oscillate. Adequate solutions and more rapid convergence can be obtained by picking a convergence parameter value that is consistent with the size of the structure being analyzed. The table below lists suggested convergence parameter values that are consistent with the structure size as determined by cable length.

<u>Cable Length (ft)</u>	<u>Convergence Parameter (ft)</u>
<10	<0.01
<100	0.01-0.1
<1000	0.1-1.0
<10,000	1.0-10.0
>10,000	5.0-20.0

These are only suggested values that may be used as initial values in order to insure that successful convergence does occur. For particular problems the user must judge for himself the adequacy of the convergence tolerance chosen. However, the user must realize that an unnecessarily small convergence parameter can cause a case to fail to converge mathematically even though a physically adequate solution has been reached in the iteration process.

## INPUT CARDS

Input cards to DECEL1 contain a 4-digit integer (-999 to 9999) card number in columns 1-4, a 4-character card type identifier in columns 5-8, and descriptive properties of the array in the remaining fields with the exception of the following input cards.

- 1 - Main Descriptive Title Card
- 2 - Parametric Descriptive Title Card
- 3 - Continuation Card for CAB
- 4 - Velocity Field for Current Option 3

The card number has two uses. First, it is used as a convenience for the user to define the order of the cards in the deck, should the deck be dropped. Secondly, it is used as a cross-check in changing parameters in the Parametric Study Source Deck: when a parameter on a card is to be changed, both the card number and type must match the card in the Cable Array Source Deck or an error will occur. In the Cable Array Source Deck, duplicate card numbers are detected as errors; however, any number of input cards may have the card number omitted with no errors.

**\*\* CABLE ARRAY SOURCE DECK CARDS \*\***

LUN CARD (optional card; if used it must be the first card in the deck)

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	~LUN	Right adjust
3	9-16	I8	Unit number of card reader	
4	17-24	I8	Unit number of line printer	
5	25-32	I8	Unit number of temporary storage tape	
6	33-40	I8	Input option (0 or 1)	See notes
7	41-48	I8	Blank if input option = 0. Unit number of source tape if input option = 1.	
8	49-56	I8	Output option (0, 1 or 2)	See notes
9	57-64	I8	Blank if output option = 0. Unit number of output tape or card punch if output option = 1 or 2.	
10	65-72		Not used	See notes
11	73-77		Not used	
12	78-80		Not used	

- NOTES:
1. The carot symbol (~) is used to indicate one blank column in the position shown.
  2. The LUN card is used to transmit the logical unit numbers of the I/O devices and the I/O options. The LUN card is optional. If it is omitted then input option 0 and output option 0 are the default options.

Two input options are available:

- 0 - The physical characteristics of the array are to be read from the cable array source deck (see CABLE ARRAY SOURCE DECK)
- 1 - The physical characteristics of the array are to be read from the cable array source tape (see CABLE ARRAY SOURCE TAPE)

**Three output options are available:**

- 0 - A structural output to the line printer (see  
STRUCTURAL OUTPUT)**
- 1 - A device location output to tape or cards (see  
DEVICE LOCATION OUTPUT)**
- 3 - both of the above**

**MAIN DESCRIPTIVE TITLE CARD**

Field	Columns	Format	Contents	Comments
1-10	1-80	8A10	Main descriptive title	See notes

**NOTE:** A single "Main Descriptive Title Card" must always follow the LUN card. If no title is desired a blank card must be inserted. This card does not adhere to the convention requiring a card number and card type, so that the entire card can be utilized for a title. If the LUN card is omitted then this must be the first input card.

NJNC CARD

<u>Field</u>	<u>Columns</u>	<u>Format</u>	<u>Contents</u>	<u>Comments</u>
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	NJNC	
3	9-16	I8	Number of junctions in original (unreduced) array	2-44
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The NJNC card is used to transmit the number of junctions in the original (unreduced array).

**ANC CARD**

<b>Field</b>	<b>Columns</b>	<b>Format</b>	<b>Contents</b>	<b>Comments</b>
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	~ANC	Right adjust
3	9-16	I8	Junction number of anchor	1-44
4	17-24	F8.0	X coordinate of anchor	ft
5	25-32	F8.0	Y coordinate of anchor	ft
6	33-40	F8.0	Z coordinate of anchor	ft
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

**NOTE:** The ANC cards are used to transmit the data in Table 1.  
There must be one ANC card for each anchor in the array.

**IR CARD**

<b>Field</b>	<b>Columns</b>	<b>Format</b>	<b>Contents</b>	<b>Comments</b>
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	~~IR	Right adjust
3	9-16	I8	Junction number assigned to a cut in the reduced array	1-44
4	17-24	I8	Junction number at which cut is made in the original array	1-44
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

**NOTE:** The IR cards are used to transmit the information contained in the table below the left-hand schematic of each of Figures 3a-3d. There must be one IR card for each cut made in going from the original to the reduced array.

CAB CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	~CAB	Right adjust
3	9-16	I8	Cable number	1-22
4	17-24	I8	s=0 junction number	1-44
5	25-32	I8	s=L junction number (after required cuts are made)	1-44
6	33-40	F8.0	Cable weight per length in surrounding fluid; + if positively buoyant, - if nega- tively buoyant	lb/ft
7	41-48	F8.0	Normal drag coefficient of cable	
8	49-56	F8.0	Cable diameter	in.
9	57-64	F8.0	Total cable length (unstressed)	ft
10	65-72	F8.0	Cable rigidity, C (see notes) if k=1, C=EA	lb
11	73-77	F5.0	Exponent in constitu- tive relation, k (see notes)	$\geq 0$
12	78-80	I3	Number of straight ele- ments by which cable is to be represented	$>0, \leq 50$

NOTE: The CAB cards are used to transmit the information contained in the table below the right-hand schematic in Figures 3a-3d (fields 3 to 5), the physical characteristics of the cables in the array (fields 6 to 11), and the fineness by which the cables in the array are to be modeled (field 12). There must be one CAB card and one continuation CAB card for each cable in the array. The constitutive relation for a cable can, in general, be written (6) as  $\epsilon = (T/C)^k$  where  $\epsilon$  is the

NOTES FOR CAB CARD (continued)

strain and T the tension. C and k are constants which depend on the cable material and construction. Fields 10 and 11 transmit the values of C and k, respectively. An inextensible cable is transmitted to DECELL by leaving fields 10 and 11 blank.

CONTINUATION CAB CARD

Field	Columns	Format	Contents	Comments
1	1-8	F8.0	Tangential drag coefficient of cable	See notes
2	9-80	9F8.0	Not used	

NOTE: Each CAB card must be followed by an additional card. If no tangential drag is desired a blank card must be inserted. This card does not adhere to the convention requiring a card number and card type since it is in fact a continuation of the tangential drag coefficient. Default value is zero.

## DCAB CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	DCAB	
3	9-16	I8	Number of cable to which device is attached	1-22
4	17-24	I8	Device type (1,2)	See notes
5	25-32	I8	Print flag for cable devices. If flag = 0, print device characteristics and location. If flag ≠ 0, don't print.	
6	33-40	F8.0	Device weight in surrounding fluid; + if positively buoyant, - if negatively buoyant	lb (See note 3)
7	41-48	F8.0	Normal drag coefficient	
8	49-56	F8.0	Diameter on which drag coefficient is based (Type 1) Frontal area on which drag coefficient is based (Type 2).	in.  ft <sup>2</sup>
9	57-64	F8.0	Device length (Type 1)	ft
10	65-72	F8.0	Unstressed distance of device from s=0 junction of the cable	ft
11	73-77	F5.0	Tangential drag coefficient	
12	78-80		Not used	

NOTE: 1. The DCAB cards are used to transmit the physical characteristics of the discrete devices (buoyancy elements, current meters, etc.) attached to the cables in the array. There must be one DCAB card for each such device

NOTES FOR DCAB CARD (continued)

in the array. Two types of devices are permitted: (a) in-line (Type 1) any elongated device (cylinder, ellipse, etc.) attached so that its longitudinal axis is aligned with the cable axis; and (b) free devices (Type 2).

2. Dummy DCAB devices with no weight and zero drag can be used as conveniences to print the location of the device in the cable array's deformed state. With no DCAB devices, no information about the cable shape between junctions is printed.
3. Include cable weight in water if device covers segment of cable.

Each device is automatically assigned a unique number based on its location on the structure. Low numbered devices are located on low numbered cables. On each cable the lowest number device is nearest the s=0 end of the cable.

DJNC CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	DJNC	
3	9-16	I8	Number of junction to which device is attached	1-44
4	17-24	I8	Not used	
5	25-32	I8	Not used	
6	33-40	F8.0	Device weight in surrounding fluid; + if positively buoyant, - if negatively buoyant	lb
7	41-48	F8.0	Device drag coefficient	
8	49-56	F8.0	Frontal area on which drag coefficient is based	ft <sup>2</sup>
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The DJNC cards are used to transmit the physical characteristics of the discrete devices attached to the junctions in the array. There must be one DJNC card for each such device in the array.

Since an in-line device cannot physically exist at a junction (cable termination), only free devices are permitted at a junction.

DJNC devices are indexed automatically for counting purposes only; they are counted in the total number of indexed devices.

DEN CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	.DEN	Right adjust
3	9-16	F8.0	Density of fluid in which array is suspended	lb s <sup>2</sup> ft <sup>-4</sup> (1.99 for seawater)
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The DEN card is used to transmit the density of the fluid in which the array is suspended.

**EOD CARD**

<b>Field</b>	<b>Columns</b>	<b>Format</b>	<b>Contents</b>	<b>Comments</b>
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	~EOD	Right adjust
3	9-16		Not used	
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

**NOTE:** The EOD card is used to specify the end of data transmission.

**\*\* PARAMETRIC STUDY SOURCE DECK CARDS \*\***

NDAT CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	NDAT	
3	9-16	I8	Current field option	See note 1
4	17-24	I8	Number of stations at which current data is taken for current field option 3. Otherwise not used.	See note 2
5	25-32	I8	Option for defining a particular parametric study as the new no current reference configuration. Option = 0, no new ref. config. Option ≠ 0, new ref. config.	
6	33-40	F8.0	PHI	degrees See note 3
7	41-48	F8.0	Device location punch output option; option ≠ 0, punch device locations on cards	See note 4
8	49-56	F8.0	Weight of device whose location is to be punched	lb
9	57-64		Not used	
10	65-72	F8.0	Velocity units input option	See note 5
11	73-77	F5.0	Number of steps used to apply full current	See notes 6 and 7 (default value = 1.0)
12	78-80		Not used	

SEE NEXT PAGE FOR NOTES

NOTE:

1. The NDAT card is used to specify that new, modified, or additional data follow and to transmit the current field option. Three current field options are available.
  - 0 - No current.
  - 1 - Current field is unidirectional and horizontal. (There is no vertical component.) The current magnitude can vary with depth. At any point in the plane Z-constant, the velocity is invariant. The no-current configuration is also calculated as part of this option.
  - 2 - Same as current field option 1 except that the current can have a directionality that depends on depth. That is, this option relaxes the unidirectional constraint on the velocity field. At any point in the plane Z-constant, the velocity is invariant. An example of a possible current candidate requiring this option would be a helical current where the axis of the helix is aligned with gravity. The no-current configuration is also calculated as part of this option.
  - 3 - Interpolation/extrapolation scheme for field current (magnitude and direction) data. The current is assumed to have no vertical component. Two, three, or four stations can be selected in the horizontal plane and at each of these stations, current (direction and magnitude) data can be obtained at up to 25 elevations. This option affords current variation in horizontal planes. The no-current configuration is also calculated as part of this option.
2. For current option 3, the value in field 4 on the NDAT card must appear on all successive NDAT cards even if the velocity field is not to be varied in any of the parametric studies.
3. The angle  $\phi$  specifies the rotation of the X-axis from the N-axis.  $\phi$  is measured positive in the clockwise sense and the N-axis is  $\phi=0$ . That is, when  $\phi=0$  then the (N,W) coordinate system is coincident with the (X,Y) coordinate system (see Figure 4). The  $\phi$  value should appear on each NDAT card.
4. It is sometimes desirable to have the locations of particular devices punched on cards for input to other programs. For example, both hydrophones and buoys may be distributed as DCAB devices along the structure, but only the location of the hydrophones is important. By specifying field 7  $\neq$  0 and field 8 = hydrophone weight, DECELL will punch for each hydrophone: (a) device index, (b) cable number, (c) distance from the  $s = 0$  end of the cable, and (d) x,y,z coordinates of the device. Preceding this punched output is a card totalling the number of cards in the punched output.

NOTES FOR NDAT CARD (continued)

5. Velocity units input option:

- 0 - input magnitude of velocity in knots (default)
- 1 - input magnitude of velocity in cm/sec
- 2 - input magnitude of velocity in ft/sec

- 6. This is a coded value: the integer portion represents the number of steps used to apply the full current; the fractional part controls printed output: a non-zero fractional part (i.e., 10.1) causes the shape calculated for each increment of the current to be printed. For example: the value 10.1 will cause the current to be applied in ten equal increments and the structure shape will be printed for each increment. A 10.0 value will apply the current in ten increments but print only the shape with the full current value applied. If plotting is requested, only the shape with the full current applied is plotted.
- 7. This input option is intended to aid in obtaining solutions where high currents cause SLOW/NO CONVERGENCE messages to be printed.

**PARAMETRIC DESCRIPTIVE TITLE CARD**

<b>Field</b>	<b>Columns</b>	<b>Format</b>	<b>Contents</b>	<b>Comments</b>
1-10	1-80	8A10	Parametric descriptive title	See notes

**NOTE:** Descriptive Title Card must always follow an NDAT card. If no title is desired, then a blank card must be inserted. This card does not adhere to the convention requiring a card number and card type, so that the entire card can be utilized for a title.

## COMP CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	COMP	
3	9-16	F8.0	Accuracy required in array equilibrium calculations (COMP value)	ft (0.01 typ)
4	17-24	F8.0	Nodal position iteration limit	See note 2 (200 default value)
5	25-32	F8.0	Imaginary reaction iteration limit	See note 2 (1000 default value)
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

## NOTES:

1. The COMP card is used to transmit the accuracy requirement imposed on the array equilibrium calculations. This accuracy requirement, specified in field 3, insures that the calculated coordinates of every point in the array are within  $\pm$  field 3 of their exact values.

The accuracy obtainable is limited by the significant figure capacity of the computer being used and by the largest linear dimension in the array. Let the number of significant figures carried in single precision be  $n$ , and let the characteristic of the common logarithm of the largest linear dimension be  $m$ . Then, the value of field 3 is usually bounded by field 3  $> 10^{m-n+3}$ . (For example, suppose  $n = 8$  and the largest dimension is 25,000 ft. Then, field 3  $> 0.1$  ft.) Occasionally, a larger minimum value must be used. A

**NOTES FOR COMP CARD (continued)**

COMP card must appear after the first NDAT card. See PARAMETRIC STUDY SOURCE DECKS. Accuracy requirements can be changed in subsequent Parametric Study Decks by using new COMP cards.

2. See the descriptions in the text on pages 18 and 19.

VEL CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	~VEL	Right adjust
3	9-16	F8.0	Z coordinate at which current velocity is specified	ft
4	17-24	F8.0	Magnitude of current at Z coordinate specified in field 3	knots; cm/sec; ft/sec (consistent with NDAT card)
5	25-32	F8.0	Direction of current at Z coordinate (current option 2 only)	degrees
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	56-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The VEL cards are used to transmit the data in Table 2. There must be one VEL card for each value of Z at which the current velocity is specified.

Up to 25 VEL cards are permitted. At least one of the Z coordinates transmitted by the VEL cards must be less than or equal to the minimum Z coordinate transmitted by the ANC cards. For further information see CURRENT FIELD INPUT OPTION 1.

The VEL cards must not appear after an NDAT card specifying a current field option = 0. All VEL cards required to transmit the current profile must appear after the first NDAT card specifying a current field option = 1. See PARAMETRIC STUDY SOURCE DECKS.

A given current profile will be applied in all subsequent parametric cases until a new field is defined.

NOTES FROM VEL CARD (continued)

Current Option 1 - Only the magnitude of the current is input (field 4). The direction is varied by the ANG card.

Current Option 2 - Both magnitude and direction of current are input fields 4 and 5, respectively. The direction of the field also may be modified by the ANG card. Current direction is to be specified from the magnetic north axis. Clockwise rotation is positive.

Current Option 3 - Fields 3, 4 and 5 are ignored. The velocity information is read from the velocity continuation group immediately following the VEL card.

The following is a brief description of the velocity cards under current option 3.

After a VEL card is encountered there will be 2, 3 or 4 sets of velocity data depending on the number of stations at which velocity profiles were measured.

Each set of data for a station will contain one Station Location Card and N Velocity Definition Cards. N is the number of Z-coordinates at which velocity is measured for the particular station. The maximum value of N is 25.

The 2, 3 or 4 sets of data are stacked as indicated in Figure 7.

The Station Location Cards and Velocity Definition Cards are defined on the next two pages.

To further clarify the velocity option 3 data requirements we present another example using 3 stations of current data. The data deck will be arranged as follows:

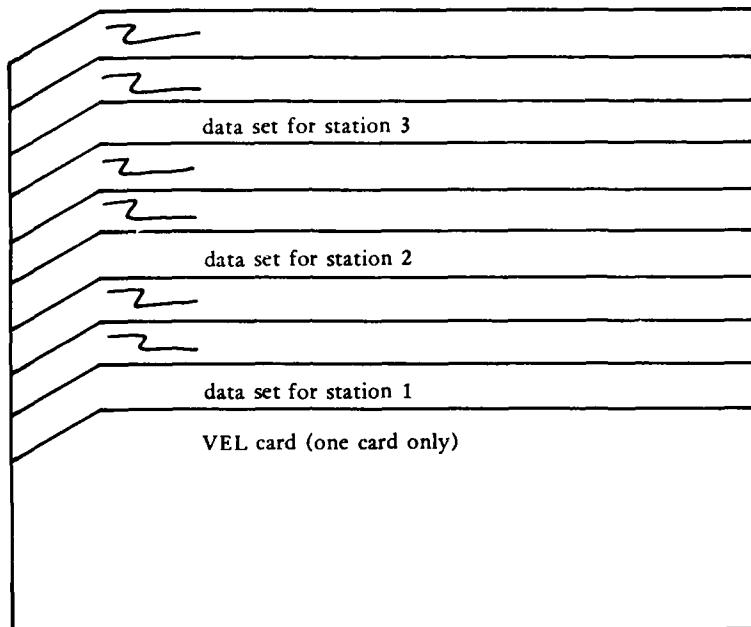


Figure 7. Arrangement of data sets for velocity option 3.

NOTES FROM VEL CARD (OPTION 3 ONLY) (continued)

Field	Columns	Format	Contents	Comments
1	1-5	I5	Station number at which velocity profile measured	
2	6-10	I5	Number of Z-coordinates at which velocity is measured for this station (field 1)	
3	11-20	F10.0	North coordinate of this station*	ft (see notes)
4	21-30	F10.0	West coordinate of this station**	ft (see notes)
5	31-80		Not used	

\*Coordinate is positive for north, negative for south.

\*\*Coordinate is positive for west, negative for east.

NOTES FROM VEL CARD (OPTION 3 ONLY) (continued)

Field	Columns	Format	Contents	Comments
1	1-5	I5	Station number	
2	6-10		Not used	
3	11-20	F10.0	Z-coordinate of velocity	ft
4	21-30	F10.0	Magnitude of velocity at Z-coordinate of this station (field 1)*	See notes
5	31-40	F10.0	Direction of current at Z-coordinate of this station (field 1)**	degrees (see notes)
6	41-80		Not used	

NOTE: There must be as many of this card as there are current readings at the station (= field 2 of preceding card).

---

\*The magnitude of velocity may be input in three different units according to the option definition on the NDAT card.

Units Option 0 - knots (default)

Units Option 1 - cm/sec

Units Option 2 - ft/sec (see NDAT card)

\*\*The direction of current is positive in the clockwise sense from the magnetic north axis (degrees).

**ANG CARD**

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	.ANG	Right adjust
3	9-16	F8.0	Initial current angle	degrees
4	17-24	F8.0	Increment in current angle	deg, > 0
5	25-32	F8.0	Final current angle	deg, ≥ field 3
6	33-40		Not used	
7	41-43		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

**NOTE:** The ANG card is used to transmit instructions for changing the angular direction of the current with respect to the N-axis for current options 1 and 2 only. DECELL calculates the array response to the specified current profile from the initial to the final current angles in increments transmitted by field 4. An ANG card must not appear after an NDAT card specifying a current field option = 0. One ANG card must appear after the first NDAT card specifying a current field option = 1, 2, or 3. See PARAMETRIC STUDY SOURCE DECKS.

If no parametric range of current direction variation is required, then Fields 3 and 5 should have identical values and field 4 should have a non-zero positive value.

When exercising the angular rotation option, it is important to recognize the difference between current options 1 and 2. For current option 1, the input value in field 3 of the ANG card establishes the directionality of the entire flow field. This is not the case for current option 2 since current directionality is established and specified as input on the VEL card.

NOTES FROM ANG CARD (continued)

For current option 2 the field 3 input value on the ANG card should be set equal to  $\phi$  (the angle between the N- and X-axes) plus the initial angle of interest. The value in field 5 of the ANG card should be set equal to  $\phi + \beta$  where  $\beta$  is the total angle through which the current is to be rotated. The value of field 4 is  $\Delta\beta$ , the increment. When current option 2 is selected and no rotation of the current field is desired, the fields 3 and 5 should be set equal to  $\phi$  and any positive value set in field 4.

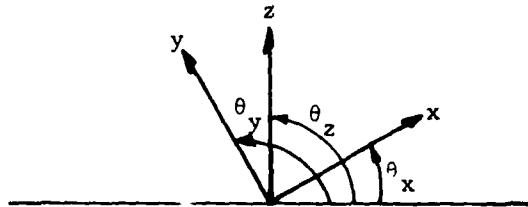
PPLT CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	PPLT	
3	9-16	F8.0	Plotting option: 0 - Undefomed only 1 - Deformed only 2 - Both	Undefomed plotted as a dotted line. Deformed plotted as a solid line.
4	17-24	F8.0	Height of plot, y	in. (default 10)
5	25-32	F8.0	View angle, x (see note)	degrees (default 30)
6	33-40	F8.0	View angle, y (see note)	degrees (default 120)
7	41-48	F8.0	View angle, z (see note)	degrees (default 90)

NOTE: For a plan or elevation view (not a perspective view) one view angle must be  $361^\circ$ . This is a code indicating which axis is perpendicular to the plot. For example, a plan view is specified by:

View Angle, x = 0.001 (0 gives the  $30^\circ$  default value)  
 View Angle, y =  $90^\circ$   
 View Angle, z =  $361^\circ$

The x, y and z view angles are shown below for the default configuration.



- $\theta_x$  - View angle for x axis. 30 degrees.
- $\theta_y$  - View angle for y axis. 120 degrees.
- $\theta_z$  - View angle for z axis. 90 degrees.

Examples perspective plots are shown in Figures 8-10.

## CPLT CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	CPLT	
3	9-16	F8.0	ZUP-Max. depth plane level	ft
4	17-24	F8.0	ZDN-Min. depth plane level	ft
5	25-32	F8.0	DZ -Delta depth	ft
6	33-40	F8.0	YIN-Height in Y direction of a single plane	in.
7	41-48	F8.0	XMIN	ft (If blank default values selected)
8	49-56	F8.0	XMAX	
9	57-64	F8.0	YMIN	
10	65-72	F8.0	YMAX	
11	73-77	F5.0	ANG-View angle Y	degrees default = 90
12	78-80	I3	NY -Number of mesh points in Y direction, including boundary	default = 6

NOTE: Current plots may be depicted at one or more depths by varying input parameters ZUP, ZDN, DZ. The vertical height for each plane of the plot is input as YIN, and the corresponding width is calculated by the program. The product of the number of planes and the vertical height of a single plane cannot exceed 10 inches.

The plots may vary in perspective view angle y over the range  $0 < \text{ANG} < 180^\circ$ , where  $\text{ANG} = 90^\circ$  is the plan view. For purposes of plotting the current field, each plane is assumed to have z coordinate zero and view angle x equal to zero.

NOTES FROM CPLT CARD (continued)

The mesh for plotting current is controlled by input NY. NY is the number of mesh points in the y direction, for a plane, including the boundary. The corresponding number of mesh points, for the x direction, is calculated by the program. (NY = 2 + number of current arrows encountered when moving from YMIN to YMAX.)

The area covered by the current field plot may be selected in two ways. If the values XMIN, XMAX, YMIN, YMAX are left blank, the program determines the area to be plotted. The area is based on the maximum and minimum anchor point coordinates. The second method is to define XMIN, XMAX, YMIN, YMAX in terms of the x, y coordinate system. If there is only one anchor point XMIN, XMAX, YMIN, YMAX must be defined by the user. A star will be plotted at each anchor point within the defined area.

Examples of current field plots are shown in Figures 11 and 12.

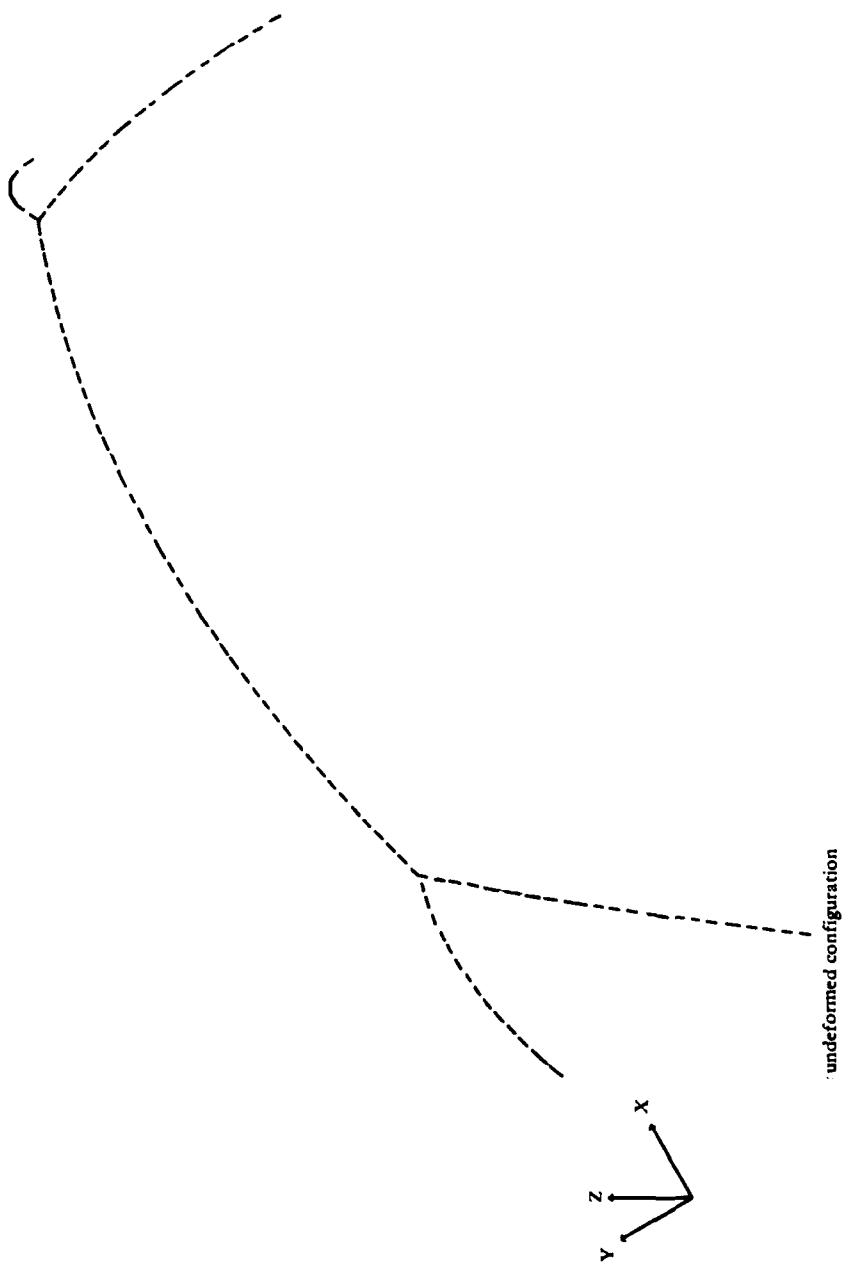


Figure 8. Perspective view of the undeformed structure (field  $\beta = 0$ ).

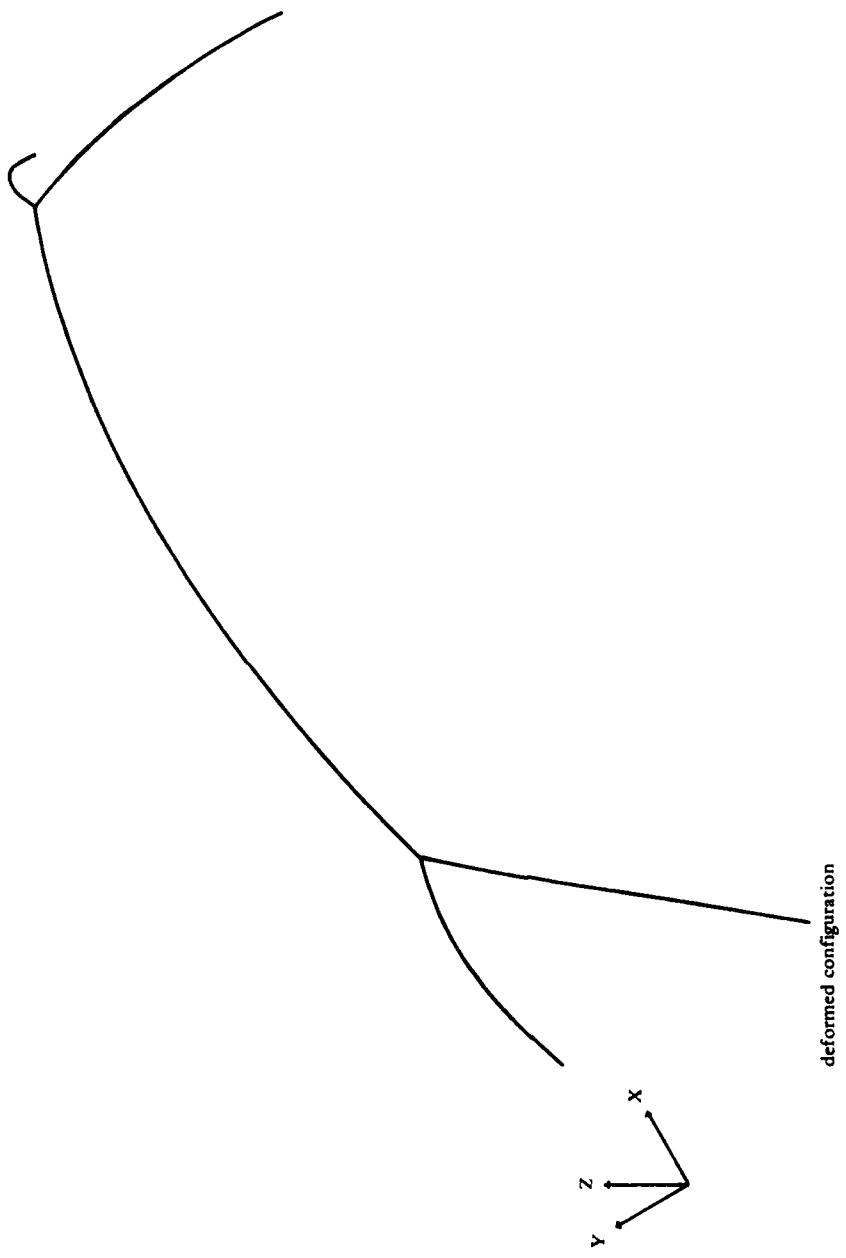


Figure 9. Perspective view of the deformed structure (field 3 = 1).

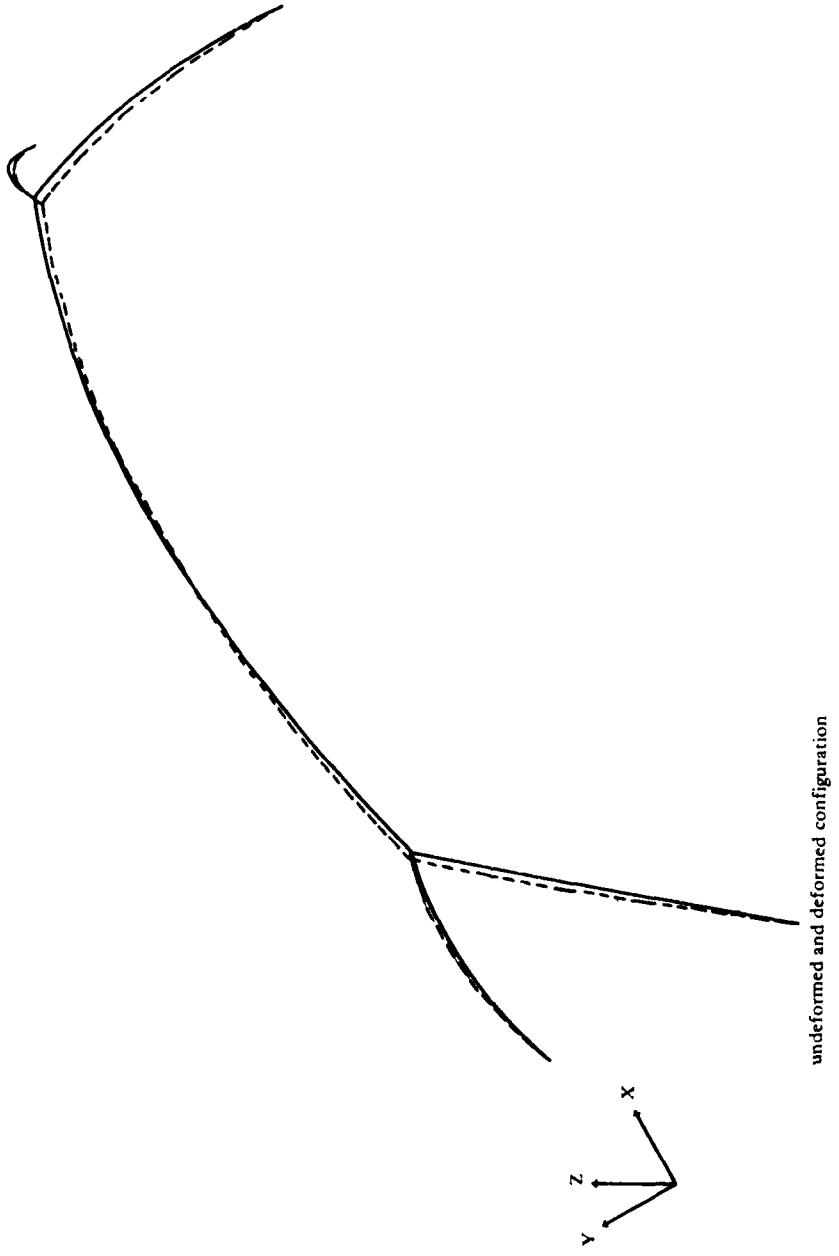


Figure 10. Perspective view of the deformed structure with the undeformed shape for comparison (field  $3 = 2$ ).

apply current profile at 45 dec increments

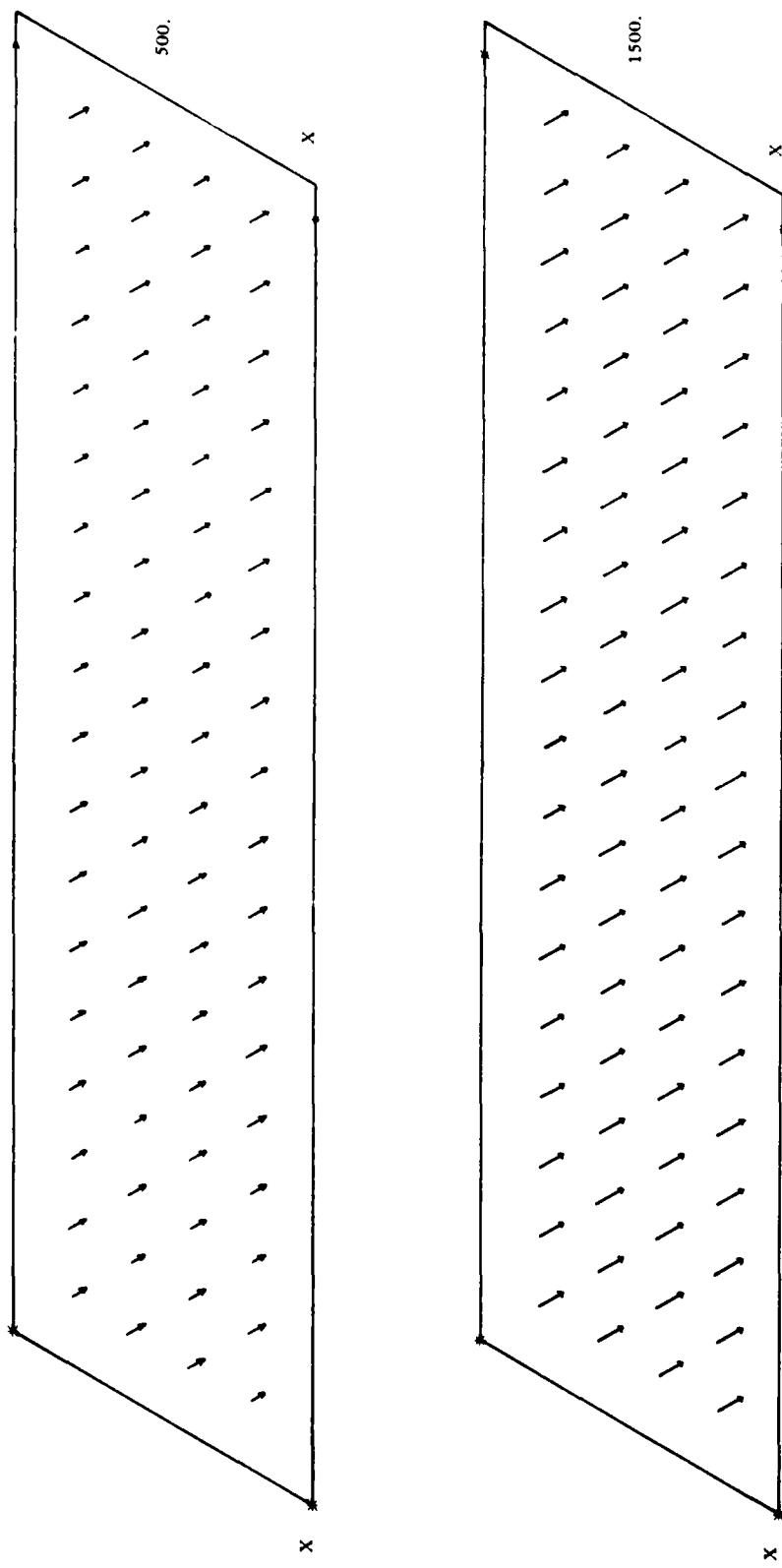


Figure 11. Unidirectional current field.

test for current option 3

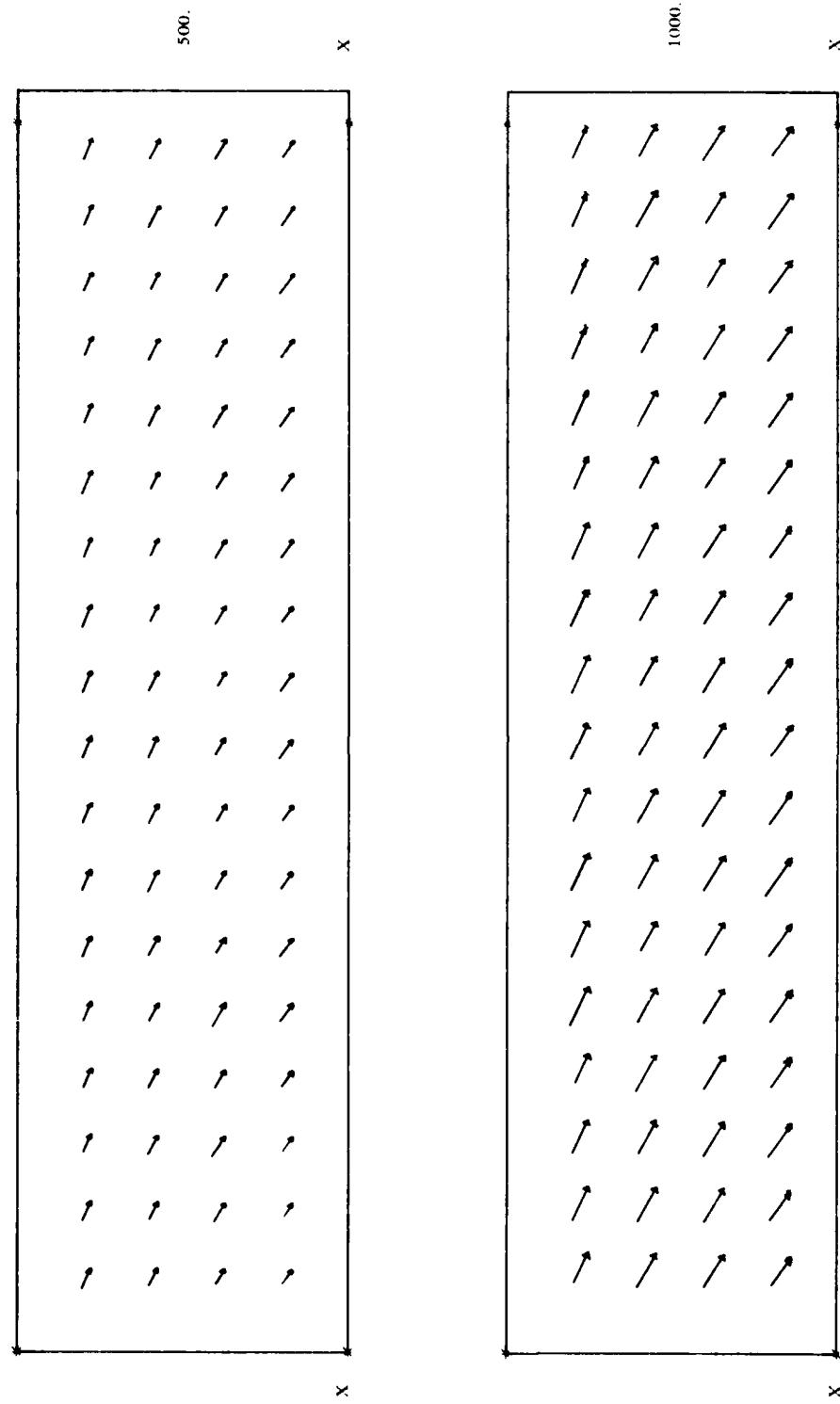


Figure 12. Non-unidirectional current field. (Note by sighting along the arrows that the field does curve.)

EOD CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	~EOD	Right adjust
3	9-16		Not used	
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The EOD card is used to specify the end of data transmission or end of a parametric case.

EOP CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	.EOP	Right adjust
3	9-16		Not used	
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The EOP card is used to specify the end of the problem and is required for a normal termination.

### Cable Array Source Deck

The cable array source deck contains all of the cards required to describe the physical characteristics of the cable array under consideration. The last card in the cable array source deck must be an EOD card to signify the end of data transmission. The form of the cable array source deck is given below.

#### Cable Array Source Deck

<u>Card Type*</u>	<u>Comments</u>
NJNC	One card
ANC	One for each array anchor
IR	One for each cut going from original to reduced array
CAB	One (plus one continuation card) for each array cable
DCAB	One for each discrete device attached to a cable
DJNC	One for each discrete device attached at a junction
DEN	One card
EOD	Must be last card in source deck

### Cable Array Source Tape

The cable array source tape is an alternate means of transmitting to DECEL1 the physical characteristics of the cable array under consideration. A recommended program for generating the cable array source tape from the cable array source deck is given below.

#### Cable Array Source Tape Generation

```
PROGRAM STAPE
DIMENSION DATA(10)
DATA(IREAD = Unit number of card reader)
DATA(ITAPE = Unit number of source tape)
1 READ(IREAD,10)(DATA(I),I=1,10),EX,NSEG
  WRITE(ITAPE,11)(DATA(I),I=1,10),EX,NSEG
  IF(DATA(2).NE.4HDCAB)G0 T0 3
  READ(IREAD,20)TANDRG
  WRITE(ITAPE,21)TANDRG
```

(continued)

\*These cards may be arbitrarily ordered except for the EOD card. It is strongly recommended that the cards in the cable array source deck be given unique card numbers (Field 1 of each card). Note that LUN, NDAT, COMP, VEL, ANG, and EOP cards are not permitted in the cable array source deck.

### Cable Array Source Tape Generation (Continued)

```
3 CONTINUE
IF(DATA(2).EQ.4H EOD)G0 T0 2
G0 T0 1
10 F0RMAT(F4.0,A4,8F8.0,F5.0,I3)
11 F0RMAT(F4.0,A4,8E15.8,/ ,E12.5,I3)
20 F0RMAT(F8.0)
21 F0RMAT(E15.8)
2 REWIND TAPE
END
```

### Parametric Study Source Decks

The parametric study source decks are used to transmit to DECEL1 accuracy requirements, current fields, and changes in the physical properties of the cable array under consideration. Each parametric study source deck must begin with an NDAT card and a Parametric Descriptive Title card and end with an EOD card. The form of the parametric study source decks is given below.

### Parametric Study Source Decks

<u>Card Type*</u>	<u>Comments</u>
NDAT	Must be first card in parametric study source deck. Field 3 (current option) can change as 0 1, 0 2, or 0 3. The changes 1 2, 1 3, and 2 3, even with intermediate zeros, are not permitted.
Parametric Title Card	NDAT card <u>must</u> be followed immediately by parametric title card.
COMP	Must appear after first NDAT card. The accuracy requirement transmitted is retained until the appearance of a COMP card in another parametric study source deck.
VEL	Must not appear after NDAT card containing current option 0. All VEL cards required to transmit a current profile must appear after the first NDAT card containing a current option 1 or 2 or 3. The current profile transmitted is retained until the appearance of a VEL card in another parametric study source deck. The appearance of the first VEL card in a parametric study source deck zeros the entire current profile. Thus, to change from one current profile to another, all VEL cards required to specify the new profile must appear in the appropriate parametric study source deck.
ANG	Must not appear after NDAT card containing current option 0. One ANG card must appear after the first NDAT card containing current option 1, 2 or 3. The current angles transmitted are retained until the appearance of an ANG card in another parametric study source deck.
ANC	Used to change anchor data. See Note.
CAB	Used to change cable data. See Note.
DCAB	Used to change discrete device on cable data. See Note.
DJNC	Used to change discrete device at junction data. See Note.
EOD	Must be last card in parametric study source deck.

\*These cards may be arbitrarily ordered except for the NDAT, Parametric Title, and EOD cards. Note that LUN, JNC, IR, DEN, and EOP cards are not permitted in the parametric study source decks.

**NOTE:** The array design changes which are permitted are those changing the physical data of the array but not the overall geometric layout of, or the number of discrete devices on, the array. These changes are keyed by matching the card number and type appearing in a parametric study source deck to the card number and type appearing in changes in the array physical data is given below.

**Summary of Changes in the Array Physical Data Permitted (P)  
and Not Permitted (NP)**

Card Type	Field Number											
	1	2	3	4	5	6	7	8	9	10	11	12
ANC	NP	NP	NP	P	P	P						Not used
CAB	NP	NP	NP	NP	NP	P	P	P	P	P	P	P
CONTINUATION CAB	P											
DCAB	NP	NP	NP	1#2	NP	P	P	P	P	P	P	P
DJNC	NP	NP	NP	NP	NP	P	P	P	P			Not used

**OVERALL INPUT DECK**

The overall input deck consists of a LUN card (optional) specifying the I/O options and the logical unit numbers of the required I/O devices, followed by the cable array source deck (or tape), followed by any number of parametric study source decks, and ended by an EOP card signifying the end of the problem. The form of the overall input deck is given below.

**Overall Input Deck**

- LUN Card (optional)
- Cable Array Source Deck (or Tape)
- Parametric Study Source Decks
- EOP Card

EXAMPLE

1. Compilation of cable array source deck errors only.

```
1000~LUN~~~~~60~~~~~61~~~~~24 (or omit this card)
*****Main Title Card*****
      Cable Array Source Deck (or Tape)
1001~EOP
```

2. Deflections of the source deck cable array due to a current profile.

```
(LUN card omitted)
*****Main Title Card*****
      Cable Array Source Deck (or Tape)
1001NDAT~~~~~1
*****Parametric Study 1 Title Card*****
1002COMP
1003~VEL
1010~VEL
1011~ANG
1012~EOD
1013~EOP
```

3. Deflections of the source deck cable array due to a current profile and effects of buoyancy changes on these deflections.

```
(LUN card omitted)
*****MAIN TITLE CARD*****
Cable Array Source Deck (or Tape) containing a card:
~~~9DJNC~~~~~3~~~~~10000.~~~~1.95~~~~35.3
1001NDAT~~~~~1
*****Parametric (see note) Study 1 Title Card*****
1002COMP
1003~VEL
1010~VEL
1011~ANG
1012~EOD
1013NDAT~~~~~1
*****Parametric Study 2 Title Card*****
~~~9DJNC~~~~~3~~~~~12500.~~~~1.95~~~~35.3
1014~EOD
1015~EOP
```

NOTE: In each case unique card numbers were assigned, otherwise an error would have resulted. However, any or all card numbers could have been omitted and no error would result.

## ERROR MESSAGES

DECELL contains a series of internal error checks to insure that the original cable array is properly reduced to a statically determinate array; the input data are consistent; and the deck is properly structured.

If errors are found, the entire list of input cards is printed; and cards with errors are identified by an error code number. The text of the coded error message is printed after the card listing. All cards are scanned for errors; however, only the first error on a card is detected. A card with a DECELL detected error should be scanned visually to check for other errors.

## DEFINITION OF ERRORS

### Type 0 -

A type 0 error indicates that the card type identifier (Field 2) is not recognizable.

### Type 1A - LUN

Field 6 not equal 0 or 1

### Type 1B - LUN

Field 8 not equal 0,1,2

### Type 1C - LUN

Non-unique numbers assigned to required I/O units.

### Type 1A - NJNC

Field 3 greater than 44 or less than 2.

### Type 1A - ANC

Field 3 greater than 44 or less than 1.

### Type 1A - IR

Field 3 = Field 4.

### Type 1B - IR

Fields 3 or 4 greater than 44 or less than 1.

### Type 1A - CAB

Field 3 greater than 22 or less than 1.

### Type 1B - CAB

Field 4 = Field 5.

### Type 1C - CAB

Fields 4 or 5 greater than 44 or less than 1.

### Type 1D - CAB

Fields 7, 8 or 9 less than or equal to 0.

### Type 1E - CAB

Fields 10 or 11 less than 0

### Type 1F - CAB

Field 10=0 and Field 11 not equal 0

### Type 1G - CAB

Field 10 not equal 0 and Field 11=0.

Type 1H - CAB  
Field 12 greater than 50 or less than 1.

Type 1A - DCAB  
Field 3 greater than 22 or less than 1.

Type 1B - DCAB  
Field 4 greater than 2 or less than 1.

Type 1C - DCAB  
Field 5 greater than 1000 or less than 1.

Type 1D - DCAB  
Field 4=1 and Field 9 less than or equal to 0.

Type 1E - DCAB  
Field 4=2 and Field 9 not equal 0.

Type 1F - DCAB  
Fields 7,8 or 10 less than 0.

Type 1A - DJNC  
Field 3 greater than 44 or less than 1.

Type 1B - DJNC  
Field 7 or 8 less than 0.

Type 1A - DEN  
Field 3 less than 0.

Type 1A - NDAT  
Field 3 not equal 0,1, or 2.

Type 1A - COMP  
Field 3 less than or equal 0.

Type 1A - ANG  
Field 4 less than or equal 0.

Type 1B - ANG  
Field 5 less than Field 3.

Type 2A - ANC  
The junction number assigned to the anchor (Field 3) has been assigned to a preceding ANC card or to an S=L junction (Field 5) on a preceding CAB card.

Type 2A - CAB  
The junction number assigned to the S=L junction (Field 5) has been assigned on a preceding CAB card or to an anchor junction (Field 3) on a preceding ANC card.

Type 3 - CAB  
A Type 3 error appears only in conjunction with a CAB card and indicates that the number assigned to the cable (Field 3) has been assigned on a preceding CAB card.

Type 4A - IR  
The junction number assigned in Field 3 has been assigned in Fields 3 or 4 of a preceding IR card.

**Type 4B - IR**

The junction number assigned in Field 4 has been assigned in Field 3 of a preceding IR card.

**Type 6A - NJNC**

An NJNC card has previously appeared in the particular source deck.

**Type 6A - DEN**

A DEN card has previously appeared in the particular source deck.

**Type 6A - COMP**

A COMP card has previously appeared in the particular source deck.

**Type 6A - VEL**

Twenty-five VEL cards have previously appeared in the particular source deck.

**Type 6B - VEL**

The Z-coordinate at which the current velocity is specified (Field 3) has been used on a preceding VEL card in the particular source deck.

**Type 7 -**

A Type 7 error indicates an inadequacy of information in cable array source deck (or tape). The other information column under the error heading contains a 1x3 matrix, the elements of which give respectively the number of NJNC cards read, the number of DEN cards read, and the number of ANC cards read. A zero element is an error (see cable array source deck).

**Type 8 -**

A Type 8 error indicates a discontinuity in numbering the cables in the array. The other information column under the error heading contains a 1x22 matrix, the elements of which contain one or zero indicating, respectively, the use or non-use of the corresponding column number as a cable number. Zeros interspersed with ones are in error (see array description).

**Type 9 -**

A Type 9 error indicates a discontinuity in numbering the junctions in the array. The other information column under the error heading contains a 1x44 matrix, the elements of which contain one or zero indicating respectively, the use or non-use of the corresponding column number as a junction number. Zeros interspersed with ones are in error (see array description and reduction to a statically determinate array).

**Type 11 -**

A Type 11 error indicates an improper reduction of the original cable array to a statically determinate array or an absence of certain input cards in the cable array source deck (or tape). The other information column

under the error heading contains a 1x5 matrix, the elements of which give, respectively, the number of CAB cards read, the number of ANC cards read, the number of junctions in the original cable array (Field 3 of the NJNC card), the number of required cuts (Eq. (1)) calculated from the preceding information, and the number of IR cards read. Column 5 not equal to column 4 is an error (see reduction to a statically determinate array).

Type 12A - IR

The junction number assigned in Field 3 is less than or equal to the number of junctions in the original (unreduced) array (Field 3 of the NJNC card).

Type 12B - IR

The junction number assigned in Field 3 is greater than the number of junctions in the original (unreduced) array plus the number of cuts made in reducing the array (Eq. (1)).

Type 12C - IR

The junction number assigned in Field 4 is greater than the number of junctions in the original (unreduced) array.

Type 12A - CAB

The junction number assigned in Field 4 is greater than the number of junctions in the original (unreduced) array (Field 3 of the NJNC card) plus the number of cuts made in reducing the array (Eq. (1)).

Type 12A - DCAB

The cable number assigned in Field 3 does not correspond to a cable number assigned to a cable (Field 3 of the CAB cards).

Type 12B - DCAB

The distance of the discrete device from the S=0 junction of the cable (Field 10) is greater than or equal to the length of the corresponding cable (Field 9 of the CAB card).

Type 12A - DJNC

The junction number assigned in Field 3 does not correspond to either a junction number assigned to an anchor (Field 3 or the ANC cards) or a junction number assigned to an S=L junction of a cable (Field 5 of the CAB cards).

Type 13 -

A Type 13 error indicates that the original cable array has not been properly reduced to a statically determinate array or that junctions have been improperly numbered. The other information column under the error heading contains the message, improper array reduction or junction numbering. Check tree representation of array (see array reduction section of Users Manual) against junction numbering on ANC and CAB cards.

Type 14A -

A Type 14 error indicates an inadequacy of information in a parametric study source deck. The other information column under the error heading contains a 1x5 matrix, the elements of which give, respectively, the number of COMP cards read, the current field option, the number of VEL cards read, the number of VEL cards containing a Z-coordinate (Field 3) less than or equal to the minimum Z-coordinate transmitted by the ANC cards (Field 6 of the ANC cards), and the number of ANG cards read. If column 1 contains a zero, then a COMP card has not appeared after the first NDAT card (see parametric study source decks).

Type 14B -

A Type 14 error indicates an inadequacy of information in a parametric study source deck. The other information column under the error heading contains a 1x5 matrix, the elements of which give, respectively, the number of COMP cards less than or equal to the minimum Z-coordinate transmitted by the ANC cards (Field 6 of the ANC cards), and the number of ANG cards read. If column 2 contains a one and any of columns 3, 4 or 5 contain a zero, then the standard current field has not been properly formulated (see parametric study source decks and standard current field).

Type 15 -

A Type 15 error indicates than an unpermitted change has been attempted in a parametric study source deck. (See parametric study source decks.)

Type 16 -

A Type 16 error indicates an improper deck structure. See cable array source deck, parametric study source decks, and overall input deck.

Type 17 -

A Type 17 error indicates that the cable array source deck (or tape) contains more than 2150 records. The other information column under the error heading contains the message common/B1/bounds exceeded. See Users Manual. A Type 17 error is readily correctable if the machine being used has sufficient core storage. This correction is achieved by changing the row dimension of DATAT on cards DES025 and INF022 from 2150 to a number exceeding the number of records in the cable array source deck (or tape). Simultaneously the comparison value on card INP615 must be changed from 2150 to the new row dimension of DATAT.

Type 18 -

A Type 18 error indicates that the accuracy required for the array equilibrium calculations (Field 3 of the COMP card) has not been obtained during the calculations. This is for one of two possible reasons.

- A. Some cable segments have gone slack (that is, the segments have near zero tension. An examination of the tensions printed out in conjunction with a Type 18 error will reveal if this is the reason. If it is, see the section on statically unstable cable arrays in Reference 2 for possible remedial actions. If it is not then ...)
- B. The accuracy required for the equilibrium calculations is simply too stringent for the computer to handle (see COMP card). An examination of the final value of the accuracy obtained, printed out in conjunction with a Type 18 error, will reveal the best accuracy obtainable. Field 3 of the COMP card should be modified to reflect this information.

#### ARRAY DESCRIPTIVE OUTPUT

Following each error-free reading of a parametric study source deck, DECEL1 transmits to the line printer a description of the physical characteristics of the cable array under study. This printout includes anchor junctions and locations, information concerning the reduction of the original cable array to a statically determine array, properties of the cables in the array, properties of the discrete devices located at array junctions total number of Type 1 and 2 devices, current field option and current profile and calculational accuracy requirements.

The format of the array descriptive output is self-explanatory. A sample printout is given in Appendix A.

#### STRUCTURAL OUTPUT

If output option 0 or 2 is selected, DECEL1 transmits to the line printer a structural output. The structural printout follows and refers to the array characterized in the array descriptive output and contains information giving:

- a. A description of the current field (i.e., no current or current from xxx degrees)
- b. The cable forces and angles at each anchor
- c. The position coordinates of the original (unreduced) array junctions, the displacement of these coordinates from the no-current coordinates, and the cable forces and angles at each junction
- d. The maximum and minimum tensions and their locations for each array cable and the maximum displacement from the no-current condition and its location for each cable
- e. The position coordinates, the displacement of these coordinates from the no-current coordinates, and the tension at each Type 1 and 2 DCAB device in the array

This latter information is printed out in the same order that the Type 1 and 2 DCAB devices are numbered. Note that it is possible to obtain the latter information for any point on any cable in the array by defining a "dummy" Type 2 DCAB device to be located at the point. A dummy Type 2 DCAB device is simply one for which fields 6, 7, and 8 of the DCAB card are left blank so that the "device" has no effect on the array equilibrium calculations.

The format of the structural output is self-explanatory. A sample printout is given in Appendix A (Figure 17).

#### DEVICE LOCATION OUTPUT

If output option 1 or 2 is selected, DECELL transmits to tape or cards a device location output. The device location output contains information giving:

1. A description of the current field (i.e., no current or current from xxx degrees)
2. The position coordinates of each Type 1 and 2 discrete device in the array

Four types of records are associated with the device location output. Each of these records is written with the format:

(A4,I4,3F10.2)

### REC Record

Field	Format	Contents
1	A4	.REC
2	I4	Record number
3	F10.2	Not used
4	F10.2	Not used
5	F10.2	Not used

NOTE: The REC record is used to identify the cable array under study. The record number (Field 2) is referenced in the array descriptive output in the statement, "DEVICE LOCATION OUTPUT RECORD XX REFERS TO THIS ARRAY." The information following a REC record refers to the identified array.

### CUR Record

Field	Format	Contents
1	A4	.CUR
2	I4	0 if no current acting on array 1 if current is acting on array
3	F10.2	Blank if Field 2 = 0 Current angle if Field 2 = 1
4	F10.2	Not used
5	F10.2	Not used

NOTE: The CUR record is used to describe the current field (i.e., no current or current from xxx degrees). The information following a CUR record refers to the identified current field.

**DEV Record**

Field	Format	Contents
1	A4	~DEV
2	I4	Discrete device index (Field 5 of the DCAB and DJNC cards)
3	F10.2	X coordinate of device
4	F10.2	Y coordinate of device
5	F10.2	Z coordinate of device

NOTE: The DEV records are used to transmit the position coordinates of the Type 1 and 2 discrete devices in the array. There is one DEV record for each indexed (Types 1 and 2) device for each identified current field.

**EOP Record**

Field	Format	Contents
1	A4	~EOP
2	I4	Not used
3	F10.2	Not used
4	F10.2	Not used
5	F10.2	Not used

NOTE: The EOP record is used to signify the end of output transmission.

A typical overall device location output file is illustrated below.

```
^REC^^1
^CUR^^0
    DEV Records (one for each indexed device)
    ^CUR^^1 current angle
        DEV Records
    ^CUR^^1 current angle
        DEV Records
    ^REC^^2
    ^CUR^^0
        DEV Records
^EOP
```

#### REFERENCES

1. Naval Research Laboratory Report 6819, The static equilibrium configuration of cable arrays by use of the method of imaginary reactions, R. A. Skop, and G. J. O'Hara, Port Hueneme, Calif., Feb 1969.
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3. Naval Research Laboratory Report 6894, The static configuration of a tri-moored, subsurface, buoy-cable array acted on by current-induced forces, by R. A. Skop, and R. E. Kaplan, Port Hueneme, Calif., May 1969.
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7. Civil Engineer Laboratory, Technical Report R-848, Seafloor construction experiment, SEACON II - an instrument tri-moor for evaluating undersea cable structure technology by T. R. Kretschmer, G. A. Edgerton, and N. D. Albertsen, Port Hueneme, Calif., Dec 1976.

**Appendix A**  
**EXAMPLE PROBLEM**

An example problem has been included both to illustrate actual input and output and as a test case. The test case can be used to confirm proper operation of DECELL when implemented on a particular host computer. The test case structure is shown in Figure 13. The structure represents an acoustic array in the horizontal leg; this leg has been buoyed at the center to keep it approximately horizontal. A signal cable rises from one anchor to a subsurface buoy. The applied current is unidirectional with the profile shown in Figure 14. The current is acting broadside to the structure. The DECELL model of the structure is shown in Figure 15; other details of the modeling are shown in Tables 4 through 8.

Input card images are shown in Figure 16. Note that one dummy-DCAB-device card was intentionally placed "out of sequence" just after the NJNC card. This illustrates that the card sequence is essentially arbitrary, except as noted elsewhere in the manual.

The output from DECELL is shown in Figures 17 and 18. Note that the "number of indexed devices" count includes the three DJNC devices. The "Array Equilibrium with no Current" portion defines both the initial positions of devices and the properties of the DCAB devices. If the "do not print" flag had been set on any DCAB card, that device would not have been tabulated here; however, its effects would have been accounted for in the solution.

In the portion of the output where the current was applied (Figure 18), the displacement of all junctions and devices is listed relative to the present no-current position and relative to the original no-current case. In this case both displacements are identical since the new no-current reference flag had not been set on the NDAT card.

Figure 19 shows the configuration of the array both in the no-current condition (dotted lines) and with current applied (solid lines). For this plot the default perspective view angles were used. Other views (plan or elevation) of the same structure in the same current could be obtained by additional identical NDAT cases with the perspective plotting angles changed accordingly.

Table 4. Cables

Cable No.	Junction		Length (ft)	Weight/Foot (lb/ft)	Diameter (in.)	Drag Coefficient
	From	To				
1	1	2	3,000	0.25	1.0	1.4
2	2	8	3,000	0.25	1.0	1.4
3	2	4	5,000	0.20	0.75	1.4
4	4	9	3,000	0.25	1.0	1.4
5	4	10	3,000	0.25	1.0	1.4
6	9	7	4,000	0.3	1.25	1.4

Table 5. Anchor Locations

Anchor No.	Junction No.	x	y	z
1	1	0	1,000	0
2	3	0	-1,000	0
3	5	7,000	-1,000	0
4	6	7,000	1,000	0

Table 6. Imaginary Reaction Cuts

Junction No.	Cut No.
3	8
5	9
6	10

Note: In the model the cables terminate at cuts rather than at anchors.

Table 7. DJNC Devices

Device Junction No.	Device Buoyancy (lb)	Device Drag Coefficient	Device Frontal Area (ft <sup>2</sup> )
2	3,000	1.0	26.0
4	3,000	1.0	26.0
7	3,000	1.0	26.0

Table 8. DCAB Devices

Device Index	On Cable No.	S Coordinate (ft)	Device Buoyancy (lb)
9	3	2,500	1,000

Note: Other dummy devices are used to obtain a printout of the spatial location of the device; these devices have not been tabulated here. Dummy devices have a very small weight and no drag.

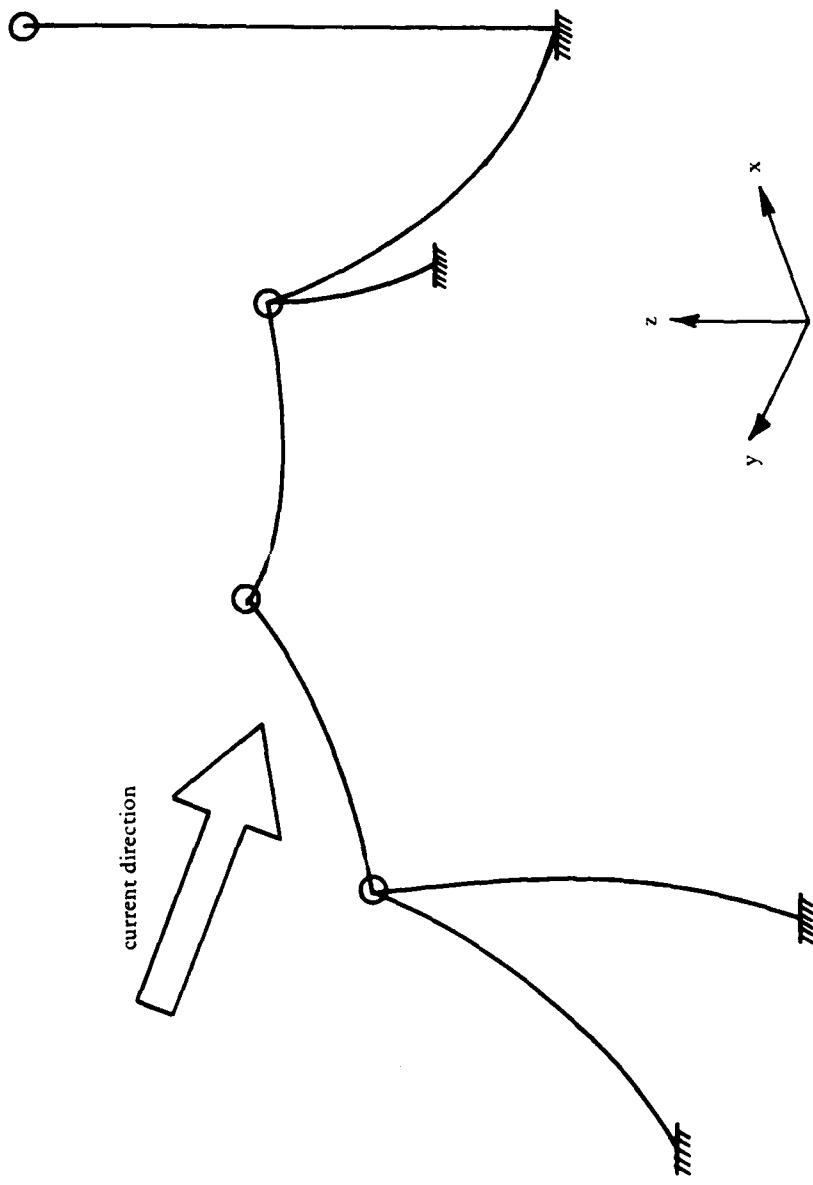


Figure 13. DECEL1 test case structure.

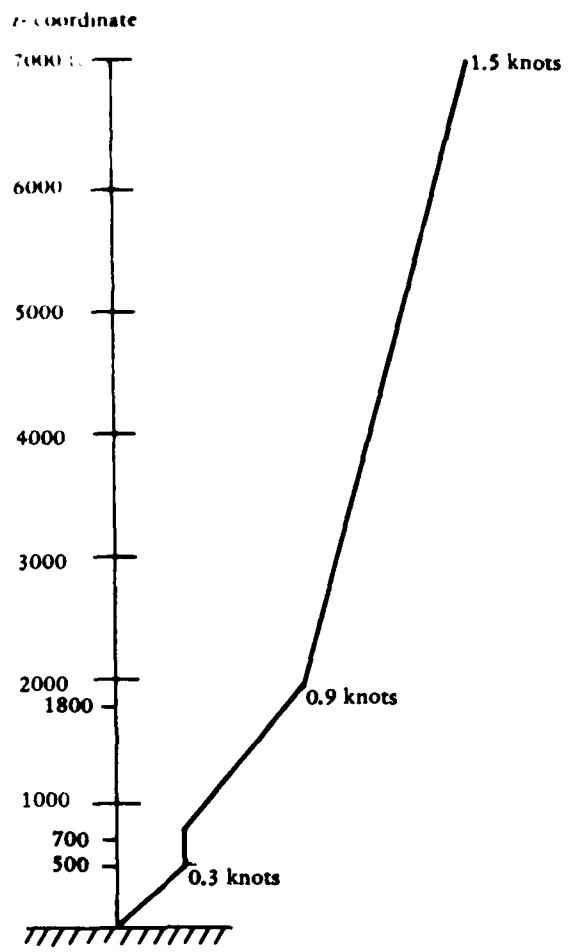


Figure 14. Current profile.

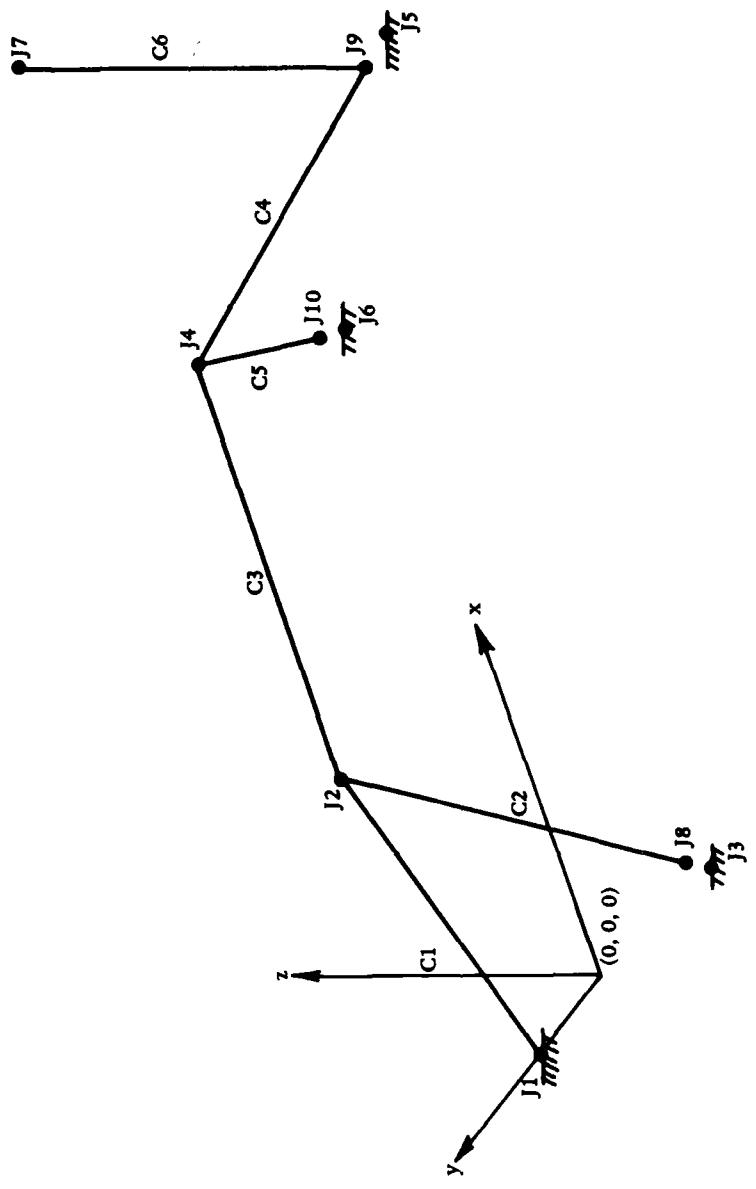


Figure 15. DECEL1 test case structure model.

## DECFLI TEST CASE

	7	2		0.01	0.01	750.		
DNJNC	1	2						
DCAB	1	0.0	1000.	0.0				
ARC	3	0.0	-1000.	0.0				
ARC	5	7000.0	-1000.	0.0				
ARC	6	7000.	1000.	0.0				
IK	8	3						
IK	9	5						
IR	10	6						
CAB	1	1	2	-0.25	1.4	1.0	3000.	50
0.03								
CAH	2	2	8	-0.25	1.4	1.0	3000.	50
0.03								
CAB	3	2	4	-0.20	1.4	0.75	5000.	50
0.03								
CAB	4	4	9	-0.25	1.4	1.0	3000.	50
0.03								
CAB	5	4	10	-0.25	1.4	1.0	3000.	50
0.03								
CAB	6	9	7	-0.30	1.4	1.25	4000.	50
0.03								
DCAB	1	2		0.001	0.01		1500.	
DCAB	1	2		0.001	0.01		2250.	
DCAB	2	2		0.001	0.01		750.	
DCAB	2	2		0.001	0.01		1500.	
DCAB	2	2		0.001	0.01		2250.	
DCAB	3	2		0.01	.1		1000.	
DCAB	3	2		0.01	.1		2000.	
DCAB	3	2		1000.	1.	5.	2500.	
DCAB	3	2		0.01	.1		3000.	
DCAB	3	2		0.01	.1		4000.	
DCAB	4	2		0.001	0.01		750.	
DCAB	4	2		0.001	0.01		1500.	
DCAB	4	2		0.001	0.01		2250.	
DCAB	5	2		0.001	0.01		750.	
DCAB	5	2		0.001	0.01		1500.	
DCAB	5	2		0.001	0.01		2250.	
DCAB	6	2		0.001	0.01		1000.	
DCAB	6	2		0.001	0.01		2000.	
DCAB	6	2		0.001	0.01		3000.	
DJNC	2			3000.	1.0	26.		
DJNC	4			3000.	1.0	26.		
DJNC	7			3000.	1.0	26.		
LEN	1.59							
EOU								
NUAT	1							
APPLY 90 DEGREE CURRENT (TOWARD -Y AXIS)								

COMP	0.1	
VEL	0.0	0.0
VFL	500.0	0.3
VEL	700.0	0.3
VEL	1800.0	0.9
VEL	7000.0	1.5
ANG	90.	1.
PPLT	2	
ECD		
ECP		

Figure 16. Input card images.

DECEL1 UPDATE INFORMATION

\*\*\*\*\*  
THIS IS THE JANUARY 1980 VERSION OF DECEL1 AS DESCRIBED IN THE USERS MANUAL  
NO UPDATES HAVE BEEN ADDED

NO ERRORS DETECTED

DECEL1 TEST CASE

APPLY 90 DEGREE CURRENT (CLOCKWISE X AXIS)

PHYSICAL CHARACTERISTICS OF THE STRUCTURAL CABLE ARRAY

PHI= 90.00

SINCE PHI=90 THE MAGNETIC AND ARRAY REFERENCED COORDINATE SYSTEMS ARE IDENTICAL.

ALL X,Y,Z RESULTS AND DISPLACEMENTS ARE GIVEN IN TERMS OF THE ARRAY FIXED COORDINATE SYSTEM.

NO. OF ANCHORS IS 4

JUNCTION NO.	X-COORDINATE	Y-COORDINATE	Z-COORDINATE
1	0.00	1000.00	0.00
3	0.00	-1000.00	0.00
5	7000.00	-1000.00	0.00
6	7000.00	1000.00	0.00

NO. OF JUNCTIONS IN ORIGINAL ARRAY IS 7

NO. OF CUTS MADE IN ORIGINAL ARRAY IS 3  
JUNCTION NO. 3 AT WHICH CUT MADE  
OF CUT 6  
9  
5  
6  
10

Figure 17. Output from DECEL1 for the example problem.

NO. OF CABLES IS 6

CABLE NO.	S=0 JUNC	S=L JUNC	LENGTH	DIA METER	WEIGHT/ LENGTH	NORM DRAG COEFFICIENT	CONSTITUTIVE EXPONENT	NO. OF ELEMENTS	TANG DRAG COEFFICIENT
1	1	2	3000.00	1.000	.250	1.400	0*	50	.030
2	2	8	3000.06	1.000	.250	1.400	0*	50	.030
3	2	4	5000.00	.750	.200	1.400	0*	50	.030
4	4	9	5000.00	1.000	.250	1.400	0*	50	.030
5	4	10	3000.00	1.000	.250	1.400	0*	50	.030
6	9	7	4000.00	1.250	.370	1.400	0*	50	.030
							0.000		

PROPERTIES OF THE DEVICES LOCATED AT JUNCTIONS ARE AS FOLLOWS

DEVICE NO.	DEVICE WEIGHT	DEVICE DRAG COEFFICIENT	DEVICE FRONTAL AREA
2	3000.00	1.000	26.00
4	3600.00	1.600	26.00
7	3000.00	1.000	26.00

TOTAL NO. OF TRANSIENT DEVICES IS 7

ACCURACY REQUIRED IN CALCULATIONS IS .1000  
DECIMAL TEST CASE

ARRAY EQUILIBRIUM WITH NO CURRENT

ARRAY ANCHORS

JUNC. NO. OF ANCHOR	CABLE AT ANCHOR	TENSION AT ANCHOR	X-COMP	Y-COMP	Z-COMP	MGR.-CUMP	MGR.-CUMP	CABLE ANGLES WRT X-AXIS XY-PLANE
1	1	974.67	460.84	-420.50	745.39	628.30	-42.01	49.87
3	2	974.89	466.85	420.50	745.41	628.31	42.01	49.87
5	4	983.22	-466.83	423.53	754.60	630.33	137.78	50.13
6	5	983.28	-466.86	-423.53	754.65	630.35	-137.79	50.13

ANCHOR CABLES

CABLE NO.	MAXIMUM TENSION	S-CORD	MINIMUM TENSION	S-CORD
1	1622.02	3000.00	974.87	CF
2	1622.04	0.00	974.89	3000.00
3	1054.82	2500.00	933.69	46.01
4	1631.29	0.00	983.22	3000.00
5	1631.35	0.00	983.28	3000.00
6	3000.00	4000.00	1800.00	0.00

Figure 17. Continued.

**ARRAY JUNCTIONS**

JUNC.	CABLE AT JUNCTION	TENSION AT JUNCTION	CABLE ANGLES WRT XY-PLANE	JUNCTION LOCATION X-CORD Y-CORD Z-CORD
2 1	1622.02	137.99	-67.21	1116.22 -2.00 2588.59
2 2	1622.04	-137.99	-67.21	
2 3	933.74	.00	-.56	
4 3	933.74	-180.00	.57	5697.72 .02 2592.27
4 4	1631.29	-42.22	-67.27	
4 5	1631.35	42.21	-67.27	
7 6	3000.00	0.00	-90.00	7000.00 -1000.00 4000.01

**INDEXED DEVICES ALONG ARRAY CABLES**

DEVICE INDEX	CABLE NO.	COORDINATE	TENSION AT DEVICE	DEVICE LOCATION X-CORD Y-CORD Z-CORD	DEVICE WEIGHT	DEVICE LENGTH	NORMAL DRAG CO	TANG DRAG CO
1	1	750.00	1124.74	698.08 599.49	.00	0.00	0.000	0.000
2	1	1500.00	1284.54	625.66 436.45	.00	0.00	0.000	0.000
3	1	2250.00	1450.98	882.06 205.51	.00	0.00	0.000	0.000
4	2	750.00	1451.00	882.06 -205.51	.00	0.00	0.000	0.000
5	2	1500.00	1284.56	625.66 -436.45	.00	0.00	0.000	0.000
6	2	2250.00	1124.76	334.41 -698.79	.00	0.00	0.000	0.000
7	3	1000.00	952.99	2103.66 .00	.00	0.00	0.000	0.000
8	3	2030.00	1012.17	3057.19 .01	.01	0.00	0.000	0.000
9	3	2500.00	1054.62	3509.25 .01	.01	2980.75 1000.00	0.000	0.000
10	3	3000.00	1119.43	3958.20 .01	.01	3193.98 3020.73	1.000	0.000
11	3	4000.00	956.85	4906.32 .01	.01	2707.82 2707.82	0.000	0.000
12	4	4600.15	1124.52	-2115.74 1967.75	.00	0.00	0.000	0.000
13	4	1500.00	1293.56	6379.21 -436.80	.00	0.00	0.000	0.000
14	4	2250.00	1133.51	6666.31 -699.00	.00	0.00	0.000	0.000
15	5	750.00	1461.21	6124.52 215.77	.00	0.00	0.000	0.000
16	5	1500.00	1293.61	6379.21 436.42	.00	0.00	0.000	0.000
17	5	2250.00	1133.57	6666.31 699.09	.00	0.00	0.000	0.000
18	6	1000.00	2100.00	7000.00 -1000.00	.00	0.00	0.000	0.000
19	6	2000.00	2400.00	7000.00 -1000.00	.00	0.00	0.000	0.000
20	6	3000.00	2700.00	7000.00 -1000.00	.00	0.00	0.000	0.000

Figure 17. Continued.

DECCELL TEST CASE  
APPLY 90 DEGREE CURRENT (CLOCKWISE - Y AXIS)

NUMBER OF ITERATIONS FOR CONVERGENCE = 12  
CURRENT FIELD OPITION IS 1

Z-COORDINATE OF CURRENT	MAGNITUDE OF CURRENT AT Z	DIRECTION OF CURRENT AT Z FROM N-AXIS
(DEGREES)	(KNOTS)	(DEGREES)
0.00	0.000	0.000
500.00	*300	0.000
700.00	*300	0.000
1000.00	*900	0.000
7000.00	1.500	0.000

\*\*\*\*\*CURRENT DIRECTION IS POSITIVE IN THE CLOCKWISE SENSE FROM THE N-AXIS\*\*\*\*\*

ARRAY EQUILIBRIUM WITH 270.00 DEGREE CURRENT

ARRAY EQUILIBRIUM WITH CURRENT DIRECTION  
270.00 DEGREES FROM X-AXIS (+ IS COUNTERCLOCKWISE)  
90.00 DEGREES FROM N-AXIS (+ IS CLOCKWISE)

ARRAY ANCHORS

JUNC. NO.	CABLE AT ANCHOR	TENSION AT ANCHOR	X-COMP	Y-COMP	Z-COMP	MCR-COMP	CABLE ANGLES WRT X-AXIS XY-PLANE
1	1	2120.84	921.12	-1197.18	1488.11	1510.53	-52.42 44.58
3	2	105.56	93.45	15.84	-46.45	94.79	9.64 -26.10
5	4	104.64	-92.76	15.83	-45.78	94.10	-25.94
6	5	2135.04	-921.38	-1202.57	1504.41	1514.96	-127.46 44.80

ARRAY CABLES

CABLE NO.	MAXIMUM TENSION	MINIMUM TENSION	S-COORD CF	MAXIMUM S-COORD CF	LOCATION OF THIS POINT X-COORD Y-COORD Z-COORD	NO CURRENT LOC. OF THIS POINT X-COORD Y-COORD Z-COORD
1	2704.86	3000.00	2120.84	0.00	986.17 3700.00 1172.55 1110.22	-421.42 2354.31 809.81 -270.59
2	696.34	0.00	94.10	2814.21	576.02 970.69 1027.61 1451.71	-739.14 -1034.93 2825.89 3510.22
3	1274.32	2500.00	1175.96	2550.07	1090.02 2561.10 3508.36 5976.03	-738.15 -738.15 -1034.93 1457.38
4	696.81	6.00	94.10	2616.90	970.61 5834.45	-738.15 2359.53
5	2724.35	0.00	2135.04	3000.00	483.26 0.00	-418.76 5897.72
6	3001.43	4000.00	1891.74	0.00	1363.45 4000.00	-2333.47 3715.67 7000.00 -1000.00

Figure 18 Output from DECCELL1.

AD-A093 356

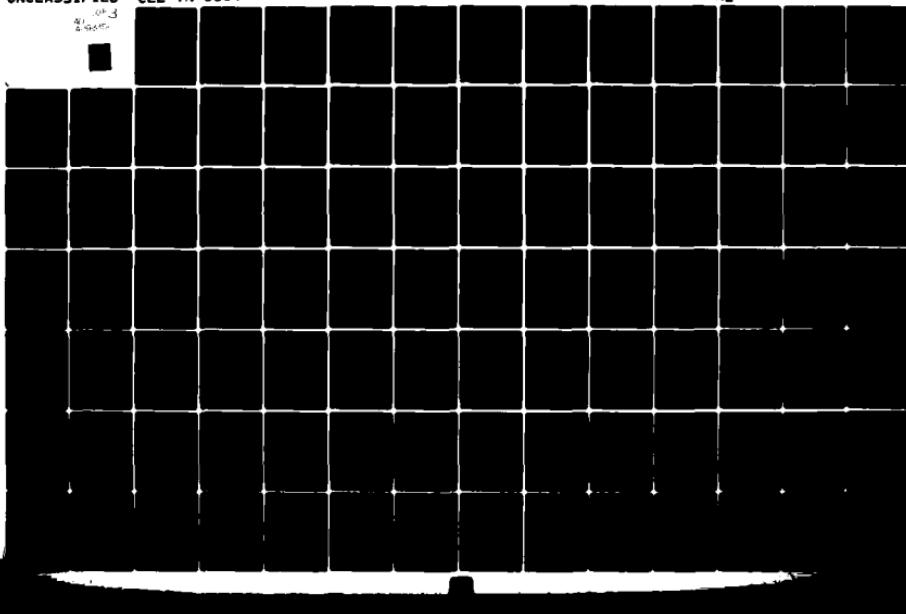
CIVIL ENGINEERING LAB (NAVY) PORT HUENEME CA  
DECCEL1 USERS MANUAL. A FORTRAN IV PROGRAM FOR COMPUTING THE STA--ETC(U)  
AUG 80 S SERGEV  
CEL-TN-1584

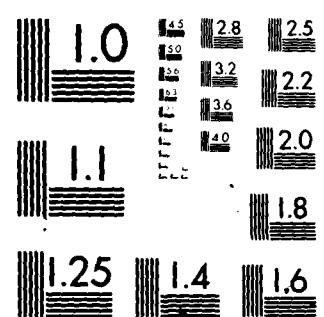
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MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS 1963-A

ARRAY JUNCTIONS

JUNC.	CABLE AT	TENSION AT	CABLE ANGLES WRT	JUNCTION LOCATION	DISP FROM NO CURRENT	DISP 1 AM ORIG NO CURRENT
NO.	JUNCTION	JUNCTION	X-AXIS XY-PLANE	X-COORD Y-COORD Z-COORD	X=DISP Y=DISP Z=DISP	X=DISP Y=DISP Z=DISP
1	27100.00	27100.00	1.36.0.81	117.0.55 -421.0.42	2354.31 -421.42 -234.28	62.33 -421.42 -234.28
2	2	696.39	-104.61	-63.07	-1.68 -1.68 -1.68	-1.68 -1.68 -1.68
2	3	1183.16	-127.14	-50	5834.45 -418.76 2359.53	-63.27 -418.76 -63.27
4	3	1183.49	-152.72	-50	-	-
4	4	696.71	-75.56	-63.00	-	-
4	5	2729.35	43.31	-60.55	-	-
7	6	3191.43	90.00	-88.23	7000.00 -2333.47 3715.67	.00 -1333.47 -284.34

INDEXED DEVICES ALONG ARRAY CABLES

DEVICE INDEX	CABLE NO.	COORDINATE	DEVICE	TENSION AT	DEVICE LOCATION	DISP FROM NO CURRENT	DISP FROM ORIG NO CURRENT
					X-COORD Y-COORD Z-COORD	X=DISP Y=DISP Z=DISP	X=DISP Y=DISP Z=DISP
1	1	750.00	2256.30	2547.87	589.93 542.51 1115.20	-104.43 -108.85 -120.97	-108.85 -120.97 -123.46
2	1	1500.00	2399.83	1500.00	614.23 208.61 1115.20	-11.43 -227.84 -123.46	-11.43 -227.84 -123.46
2	1	2250.00	2547.87	898.33	-134.96 1718.08 1662.67	-340.67 -166.34 -166.34	-340.67 -166.34 -166.34
3	1	2750.00	521.60	1067.69	-688.35 1067.69 906.55	-482.83 -241.75 -241.75	-482.83 -241.75 -241.75
4	2	3000.00	341.51	906.55	-820.23 943.19 894.13	-363.78 -295.48 -295.48	-363.78 -295.48 -295.48
5	2	3250.00	169.94	620.14	-894.13 257.07 285.72	-195.35 -342.41 -285.72	-195.35 -342.41 -285.72
6	2	3500.00	1193.47	2092.39	-802.26 2417.37 2650.43	-802.26 -267.46 -330.32	-802.26 -267.46 -330.32
7	3	3750.00	1239.35	3040.22	-1006.85 2825.47 1668.23	-16.97 -1006.86 -330.32	-16.97 -1006.86 -330.32
8	3	4000.00	1274.32	3507.35	-1034.92 1668.23 948.62	-1.90 -1034.93 -368.51	-1.90 -1034.93 -368.51
9	3	4250.00	1245.35	3972.33	-1007.15 2683.28 1118.42	14.13 -1007.16 -337.45	14.13 -1007.16 -337.45
10	3	4500.00	1196.75	4916.46	-801.46 2436.58 590.79	10.14 -801.46 -271.24	10.14 -801.46 -271.24
11	3	4750.00	522.08	-686.98	1668.23 1866.18 1866.18	-481.25 -239.48 -186.18	-481.25 -239.48 -186.18
12	4	5000.00	361.95	5938.34	-619.88 1866.18 261.18	-383.08 -292.72 -281.18	-383.08 -292.72 -281.18
13	4	5250.00	1500.00	6098.03	-819.88 948.62 948.62	-339.74 -339.74 -286.39	-339.74 -339.74 -286.39
14	4	5500.00	170.11	6381.92	-894.01 1722.43 1722.43	-185.29 -185.29 -174.40	-185.29 -185.29 -174.40
14	5	5750.00	2563.14	6107.12	-132.76 1118.42 1118.42	-338.53 -226.63 -122.92	-338.53 -226.63 -122.92
15	5	6000.00	2613.83	6389.56	210.20 590.79 590.79	10.35 17.69 -108.30	10.35 17.69 -108.30
16	5	6250.00	2270.95	6686.00	544.31 17.69 -108.30	-56.85 17.69 -108.30	-56.85 17.69 -108.30
17	5	6500.00	2149.66	7000.00	-1507.81 861.12 861.12	-138.68 -507.81 0.00	-138.68 -507.81 0.00
18	6	6750.00	2419.27	7000.00	-1930.95 1766.54 1766.54	-233.46 -930.95 0.00	-233.46 -930.95 0.00
19	6	7000.00	2000.00	2704.36	-2215.68 7000.00 7000.00	-276.09 -1215.68 0.00	-276.09 -1215.68 0.00
20	6	7250.00	3000.00				

ANALYSIS CUMPLIFIED

Figure 18. Continued.

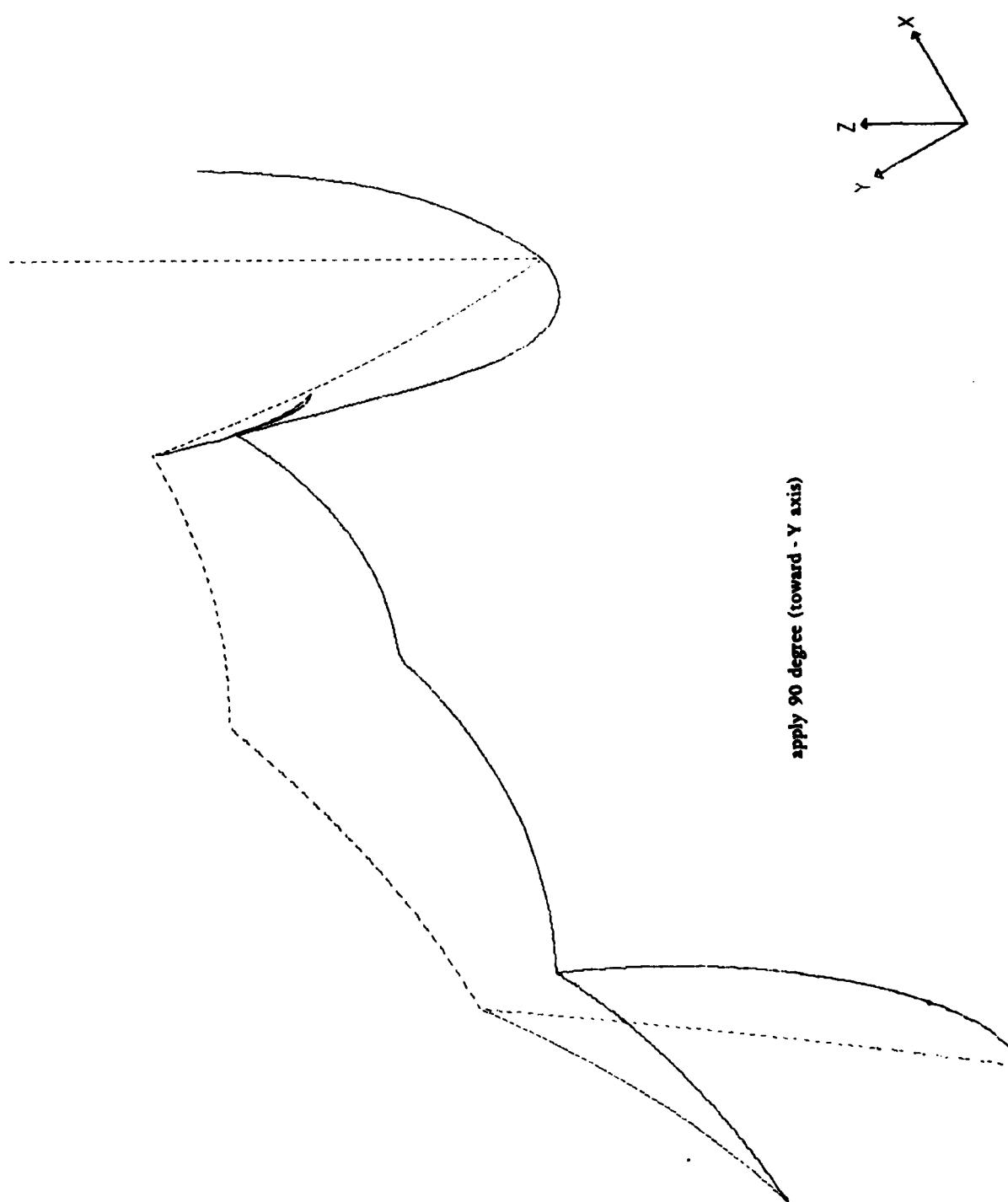


Figure 19. Undeformed and deformed configurations of the test case structure.

**Appendix B**  
**DECELL PROGRAM LISTING**

PHOTOGRAPH DECELL1

HTN 4.60433E 03/07/80 11.41.06 PAGE 1

1       DECELL1  
2       PROGRAM DECELL1(INPUT,OUTPUT,TAPE8,TAPE24,TAPE25,TAPE60=INPUT,TAPE6  
3        11=OUTPUT,TAPE3,TAPE4,TAPE10=FILE)  
4  
5       C     A FORTRAN IV PROGRAM FOR COMPUTING THE STATIC DEFLECTIONS  
6       C     OF STRUCTURAL CAHLE ARRAYS  
7  
8  
9       C     DECELL1 IS THE CIVIL ENGINEERING LABORATORY'S ENHANCED  
10      C     VERSION OF THE \*DESADE\* PROGRAM WRITTEN BY RICHARD SKOOP  
11      C     AND JAMES MARK OF N.R.L. (\*DECELL1\* MEANS DESADE-CEL VERSION)  
12  
13  
14      C     QUESTIONS OR COMMENTS ABOUT DECELL1 SHOULD BE DIRECTED TO-  
15      C     STEVE SERGEY PHONE-(805) 982-5500  
16  
17  
18      C     COMMON /83/ VELX(125)\*VELY(125)  
19      C     PJUNCN /81/ IEJUNC,IRJDEL,IAJDELTA,IRS,TEJUNC,E,ES,FCAH,RCAH,JUMP,  
20      C     PJUNCN,PCAH,DCAH,PCAB0,KCAR0THETA,PJUNCO  
21  
22      C     COMMON /82/ MCAB,KNONE,ERJUNC,IRJUNC,DAL,DATN,H,PJUNC,CUCAH,DCAB,  
23      C     IFATE,NANC,ANJUNC,IEKAU,IPKNU,INTAPE,OUTAPE,ITIME,IFLG,OFLGNR,THE  
24      C     IAS,THEIAS,CDPDU,IETAB,IIJUNC,RHU,TEST,INSEG,ZVEL,VELZ,PIR,ECICA8,  
25      C     3EPCAH,2JUNC,LJUNC,PAH,ICAB,IVOPT,WCAH,1UEV,IC-ECK,NDEV,NDATC  
26      C     COMMON /S1/ TITLE,IPHA,CONTIS,IUNIT,VELXP(25)\*VELY(25)\*VELYP(25)  
27      C     COMMON /PL1/ KPH1,SIZE,TH3,IPOP,KCPL1  
28      C     COMMON /NITER/ KOUNIP,NIT,WATER,NSTEPS,ISTEP,PERCNTV,INPRINT  
29      C     COMMON /PIBLV/ PL  
30      C     DIMENSION PJUNC(3,51,22), RCAAH(3,51,22), PJJUNC(3,44), TJJUNC(3,44), PJJUNC(3,44)  
31      C     DIMENSION FCAH(3,51,22), RCAAH(3,51,22), PJJUNC(3,44), PCAH(3,51,22)  
32      C     DIMENSION PCAH(3,51,22), RCAAH(3,51,22)  
33      C     DIMENSION PJUNC(3,44), CUCAH(22), UCAB(22), ANJUNC(44), TFS(14)  
34      C     DIMENSION ZVIL(25), VELZ(25), ECICA8(22), EXPCA8(22), ZJUNC(22)  
35      C     DIMENSION LON(125), FATH(22), ICAB(22), WCAH(22), IUEV(100)  
36      C     DIMENSION ICHCK(44)  
37      C     DIMENSION UATT(2154,11)  
38      C     EQUIVALENCE ICHCK(11),PJJUNC(11)  
39      C     INTEGER ONTAK,ZJUNC,ERJUNC,ANJUNC,OFLG  
40      C     REAL Th,Re  
41      C     CALL Inform  
42      C     F1=2,\*ASIN(1.0)  
43  
44  
45  
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57

C     NT IS THE NUMBER OF ITERATIONS ALLOWED BEFORE THE PROGRAM IS  
C     TERMINATED  
C     IF CONVERGENCE HAS NOT BEEN REACHED BY NT/2 ITERATIONS, AN  
C     AVERAGE OF SUCCESSIVE NOVEL POSITIONS WILL BE MADE FOR AN  
C     ADDITIONAL NT/2 ITERATIONS.  
C  
5     IFINS1=1  
5     ISCH=25  
5     IFIN1) ISCH

PROGRAM LEVEL 1 74/74 UP1=1 FIN 4.6+433E 03/07/80 11.41.06 PAGE 2  
 ADVANTAGE  
 MCUM>0  
 ACURTHEC  
 60 C  
 L1ME=1  
 CALL INPUT TO READ DATA AND IDENTIFY ERRORS  
 C  
 IF (MCUM>0) IF1MS=0  
 65 IN CALL INPUT  
 IF (MCUM>0) IF1MS=0  
 C  
 CHECK TO SEE IF ANY ERRORS IN DATA  
 C  
 IF (FATE>NE.0.) GO TO 305  
 70 C  
 GET HERE IF NO ERRORS -- PRINT OUT PHYSICAL CHARACTERISTICS OF ARR  
 C  
 ABLE (IPRN),3101  
 CALL PHSUUT  
 75 C  
 KPULI IS A MULTIPLIER FOR CHANGING CURRENT ANGLE THETA  
 C  
 KPULI=0  
 JE (L1FHST,NE.0.) GO TO 15  
 76 C  
 JUMP TO --NU CURRENT  
 C  
 JUMP TO --NU CURRENT  
 C  
 JUMP TO --CURRENT  
 78 C  
 JUMP TO  
 79 C  
 JF (L1FHST,NE.0.) GO TO 15  
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115      DO 45 J=1,3          115
        LEJ
        45 FFJUNC(I,K)=FFJUNC(I,K)+EFORCE(I,K)*KUMMY(KUMMY)    116
        GO TO 35
        30 KUMMY(I,J)=H(I,K)*1.000001                         117
        MUMAT(I,J)=H(I,K)*1.000001
        UC-55-J=1,J
        I=J
        55 FCAH(I,M,K)=FCAB(I,M,K)+FFORCE(I,M,K)             118
        GO TO 35
120
125      C   GET HERE AT END OF TAPE                           119
        C   GO REWIND INTAPE                                     120
        C   NOW CALCULATE THE FORCE/LENGTH IN DIRECTION I AT NODE M ON CABLE N 121
        C   CFORCE(I,M,K) IS ROUTINE FOR DOING THIS -- INTEGRATE_BY_IHAPEZOIDA 122
        C   WHILE OVER SEGMENT TO GET TOTAL FORCE AND ADD TO OCAB FORCES 123
        C
        10 65 J=1,NCAH
        KAJ
        130      INHMINIQUE(K)=1
        DO 65 MM=1,10NN
        MM
        10 65 MM=1,3
        11 65 II=1,3
        140      I=II+CAH(I,M,K)=FCAB(I,M,K)+CFORCE(I,M,K)+H(K)*0.5
        141
        C   ALL FORCES ARE NOW CALCULATED AND EQUILIBRIUM CAN BE DETERMINED 142
        C   LEAP = 1 FIRST TIME THROUGH IMAGINARY REACTION ROUTINE 143
        C   LEAP = 2 ANY OTHER TIME 144
        C   SKIP THIS SECTION IF NO TRAS 145
        C
        146      IF (NIR.EC.) GO TO 70
        IF (JUMP.EC.) CALL START
        LEAP=1
        147
        C   IF (NIR.EC.) GO TO 70
        IF (JUMP.EC.) CALL START
        LEAP=1
        148
        C   INITIALIZE HLLTA
        C   HLLTA=DELTA/I
        149
        150      C   INITIALIZE HLLTA
        C
        151
        152
        153
        154
        155      C   GET HERE TO INITIALIZE TOTAL FORCES AT THE JUNCTIONS, FFJUNC, AND 155
        C   IF THE IMAGINARY REACTION LIFTRATION NOT SATISFIED -- ALSO IF NO IR 156
        C   157
        C   158
        C   159
        C   160
        C   161
        C   162
        C   163
        C   164
        C   165
        C   166
        C   167
        C   168
        C   169
        C   170
        C   171
        165      C   ADD APPROXIMATE REACTIONS TO FFJUNC -- SKIP THIS SECTION IF NO IR 162
        C   IF (NIR.EC.) GO TO 95
        C   UC 96 J=1,FFJUNC
        C   UC 96 K=1,11W
        C   IF ((J.EQ.I)HJUNC(K).OR.(J.EQ.F)HJUNC(K)) GO TO 90
        C   UC 95 I=1,J
        C   170
        C   171
        174      C   IF JUNC(I,J)=FFJUNC(I,J)+H(I,J)

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      94 CONTINUE
C   IF JUNC IS NOT DETERMINED AND THE REACTIVE FORCES IN THE ARRAY HCA
C   CAN BE CALCULATED BY SUMMING FROM THE FREE ENDS TO THE FIXED ANCHO
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      95 NC 130 #1,NCAB
      96 IM,DR,NCAB,I=1,N
      97 KAPATH(INDX)
      98 INNN=NNODE(K)
      99 IF,L,JNLJUNC(K)
      100 DO,109 I=1,3
      101 HCAH(I,INNN,K)=TCJUNC(I,INLJ)
      102 HCAH(I,INNN,K)=TCJUNC(I,INRJ)
      103
      104 DO,115 I=1,3
      105 HCAH(I,INNN,K)=RCAB(I,INN,N,K)+RCAB(I,INL,K)
      106 IF(L,JNLJUNC(L),EQ,2)JUNC(L)= 60 TO 105
      107 DO,110 I=1,3
      108 HCAH(I,INNN,K)=RCAB(I,INN,N,K)+RCAB(I,INR,K)
      109 CONTINUE
      110 DO,125 M=1,INNN
      111 HCAH(M,INNN)=M-1,M
      112 IF,(M,EG,1) GO TO 130
      113 DO,120 I=1,3
      114 HCAH(I,M-1,K)=RCAB(I,M,K)+FCAB(I,M-1,K)
      115 CONTINUE
      116 CONTINUE
      117
      118 ALL REACTIVE FORCES ARE NOW DETERMINED AND THE CONFIGURATION OF THE
      119 ARRAY PCAM AND HJUNC CAN BE FOUND BY INTEGRATING FROM THE FIXED
      120 ANCHOR TO THE FREE ENDS -- INTEGRATION BY THE TRAPEZOIDAL RULE IS
      121 AGAIN USED
      122
      123 DO,155 N=1,NCAN
      124 KAPATH(N)
      125 INNN,JUNC(K)
      126 INNN=NNODE(K)
      127 INZ=2,JUNC(K)
      128
      129 DO,135 I=1,3
      130 HCAH(I,1,K)=PCAB(I,INZ)
      131 HCAH(I,1,K)=MM#2,INNN
      132 DO,145 I=1,3
      133 IF,(I,TCAB(M,K),NE,0,) GU TU 149
      134 HCAH(I,M,K)=PCAB(I,M-1,K)+(TCAB(M-1,K)*HCAH(I,M-1,K))/TCAB(M,K)
      135 HCAH(I,M,K)=PCAB(I,M-1,K)+(TCAB(M-1,K)*HCAH(I,M-1,K))/TCAB(M,K)/2
      136
      137 CONTINUE
      138 DO,150 I=1,3
      139 HCAH(I,1,K)=PCAB(I,INN#K)
      140 CONTINUE
      141 IF,(KUW,I,L,1,1/2) GU TU 175
      142 IF,(KUW,I,L,1,1/2) GU TU 175
      143 HCAH(N=1,NCAN)
      144 KAPATH(N)
      145 INNN=NNODE(K)
      146
      147 DO,170 N=1,NCAN
      148 KAPATH(N)
      149 INNN=NNODE(K)
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230      UC 160 I=1,MNN          229
         UC 160 I=1,3          230
         160 PCABIL(M,K)=0.5*(PCABIL(M,K)+PCABEL(M,K)) 231
         DO 165 I=1,3          232
165  PJUNCT(I,I,NLN)=PCABIL(I,I,NLN,K)          233
170  CONTINUE          234
175  CONTINUE          235
C
C  ARRAY-CONFIGURATION NOW DETERMINED -- CHECK TO SEE IF IT SATISFIES 236
C  GEOMETRIC CONSTRAINTS -- SKIP THIS SECTION IF NO IT'S 237
C
C  IF (NIR.EQ.0) GO TO 245 238
C
C  CALCULATE ERROR E 239
C
C  E2=0. 240
C  UC 180 N=MNN          241
C  KIN=IJUNC(I,I)          242
KIN=IJUNC(I,I)
DO 180 I=1,3          243
180 E2=E2+(PJUNCT(I,I,NLN)-PJJUNC(I,I,NLN))*#2          244
ESQR(E2)          245
C
C  COMPARE ERROR TO ACCURACY REQUIREMENTS 246
C
C  IF (E.LE.COMPD/10.) GC TO 245 247
C
C  GET HERE IF GEOMETRIC CONSTRAINTS NOT SATISFIED 248
C
C  GO TO 185,220, LEAP 249
C
C  GET HERE FIRST TIME THROUGH IMAGINARY REACTION ROUTINE 250
C
C  185 LEAPS2          251
KTH=0
FPREV=0.0
C
C  STORE SUCCESSFUL POSITIONS AND REACTIONS 252
C
C  190 F=0 253
C
C  KIN=MNN,M+I,I/2 ITERATIONS THEN BEGIN THE CHECK FOR SLOW CONVERGENCE 254
C  ALLOW MAXI=F/2 ITERATIONS 255
C
C  IF (KIN>0.05*MAXI/2) GO TO 256
C
C  CONVERGENCE = IF THE DISPLACEMENT 257
C  ERROR IS LARGE COMPARED TO THE CONVERGENCE TOLERANCE AND IS 258
C  CHANGING SLOWLY = SLOW CONVERGENCE IS INDICATED AFTER MAXITER/2 259
C  ITERATIONS 260
C
C  IF (KIN>C1*AND>E0)*COMPUS100.0*AND*EPREV>E1*COMPDI GO TO 261
C  LIMIT THE ITERATIONS TO SATISFY THE DISPLACEMENT TOLERANCE AT THE 262
C  CUTS TO MAXITER 263
C  IF (KIN>C1*MAXITER) GO TO 264
C
C  GO TO 210 265
C
C  195 WRITE (IPRN1,320) KIN 266
C  GC TO 205 267
C
C  260 WRITE (IPRN1,325) M11,F4 268
C  265 WRITE (IPRN1,320) FILE 269
C  *FILE (IPRN1,335) EPREV*E*COMPDI 270
270
275
280
285

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IPCIVEL,I=1,KIN=100
IF (IRSTEN$G1=1) WRITE (IPRNT,340) IPCIVEL
      WRITE (IPRNT,1345)
      GC TO 305
215 EPICVEL
      IC 215 KIN,NAH
      KEN=EHJUNC(N)
      NH=IHJUNC(N)
      UC 215 I=1,3
      PJUNCS(I,KEN)=PJUNC(I,KEN)
      PJUNCS(I,KIN)=PJUNC(I,KIN)
      215 IRS(I,KIN)=IR(I,KIN)
      GC TO 225

C   SET HERE ANY OTHER TIME THROUGH IMAGINARY REACTION ROUTINE
C   SEE IF ILLATION SUCCESSFUL
      C 220 IF (ELTLES) GO TO 190
      C REDUCE DELTA IF NOT SUCCESSFUL ITERATION
      C DELTA=DELTA/2.

C   CALCULATE NEW IMAGINARY AND EQUILIBRATING REACTIONS AND GO BACK TO
      C   RECALCULATE ARRAY EQUILIBRIUM
      C 225 DO 230 NZ+1,NAH
      KEN=EHJUNC(N)
      UC 230 I=1,J
      230 IR(I,KEN)=0.
      UC 235 N=1,NAH
      NEN=EHJUNC(N)
      NH=IHJUNC(N)
      10 235 I=1,3
      IR(I,KIN)=IRS(I,KIN)+DELTAS*(PJUNCS(I,KEN)-PJUNCS(I,KIN))/ES
      235 IR(I,KEN)=IR(I,KEN)-TR(I,KIN)

C   CHECK CHANGES IN IMAGINARY REACTIONS
      C 240 DO 245 NZ+1,NAH
      KIN=IHJUNC(N)
      UC 245 I=1,3
      IF (IR(I,KIN)-NE.IRS(I,KIN)) GO TO 70
      245 CONTINUE

C   NO CHANGES -- TIME TO QUIT
      C CALL ERROR
      GC TO 335

335 C   GET MEPE IN ACCURACY REQUIREMENTS SATISFIED OR NO IRS
      C   OUTPUT EQUALIBRIUM IF NO CURRENT -- IF CURRENT, F FIRST CHECK TO SEE
      C   IF ACCURACY REQUIREMENT SATISFIED BY SUCCESSIVE APPROXIMATIONS
      C   246 IF TRUE
          C   IF (JUMP=NE.0) GO TO 250
      250 CONTINUE

```

PROGRAM 1.ECFL1 7474 OPT=1

FIN 4.6.433E

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343  
JL.NE=JUMP+1  
344  
345 DC 10 (225,235)\* JUM  
IF ((JFLG.EQ.0).OR.(QFLG.EQ.0)) CALL STRUJI  
IF ((KPLT.NE.0).AND.(JN.AC.0)) CALL PERPLT (IVOPT,NCAB,NNODE,PCAB,PC  
JN,NTITLE)  
IF ((QFLG.EQ.0).OR.(QFLG.EQ.0)) CALL TAPOUT  
IF ((JFLG.EQ.0).OR.(QFLG.EQ.0)) GO TO 270  
IF (JUM.NE.0) GO TO 270  
DC 250 N=1,NCAH  
IN.WHENODE(IN)  
DC 265 M=1,1,VAN  
DC 266 I=1,3  
PCAB(1,M,N)=FCAH(1,M,N)  
267 RCAB(1,M,N)=HCAB(1,M,N)  
DC 265 N=1,N,JUNC  
DC 265 I=1,3  
268 PUN(COL1)=PUNC(1,N)  
IF ((KPLT.NE.0).AND.(IVPT.EQ.0)) CALL PERPLT (IVOPT,NCAH,NNODE,PCAB,  
JPCAB(TITLE))  
C APPLY CURRENT IF REQUIRED  
C 361  
362  
363  
364  
365 C 271 IF ((IVOPT.EQ.0)) GO TO 300  
JL.NP=1  
IF ((JUM.EC.0)) GO TO 275  
IF ((KPLT.NE.0)) CALL CPLT (IVOPT,IPRNT,PJUNC,NANC,TITLE,ANJUNC)  
IF ((TMNGE,THETA)) GO TO 309  
RESULT=KMULT\*I  
IF THI=1  
C STORE EXISTING CONFIGURATION FOR COMPARISON PURPOSES  
C 373  
374  
375 DC 280 N=1,NCAH  
IN.WHENODE(IN)  
DC 280 V=1,1,VAN  
DC 280 I=1,3  
PCAB(1,M,N)=FCAH(1,M,N)  
281 CCNTRUE  
C RECALCULATE FORCES  
C 382  
383 IF ((IFT.EQ.0)) GO TO 20  
GO TO 15  
C IF THERE IF CURRENT -- CHECK SUCCESSIVE APPROXIMATION ACCURACY  
C 387  
388  
389  
390 C 390  
C INIT THE INITIAL NUMBER OF ITERATIONS TO GET THE CARL SHAPE  
C 391  
C TO HIT ITERATIONS WRITE (IPRNT,350) KOUNTH,HULLCY,COMPD  
C 392  
C IF (KOUNTH.GE.NFL) CALL STRUJI  
C 393  
C IF (KOUNTH.GE.NFL) CALL STRUJI  
C 394  
C IF (KOUNTH.GE.NFL) GO TO 399  
C 395 DC 295 K=1,NCAH  
IN.WHENODE(IN)  
DC 295 M=1,NNOD  
U=0.

PROGRAM UECFL1 74/7+ OPT=1

FIN 4.6433E 03/07/80 11.41.06 PAGE 8

```
400      UC 230 J=1,N2
290 0=*(PCAB(I,M,N))-PCAB(I,M,N))**2          *89
C   IF NOT ACCURATE STORE CONFIGURATION AND RECALCULATE FORCES
C
405      IF (SGRT(U).GT.COMPU) GO TO 275
295  CONTINUE
C   GET HERE IF POSITION ACCURATE AND OUTPUT POSITION
C
410      IF (INCNPNEG.1.AND.ISTEP.LT.NSTEPS) CALL STROUT
C   CHECK TO SEE IF CURRENT IS TO BE INCREMENTED
C   IF (NSTEPS.EQ.1) GO TO 255
411      IF (NSTEP.LE.NSTEPS) NSTEP=NSTEP+1
412      IF (NSTEP.GT.NSTEPS) NSTEP=NSTEPS
413      IF (NSTEP.GT.NSTEPS) GO TO 255
414      GO TO 275
C   GO BACK FOR MORE DATA
415
C
300  IF(INITIAL .NOT.TRUE.) GO TO 101
305  CONTINUE
310  WRITE (IPRINT,355)
      GO TO 5
420
425
C
310  FORMAT (//,1X,1BNU ERRORS DETECTED)
315  FORMAT (F4.,0A4.0E15.8)
320  FORMAT (1B123HLOW CONVERGENCE AFTER 151H ITERATIONS/)
325  FORMAT (1B123HCONVERGENCE IN 151H ITERATIONS/)
330  FORMAT (1B1 CASE TITLE/1X,0I10,1X,0A10,1)
335  FORMAT (124H PREVIOUS ERROR (COMP VALUE) = 'E15.5/24H PRESENT ERROR VALUE
1 = 'E15.5/34H ACCEPTABLE ERROR (COMP VALUE) = 'E15.5)
340  FORMAT (123H PRESENT VALUE OF CURRENT = '14.22H PERCENT OF FULL VA
1LUE)
345  FORMAT (//39H PARAMETRIC CASE TERMINATED, SEE MANUAL)
350  FORMAT (123HUMPHOGHAY DID NOT CONVERGE AFTER 151X138ITERATIONS,
1 PARAMETRIC CASE TERMINATED/26H BEST ACCURACY CATTAINED = 'E15.4/2
27H DESIRED ACCURACY (CUMP) = 'E15.4//28H APPROXIMATE RESULTS PRIN
3TEUD/1X.27(I1H))
355  FORMAT (1I1)
      END
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CARD NR. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

250 1 250 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
341 1 341 THIS IF DEGENERATES INTO A SIMPLE TRANSFER TO THE LABEL INDICATED.
344 1 344 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

SUBROUTINE INFORM 74/74 OPT=1

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PAGE 1

```
1      *DECK INFORM
2      SUBROUTINE INFORM
3      C
4      C THIS SUBROUTINE IS USED TO INFORM THE USER OF UPDATES THAT HAVE
5      C BEEN ADDED TO DECFL THAT MAY AFFECT INPUT OR CALCULATIONS OR
6      C OUTPUT. ANY NEW UPDATES SHOULD BE DESCRIBED HERE BY ADDING TO THE
7      C ANY NEW UPDATES SHOULD BE DESCRIBED HERE BY ADDING TO THE
8      C ANY NEW UPDATES SHOULD BE DESCRIBED HERE BY ADDING TO THE
9      C ANY NEW UPDATES SHOULD BE DESCRIBED HERE BY ADDING TO THE
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17     C ANY NEW UPDATES SHOULD BE DESCRIBED HERE BY ADDING TO THE
18     C ANY NEW UPDATES SHOULD BE DESCRIBED HERE BY ADDING TO THE
19     C ANY NEW UPDATES SHOULD BE DESCRIBED HERE BY ADDING TO THE
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FIN 4.6433E

03/07/80 11:41:06

PAGE 1

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1      FUNCTION CFORCE    74/74   OPT=1

4      SUBROUTINE CFORCE (I,M,N)
5
6      C THIS ROUTINE CALCULATES THE FORCE/LENGTH IN DIRECTION I AT NODE M
7      C IN CABLE N USING THE NORMAL DRAG FORCE APPROXIMATION
8
9      C
10     COMMON /B3/  VELX(25),VELY(25),
11          EJUNC,IR,DELT,IIRS,TFJUNC,E,ES,FCAB,R,CAB,JUMP,CFO
12          PCAB,PCLB,PCAB0,RCAB0,THETA,P_JUNC,
13          COMMUN/B2/  NCAH,NNODE,EHJUNC,DATI,DATN,T,PJUNC,CDCA,B,DCAB,CFO
14          IFLATE,NANC,AHJUNC,IHEAD,JPNT,INTAPE,UTAPE,ITIME,OFLG,NIR,THECFO
15          2TAS,THEIAE,CUPD,THETAB,NJUNC,PHOTEST,INSEG,ZVEL,VELZ,PIP,ECICAB,CFO
16          EXP CAB,ZJUNC,LJUNC,PATH,ICAB,ILOPT,MCAB,IDEV,ICHECK,NDATC,CFO
17          COMMUN /P1B/N  PI
18
19     DIMENSION FEJUNC(3,44), IRSL(3,44), IFJUNC(3,44), PJUNC(3,44), PJUNC0(CFO
20
21     DIMENSION FCAB(3,51,22), RCAB(3,51,22), PJUNC(3,44), PCAB(3,51,22)CFO
22
23     DIMENSION PCAB(3,51,22), PCAB0(3,51,22), RCABU(3,51,22)CFO
24
25     DIMENSION NJUCE(22), ERJUNC(44), IRJUNC(44), DAT1(10), DATN(10), CFO
26     1(22)CFO
27
28     DIMENSION PJUNC(3,44), CUCAB(22), DCAB(22), AHJUNC(44), TEST(14)CFO
29     DIMENSION ZVEL(25), ECLCAB(22), EXP CAB(22), ZJUNC(22)CFO
30
31     DIMENSION LJUNC(22), PA1H(22), ICAB(22), MCAB(22), IUEV(1000)CFO
32
33     DIMENSION ICHECK(44)CFO
34
35     DIMENSION WICAB(3), VA0H(3), PSPACE(3)CFO
36
37     DIMENSION WM(3), VT(3)CFO
38
39     INTEGER ULTAPE,2JUNC,EHJUNC,AHJUNC,OFLGCFO
40
41     INTEGER PATHCFO
42     REAL IR,IRS
43
44     C CALCULATE THE WEIGHT/LENGTH VECTOR
45     C
46     C WICAB(1)=0,
47     C WICAB(2)=0,
48     C WICAB(3)=MCAB(N)
49
50     C CHECK TO SEE IF CURRENT OH NO CURRENT
51
52     C JUM=JUMP+1
53     C GC 10 (5,10), JUM
54
55     C GET HERE IF NC CURRENT
56
57     C S CFORCE=WICAB(1)
58     C RETURN
59
60
61     C GET HERE IF CURRENT
62     C CALCULATE LOCATION OF NODE IN SPACE
63
64
65     C UC 15 K=1,3
66     C PSPACE(IK)=PAT(K,M,N)
67     C F (IVOP1,EIG,3) CALL INTEL (INW,PSPACE)
68
69     C UC 20 K=1,3
70     C WICAB(K)=VELCC(K,PSPACE)

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25 CONTINUE
C CALCULATE THE TANGENTIAL PROJECTION OF THE CURRENT ON THE CABLE
60 C VPH0J=6.0
C DC=30 KK=1,3
      NKK
      VPH0J=VPRC(J*WH(K)*KCAB(K,M,N)/TCAB(M,N)
C CALCULATE THE NORMAL COMPONENT OF THE CURRENT AND ITS MAGNITUDE
65 C DC=35 KK=1,3
      NKK
      VNMAG=VNMAG*(VKRM(1)**2+VNORM(2)**2+VNORM(3)**2)
C CALCULATE THE FORCE/LENGTH
70 C
75 C CALCULATE TANGENTIAL COMPONENT OF CURRENT AND ITS MAGNITUDE
C
80 C VT(1)=WH(1)-VNORM(1)
C VT(2)=WH(2)-VNORM(2)
C VT(3)=WH(3)-VNORM(3)
C VIM=SLR(I,J)**2+VT(2)**2+VT(3)**2
C FUFHC=VFCAB(I)+RH0*(5*(UCAB(N)/12.0)*EXCAB(M,N)*(VNMG*VNORM(I)*
C CAH(N)+VPAV(I))*TUCAB(I)*P1)
      RETURN
85 C
      END

```

## CAPTION. SEVERITY DETAILS : DIAGNOSTS OF PROBLEM

AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

FUNCTION EFORCE 74/74 OPT=1  
 FTN 4.0+4.33E 03/07/80 11:41:06 PAGE 1

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 1 *DECK EFORCE
 2   FUNCTION EFORCE (I,J,N)
 3
 4   C THIS ROUTINE CALCULATES THE DEVICE FORCES IN DIRECTION I
 5   C USING THE NORMAL DRAG APPROXIMATION FOR IN-LINE DEVICES
 6
 7   COMMON /H2/ VEL(25),VELY(25)
 8   COMMON /H1/ FEJUNC,IR,DELTA,IHS,TFJUNC,E,ES,FCAB,DCAB,JUMP,EFO
 9   IPJUNC,PCAB,PLAIE,PCABU,WCABO,THETA,PJUNCU
10   COMMON /H2/ NCAH,NODE,ERJUNC,IRJUNC,UAT,IATN,TPJUNC,CUCAB,DCAB,EFO
11   AFATE,MANC,ARJUNC,INHEAD,OUTAFT,INTAPE,UTAPE,TEST,PRNI,IFLG,OFLG,NR,THEFO
12   PLAS,THETAE,CURPD,THETAB,INJUNC,RHO,TEST,NSEG,ZVEL,VELZ,PIP,ECICAB,EFO
13   EXP CAB,ZJUNC,LJUNC,PAIM,ICAB,IVOPT,WCAB,IDEV,ICHECK,INDEV,NDATC
14   COMMON /ANDG/ TDCAH(22),TDCAU(1000)
15   COMMON /PULK/P1
16   DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), 1FJUNC(3,44), PJUNC(3,44)
17   DIMENSION FCAB(3,51,22), WCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22)EFO
18   DIMENSION PCAHE(3,51,22), PCABO(3,51,22), RCAAU(3,51,22)
19   DIMENSION NNODE(22), ERJUNC(44), IRJUNC(44), DAT(10), DAIN(10), MEFO
20   DIMENSION PJUNC(3,44), CDCAU(22), DCAB(22), ANJUNC(44), TEST(14)
21   DIMENSION ZVEL(25), VEL(25), ECICAB(22), EXP CAB(22), ZJUNC(22)
22   DIMENSION LJUNC(22), PATH(22), ICAB(22), WCAB(22), IDEV(1000)
23   DIMENSION ICHECK(44)
24   DIMENSION WIEL(3), VNR(3), PSPACE(3)
25   DIMENSION W(3), WTCAB(3), VT(3)
26   INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
27   INTEGER PATH
28   REAL IR,IHS
29
30   C INITIALIZE LOCAL VARIABLES
31
32
33
34
35   C
36   C
37   C
38   C
39   C
40   C
41   C
42   C
43   C
44   C
45   C
46
47
48
49
50   C
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C GET HERE IF CURRENT OF DEVICE IN SPACE          EFO 58
C CALCULATE LOCATION OF DEVICE IN SPACE          EFO 59
C
C 11 INC 15 KK#1,3                                EFO 60
C
C 15 PSPACE(K)=SPACE(K)
C   IF ((VOPT(EG,3)) CALL INTVEL (TH,PSPACE)    EFO 61
C     IF ((VOP(EG,3)) GO TO 25                   EFO 62
C     IF ((VOP(EG,3)) GO TO 25                   EFO 63
C     DC 20 KK#1,3                                EFO 64
C     20 WH(K)=VELOC(K,PSPACE)                   EFO 65
C     25 CONTINUE                                 EFO 66
C
C 70 C CHECK IF DEVICE IS IN-LINE OR FREE          EFO 67
C
C 75 C GET HERE IF FREE TYPE DEVICE == CALCULATE MAGNITUDE OF THE CURRENT EFO 68
C   GC_10_(35,39),J JMP
C   30 VMAG=SQR(W(1)**2+W(2)**2+W(3)**2)          EFO 69
C
C 80 C CALCULATE THE FORCE ON THE FREE DEVICE      EFO 70
C   EFORCE=INTEL(1)*(HFO/2.)*DAT(17)*DAT(18)*VMAG*W(1)  EFO 71
C
C 85 C GET HERE IF IN-LINE DEVICE                  EFO 72
C   CALCULATE THE TANGENTIAL PROJECTION ON THE CURRENT ON THE DEVICE EFO 73
C   TANG(1) EVALUATES THE UNIT TANGENT TO A CAABLE AT ANY POINT EFO 74
C
C 90 C KK#1,3                                     EFO 75
C   UC 4U_KK#1,3
C   KK#1,3
C   VPROJ=VPROJ*W(1)*W(1)*TANG(K)
C
C 95 C CALCULATE THE NORMAL COMPONENT OF THE CURRENT AND ITS MAGNITUDE EFO 76
C   100 KK#1,3
C   KK#1,3
C   NZK
C   45 VJRH(K)=W(K)-VPHO*(ANG(K))
C   VMAG=SQR(W(1)**2+W(2)**2+W(3)**2)          EFO 77
C
C 100 C CALCULATE THE TANG. COMPONENT OF THE CURRENT AND ITS MAGNITUDE EFO 78
C   V(1)=W(1)-VNORM(1)
C   V(2)=W(2)-VNORM(2)
C   V(3)=W(3)-VNORM(3)
C   VIM=SQRT(V(1)**2+V(2)**2+V(3)**2)          EFO 79
C
C 110 C CALCULATE THE FORCE IN THE IN-LINE DEVICE      EFO 80
C   THM#1=TEL(1)
C   THM#2=VPHO*VNORM(1)*(L*UMU-CUCAB(N)*DCAB(N)/12.)
C   THM#3=VNORM(1)*PI*(L*VUCAH(N)*TOCAH(N)*DCAH(N)/12.)
C   EFORCE=THM#1+0.5*HFO*DL*(THM#2+THM#3)
C
C 115 C RETURN                                     EFO 81

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FUNCTION FORCE 74/74 OPTIM PAGE 3  
FTN 4.6+4.33E 03/07/80 11.41.06  
115 END EFO 115-

CARD NO. SEVERITY DETAILS DIAGNOSTS OF PROBLEM

52 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
74 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

SUBROUTINE THRUH

FIN 4.6.43E

03/01/80 11.41.06

PAGE 1

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1      SUBLK FPNH  
2      SUBROUTINE THRUH  
3      C  IF IS RQD(L) GENERATES A TYPE 18 ERROR MESSAGE  
4      C  HERE IF ALL IMAGINARY REACTIONS DJ NOT CHANGE  
5      C  
6      COMMON /D3/ VELX(125), VELY(125)  
7      CCNOM, R11, FEJUNC, L, DELTA, IMS, FCAB, MCAD, JUMP, ERR  
8      PJUNC, PLAD, PCABE, PCABD, RCABD, THETA, PJUNC  
9      CCABD, /32/ NCAB, NODC, THJUNC, TRJUNC, DATI, DATN, H, PJUNC, CUCAB, DCAB, ERR  
10     IFLAT, INANC, ANJUNC, IFLG, OFLG, NI, THEERR  
11     21AS, THEIA, COMP, THEIA, NJUNC, PTHO, TESI, NVSEG, VELZ, PIP, ECICAB, ERR  
12     3EP, CAB, 2JUNC, JUNC, PATH, ICAB, DIVPT, MCAB, IOFV, 1CPECK, ND, EV, RUMTC, ERR  
13     DIMENSION FEJUNC(13,4), IR(13,4), IR(13,4,4), IFJUNC(13,4,4), PJUNC(14,4)  
14     DIMENSION FLAB(3,51,22), RCAB(3,51,22), PJUNC(3,51,22), PCAH(3,51,22), ERR  
15     DIMENSION PCAE(3,51,22), PCABD(3,51,22), WCAB(3,51,22), ERR  
16     DIMENSION NJDC(122), EHJUNC(144), IRJUNC(144), DATI(110), DATN(110), MERR  
17     1(22) 1(22)  
18     DIMENSION PJUAC(3,44), CUCAB(122), DCAB(122), AJJUNC(44), TEST(114), ERR  
19     DIMENSION ZVEL(125), VEL(125), ECICAB(122), EXP CAB(122), 2JUNC(22), ERR  
20     DIMENSION LUJUNC(22), PA1H(122), ICAB(122), MCAB(122), ILEV(1000), ERR  
21     DIMENSION ICHECK(44)  
22     INTEGER ULTAP, ZJUNC, EHJUNC, AJJUNC, OFLG  
23     REAL IP, IKS  
24     F=F*10.  
25     WRITE (IPR,1,25)  
26     JUNEJUMPF  
27     GC TU (5,16), JUM  
28     5 WRITE (IPRN,1,30)  
29     GC TU 15  
30     10 WRITE (IPRN,1,35) THEIA  
31     15 WRITE (IPRN,1,40) L  
32     1C 20 N=1,NCAB  
33     NK=N  
34     WRITE (IPRN,1,45) NN  
35     L=IRUF (N)  
36     1C 20 M=1,1L  
37     MK=M  
38     1=TCAN (1-M,1,L)  
39     SEM (N) = ((M-1)/L)  
40     1, M=1,1L  
41     1=WF (IPRN,1,50) 1,1  
42     MF (IPRN,  
43     1, M=1,1L  
44     1=WF (IPRN,1,50) 1,1  
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482    1=WF (IPRN,1,50) 1,1  
483    MF (IPRN,  
484    1, M=1,1L  
485    1=WF (IPRN,1,50) 1,1  
486    MF (IPRN,  
487    1, M=1,1L  
488    1=WF (IPRN,1,50) 1,1  
489    MF (IPRN,  
490    1, M=1,1L  
491    1=WF (IPRN,1,50) 1,1  
492    MF (IPRN,  
493    1, M=1,1L  
494    1=WF (IPRN,1,50) 1,1  
495    MF (IPRN,  
496    1, M=1,1L  
497    1=WF (IPRN,1,50) 1,1  
498    MF (IPRN,  
499    1, M=1,1L  
500    1=WF (IPRN,1,50) 1,1  
501    MF (IPRN,  
502    1, M=1,1L  
503    1=WF (IPRN,1,50) 1,1  
504    MF (IPRN,  
505    1, M=1,1L  
506    1=WF (IPRN,1,50) 1,1  
507    MF (IPRN,  
508    1, M=1,1L  
509    1=WF (IPRN,1,50) 1,1  
510    MF (IPRN,  
511    1, M=1,1L  
512    1=WF (IPRN,1,50) 1,1  
513    MF (IPRN,  
514    1, M=1,1L  
515    1=WF (IPRN,1,50) 1,1  
516    MF (IPRN,  
517    1, M=1,1L  
518    1=WF (IPRN,1,50) 1,1  
519    MF (IPRN,  
520    1, M=1,1L  
521    1=WF (IPRN,1,50) 1,1  
522    MF (IPRN,  
523    1, M=1,1L  
524    1=WF (IPRN,1,50) 1,1  
525    MF (IPRN,  
526    1, M=1,1L  
527    1=WF (IPRN,1,50) 1,1  
528    MF (IPRN,  
529    1, M=1,1L  
530    1=WF (IPRN,1,50) 1,1  
531    MF (IPRN,  
532    1, M=1,1L  
533    1=WF (IPRN,1,50) 1,1  
534    MF (IPRN,  
535    1, M=1,1L  
536    1=WF (IPRN,1,50) 1,1  
537    MF (IPRN,  
538    1, M=1,1L  
539    1=WF (IPRN,1,50) 1,1  
540    MF (IPRN,  
541    1, M=1,1L  
542    1=WF (IPRN,1,50) 1,1  
543    MF (IPRN,  
544    1, M=1,1L  
545    1=WF (IPRN,1,50) 1,1  
546    MF (IPRN,  
547    1, M=1,1L  
548    1=WF (IPRN,1,50) 1,1  
549    MF (IPRN,  
550    1, M=1,1L  
551    1=WF (IPRN,1,50) 1,1  
552    MF (IPRN,  
553    1, M=1,1L  
554    1=WF (IPRN,1,50) 1,1  
555    MF (IPRN,  
556    1, M=1,1L  
557    1=WF (IPRN,1,50) 1,1  
558    MF (IPRN,  
559    1, M=1,1L  
560    1=WF (IPRN,1,50) 1,1  
561    MF (IPRN,  
562    1, M=1,1L  
563    1=WF (IPRN,1,50) 1,1  
564    MF (IPRN,  
565    1, M=1,1L  
566    1=WF (IPRN,1,50) 1,1  
567    MF (IPRN,  
568    1, M=1,1L  
569    1=WF (IPRN,1,50) 1,1  
570    MF (IPRN,  
571    1, M=1,1L  
572    1=WF (IPRN,1,50) 1,1  
573    MF (IPRN,  
574    1, M=1,1L  
575    1=WF (IPRN,1,50) 1,1  
576    MF (IPRN,  
577    1, M=1,1L  
578    1=WF (IPRN,1,50) 1,1  
579    MF (IPRN,  
580    1, M=1,1L  
581    1=WF (IPRN,1,50) 1,1  
582    MF (IPRN,  
583    1, M=1,1L  
584    1=WF (IPRN,1,50) 1,1  
585    MF (IPRN,  
586    1, M=1,1L  
587    1=WF (IPRN,1,50) 1,1  
588    MF (IPRN,  
589    1, M=1,1L  
590    1=WF (IPRN,1,50) 1,1  
591    MF (IPRN,  
592    1, M=1,1L  
593    1=WF (IPRN,1,50) 1,1  
594    MF (IPRN,  
595    1, M=1,1L  
596    1=WF (IPRN,1,50) 1,1  
597    MF (IPRN,  
598    1, M=1,1L  
599    1=WF (IPRN,1,50) 1,1  
600    MF (IPRN,  
601    1, M=1,1L  
602    1=WF (IPRN,1,50) 1,1  
603    MF (IPRN,  
604    1, M=1,1L  
605    1=WF (IPRN,1,50) 1,1  
606    MF (IPRN,  
607    1, M=1,1L  
608    1=WF (IPRN,1,50) 1,1  
609    MF (IPRN,  
610    1, M=1,1L  
611    1=WF (IPRN,1,50) 1,1  
612    MF (IPRN,  
613    1, M=1,1L  
614    1=WF (IPRN,1,50) 1,1  
615    MF (IPRN,  
616    1, M=1,1L  
617    1=WF (IPRN,1,50) 1,1  
618    MF (IPRN,  
619    1, M=1,1L  
620    1=WF (IPRN,1,50) 1,1  
621    MF (IPRN,  
622    1, M=1,1L  
623    1=WF (IPRN,1,50) 1,1  
624    MF (IPRN,  
625    1, M=1,1L  
626    1=WF (IPRN,1,50) 1,1  
627    MF (IPRN,  
628    1, M=1,1L  
629    1=WF (IPRN,1,50) 1,1  
630    MF (IPRN,  
631    1, M=1,1L  
632    1=WF (IPRN,1,50) 1,1  
633    MF (IPRN,  
634    1, M=1,1L  
635    1=WF (IPRN,1,50) 1,1  
636    MF (IPRN,  
637    1, M=1,1L  
638    1=WF (IPRN,1,50) 1,1  
639    MF (IPRN,  
640    1, M=1,1L  
641    1=WF (IPRN,1,50) 1,1  
642    MF (IPRN,  
643    1, M=1,1L  
644    1=WF (IPRN,1,50) 1,1  
645    MF (IPRN,  
646    1, M=1,1L  
647    1=WF (IPRN,1,50) 1,1  
648    MF (IPRN,  
649    1, M=1,1L  
650    1=WF (IPRN,1,50) 1,1  
651    MF (IPRN,  
652    1, M=1,1L  
653    1=WF (IPRN,1,50) 1,1  
654    MF (IPRN,  
655    1, M=1,1L  
656    1=WF (IPRN,1,50) 1,1  
657    MF (IPRN,  
658    1, M=1,1L  
659    1=WF (IPRN,1,50) 1,1  
660    MF (IPRN,  
661    1, M=1,1L  
662    1=WF (IPRN,1,50) 1,1  
663    MF (IPRN,  
664    1, M=1,1L  
665    1=WF (IPRN,1,50) 1,1  
666    MF (IPRN,  
667    1, M=1,1L  
668    1=WF (IPRN
```

SUBROUTINE UNKNOWN      74/74      OPT=1  
CARD NR. SEVERITY DETAILS      DIAGNOSIS OF PROBLEM

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31    1    AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

FUNCTION EXCAB 74/74 OPT=1

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```
1      *BLCK EXCAB
2      FUNCTION EXCAB (M,K)
3
4      C THIS ROUTINE CALCULATES (1 + STRAIN) AT NODE M OF CAULE K
5
6      COMMON /RJ/ VEL_X(25),VEL_Y(25)
7      COMMON /BL/ FEJUNC,IR,DELTA,IRS,TEJUNC,E,ES,FCAB,RCAB,JUMP,EXC
8      IJUNC,PJUNC,PCAB,FCAB,RCAB,TMETA,PJUNC
9      COMMON /H2/ NCAB,NOD,ERJUNC,IRJUNC,DAFH,PJUNC,CUCAB,DCAB,EXC
10     IFATE,NANC,ANJUNC,IREAD,ISPRINT,INTAPE,OUTAPE,ITIME,IFLG,NIA,THE,EXC
11     2IAS,THEIAL,CUPD,THEIAB,NJUNC,RMU,TEST,IVSEG,ZVEL,VELZ,PIPECAB,EXC
12     3EXP CAB,ZJUNC,LJUNC,CAB,IVOPT,CAB,IDEV,ICHECK,INDEV,NDATC,EXC
13     DIMENSION FEJUNC(3+44), IH(3+44), IHS(3+44), IFJUNC(3+44), PJUNC(IEXC
14     13+44)
15     DIMENSION FCAB(3+5),PJAC(3+51+22), PJJUNC(3+44), PCAB(3+51+22)EXC
16     DIMENSION PCAHO(3+51+22), RCABHO(3+51+22)EXC
17     DIMENSION NJUCE(25), ERJUNC(44), IRJUNC(44), DAI(10), DAIN(10), HEAC
18     1(22)
19     DIMENSION PJUC(3+44), DCAB(22), ANJUNC(44), TEST(14)EXC
20     DIMENSION ZVEL(25), ECICAB(22), EXP CAB(22), ZJUNC(22)EXC
21     DIMENSION LJUNC(22), PATH(22), ICAB(22), MCAB(22), IOEV(1000)EXC
22     DIMENSION ICHEC(44)
23     INTEGER PATH
24     REAL IR,IRS
25     IF (EXPCAB(K)-EV>0.) GO TO 5
26     IF (CAB(M,K)/ECICAB(K))**EXPCAB(K)
27     HETURN
28     5 EXCAB=1.
29     HETURN
30
31     END
```

SUBROUTINE INPUT      14/1+      0P1=1      F7N 4.6+433E      03/07/80      11.41.06      PAGE 1

•DECK INPUT      C

THIS ROUTINE READS ALL DATA AND IDENTIFIES ERRORS IN  
 DATA, DECK STRUCTURE, AND ARRAY REPRESENTATION      C

COMMON /H3/ VELX(25),VELY(25)  
 COMMON /H1/ FEJUNC,IH,DELT,A,IMS,IFJUNC,E,ES,FCAB,R CAB,JUMP      INP 1  
 JPJUNC,PCAB,PCABD,R CAB,THETA,PJUNC      INP 2  
 PCABD,NCA,B2/ NCA,B,NCAB,NCABD,ERJUNC,IRJUNC,DATI,DATA,M,PJUNC,DCAB,DCAB,INP 3  
 IFATE,NANC,ANJUNC,IREAD,IPNT,INTAPE,UTAPE,ITIME,IFLG,OFLG,NIR,THEINP 8  
 2IAS,THETAE,CMPD,THETAHJUNC,HU,TEST,NSSEG,ZVEL,VFLZ,PIPECICAB,INP 10  
 3EXPAT,ZJUNC,OLJUNC,PATH,ICAB,IVOPT,MCAB,IDEV,ICHECK,NEV,NDATC,INP 11  
 CC4MUN,ACVEL,VMAE(25,4),VDIR(25,4),ZPT(25,4),XP1(4),YP1(4),NPPTS(4)INP 12  
 1)INSTA  
 COMMON /VEL/ IFVEL  
 COMMON /REF/ NUCUR  
 COMMON /ANDRG/ TDCAB(1000)  
 COMMON /TITLE/ TITLE(8),PHI,CUNITS,IUNIT,VELXP(25),VELYP(25)      INP 13  
 COMMON /PL/ IPUNCH,IPACH,(ITLE(8),DEVWI      INP 14  
 COMMON /BIN/ ISCH  
 COMMON /PLT/ KPLT,SIZE,IH(3),IPOPI,KPLT      INP 15  
 COMMON /CP/ ZUP,ZUN,02,XMIN,XMAX,YMIN,YMAX,YN,ANG,NY      INP 16  
 COMMON /PIALK/ PI  
 COMMON /KITEH/ KOUNTR,NIT,MASTER,NSTEPS,ISTEP,PERCENTV,INCPRINT      INP 17  
 DIMENSION FEJUNC(3,44),IR(3,44),TRS(3,44),TFJUNC(3,44),PJUNC(1,1)INP 18  
 13\*44)  
 DIMENSION FCAB(3,51,22),HCAR(3,51,22),PJUNC(3,44),PCA8(3,51,22)INP 19  
 1) DIMENSION PCA8(3,51,22),RCABO(3,51,22),RCABU(3,51,22)      INP 20  
 36 DIMENSION HANGLE(22),EHJUNC(44),DATI(10),DATN(10),WIMP(30)INP 21  
 1(22) DIMENSION PJUNC(3,44),CUCAB(22),DCAB(22),ANJUNC(44),TEST(14)      INP 22  
 DIMENSION ZVEL(25),VEL(25),ECICAB(22),EXP CAB(22),JUNC(22)INP 23  
 DIMENSION LUNCI(22),PAIH(22),ICAH(22),WCAB(22),IUEV(1000)      INP 24  
 DIMENSION SICK(44)      INP 25  
 DIMENSION HALL(2150,10)      INP 26  
 DIMENSION ITEST(14)      INP 27  
 DIMENSION SJUER(8)      INP 28  
 EQUIVALENCE (DATI(1),FEJUNC(1))  
 EQUIVALENCE (ITEST(1),TEST(1))  
 INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG  
 INTEGER PATH  
 REAL IR,IRS      INP 29

C THIS IS THE BEGINNING OF THE INPUT SECTION  
 C INITIALE ALL CONSTANTS, FLAGS, ARRAYS, AND COUNTERS      C

IF (ITIME.EQ.0) GC TO 20      INP 30  
 ITEST(1)=4H      INP 31  
 ITEST(2)=4H ANC      INP 32  
 ITEST(3)=6MDJNC      INP 33  
 ITEST(4)=4HDCAH      INP 34  
 TEST(5)=4H CAB      INP 35  
 ITEST(6)=4H DFN      INP 36  
 ITEST(7)=4H NCUMP      INP 37  
 ITEST(8)=4H ANG      INP 38

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FIN 4.6433E

SUBROUTINE INPUT 7474 04181

FIN 4.6433E

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115 C FIRST CARD IS TITLE CARD SET DEFAULTS FOR LUN CARD

C DATA(1)=4H

C DATA(2)=4H LUN

C DATA(3)=60

C DATA(4)=61

C DATA(5)=24

C DATA(6)=0\*

C DATA(7)=0\*

C DATA(8)=0\*

C DATA(9)=0\*

C DATA(10)=0\*

C GC 10 46

130 C FIRST CARD IS LUN CARD

C JS DECODE (NU,630,TITLEM), DATA1

C {READ(DATA1,3)

C (TITLEM) .NE. 0.) READ=DATA1(7)

C READ (IREAD,620) TITLEM

C SAVE INPUT ON TAPE

C IBAD=U

C IFORM=1

C WRITE (LISCR) IFORM,BAD

C WHILE (TSCH,620) TITLEM

C 40 IPRTN=DATA1(4)\*0.1

C 45 IF (IFEO) .EQ. 0) GC 10 320

C IF (IFFO) .NE. 0) GC 10 160

C HEAD ONE INPUT RECORD INTO DATA ARRAY

C 50 CONTINUE

C IF (IFLG .EQ. 0) READ (IREAD,620) STORE

C IF (IFLG .EQ. 1) READ (IREAD,635) (DATA1,1),I=1,10) .EX. ,NSEG

C SAVE INPUT ON TAPE

C IBAD=G

C IFORM=2

C WRITE (LISCR) IFORM,BAD

C IF (IFLG .EQ. 0) WHILE (TSCH,620) STORE

C IF (IFLG .EQ. 0) DECODE (B0,630) STORE) DATA1,EX,NSEG

C TYPE AND BRANCH

C IF (IFLG .EQ. 0) GC 10 55

C IF ((DATA1(2) .EQ. TEST(12)) .OR. (DATA1(2) .EQ. 1TEST(14))) GO TO 10 55

C 66 UC 60 J=1,14

C IF (DATA1(2) .EQ. TEST(11)) GO TO (65,PS,100+105,120,130,615,615,135,1

C 159,615,155,615,325),I

C 67 CONTINUE

C GET HERE IF CARD UNIDENTIFIABLE

C INP 170

C INP 171

```

    C GET HERE IF IN CARF HEAD
    C
175   C   65 IF ((DAT1(3).NE.DAT1(4)). GO TO 70
    C   70 DAT1(3)=7
    C   70 DC 75 I=3.4
    C   70 ((DAT1(I)).LT.1).OR.((DAT1(I).GT.44.)) IRAD=8
    C   70 ((DAT1(I)).LT.0).OR.((DAT1(I).GT.44.)) GO TO 545
    C   75 CONTINUE
    C
180   C GET HERE IF DATA OK
    C COUNT IR AND STORE DATA
    C
185   C NIR.NIR=1
    C IRJUNC(INIR)=DAT1(3)
    C ERJUNC(INIR)=DAT1(4)
    C
190   C DO 80 N=1,NH
    C IF ((IRJUNC(INIR).EQ.ERJUNC(IN)) IRAD=33
    C IF ((IRJUNC(INIR).EQ.ERJUNC(IN)) GO TO 560
    C IF ((IRJUNC(INIR).EQ.IRJUNC(IN)).AND.(NIR.NE.N)) IRAD=33
    C IF ((IRJUNC(INIR).EQ.IRJUNC(IN)).AND.(NIR.NE.N)) GO TO 560
    C
195   C 80 CONTINUE
    C GO TO 500
    C
200   C GET HERE IF ANC CARD READ
    C
205   C 85 INDEX=DAT1(3)
    C IF ((DAT1(3).LT.1).OR.((DAT1(3).GT.44.)) IRAD=6
    C IF ((DAT1(3).LT.1).OR.((DAT1(3).GT.44.)) GO TO 545
    C IF ((ICHECK1(INDEX).NE.0) IBAD=30
    C IF ((ICHECK1(INDEX).NE.0) GO TO 550
    C
210   C GET HERE IF DATA OK -- COUNT ANCHOR AND STORE DATA
    C
214   C NANC=NANC+1
    C ANJUNC(NANC)=DAT1(3)
    C ICHECK1(INDEX)=1
    C
215   C 90 DO 95 I=1,3
    C 95 PJUNC(I+INDEX)=DAT1(1+3)
    C 95 GO TO 500
    C
216   C GET HERE IF DJNC CARD HEAD
    C
220   C 100 DAT1(4)=2
    C IF ((DAT1(3).LT.1).OR.((DAT1(3).GT.44.)) IRAD=23
    C IF ((DAT1(3).LT.1).OR.((DAT1(3).GT.44.)) GO TO 545
    C IF ((DAT1(3).LT.0).OR.((DAT1(3).LT.0)).IRAD=24
    C IF ((DAT1(3).LT.0).OR.((DAT1(3).LT.0)).GO TO 545
    C IF ((DAT1(7).LT.0).OR.((DAT1(7).LT.0)).INUEV=INUEV+1
    C INUEA=INUEV
    C 96 GO TO 500
    C
225   C GET HERE IF UCAB CARD READ
    C

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```

C 105 DC 110 1=12          INP 229
230      1D=DAI(4)          INP 230
      IF (1D.EW.0.) GO TO 115  INP 231
115      CONTINUE           INP 232
      IBAO=18               INP 233
      INDEX=INDEX+1         INP 234
      INDEX=INDEX
      IF ((INDEX.LT.1.) OR. (INDEX.GT.1000)) IBAU=19  INP 235
      IF ((DAI(1)(3).LT.1.) OR. (DAI(1)(3).GT.22.)) IBAU=17  INP 236
      IF ((DAI(1)(3).LT.1.) OR. (DAI(1)(3).GT.22.)) GO TO 545  INP 237
      INDEX=INDEX+1         INP 238
      INDEX=INDEX
      IF ((INDEX.LT.1.) OR. (INDEX.GT.1000)) IBAU=19  INP 239
      IF ((DAI(1)(7).LT.0.) OR. (DAI(1)(8).LT.0.)) IBAU=22  INP 240
      IF ((DAI(1)(7).LT.0.) OR. (DAI(1)(8).LT.0.)) GO TO 545  INP 241
      IF ((DAI(1)(7).LT.0.) OR. (DAI(1)(8).LT.0.)) GO TO 545  INP 242
      IF ((DAI(1)(4).EQ.2.) AND. (DAI(1)(9).NE.0.)) IBAU=21  INP 243
      IF ((DAI(1)(4).EQ.2.) AND. (DAI(1)(9).NE.0.)) GO TO 545  INP 244
      IF ((DAI(1)(4).EQ.2.) AND. (DAI(1)(9).NE.0.)) GO TO 545  INP 245
      IF ((DAI(1)(4).EQ.1.) AND. (DAI(1)(9).LE.0.)) IBAU=20  INP 246
      IF ((DAI(1)(4).EQ.1.) AND. (DAI(1)(9).LE.0.)) GO TO 545  INP 247
      IF ((DAI(1)(4).EQ.1.) AND. (DAI(1)(9).LE.0.)) GO TO 545  INP 248
      IF ((DAI(1)(10).LT.0.) IBAU=22  INP 249
      IF ((DAI(1)(10).LT.0.) IBAU=22  INP 250
      IF ((DAI(1)(10).LT.0.) GO TO 545  INP 251
      TDCAB(INDEX)=EX
      GC TO 540               INP 252
C     GET HERE IF CAB CARD READ
C     INDEX=DAI(1)(3)
C     120 INDEX=DAI(1)(3)
      IF (1FLG.EW.0.) READ (IREAD,620) STORE
      IF (1FLG.EQ.1) READ (IREAD,645) TDCAH(INDEX)
C     SAVE INPUT ON TAPE
C     C
      IBAU#U
      IFORM=3
      WRITE (ISCH,1F0K) IBAU
      IF (IFLAG.EC.0) WRITE (ISCP,620) STORE
      IF ((IFLAG.EW.0) DECINE (10,640,STORE) TDCAB(INDEX))
      DECODE (10,640,STORE) TDCAB(INDEX)
      IF ((DAI(1)(3).LT.1.) OR. (DAI(1)(3).GT.22.)) IBAU=9
      IF ((DAI(1)(3).LT.1.) OR. (DAI(1)(3).GT.22.)) GO TO 545
      IF ((DAI(1)(4).EQ.DATI(5)) IBAU=10
      IF ((DAI(1)(4).EQ.DATI(5)) GO TO 545
      IF ((DAI(1)(4).EQ.DATI(5)) CM. (DAI(1)(5).GT.44.)) IBAU=11
      IF ((DAI(1)(4).GT.44.) CR. (DAI(1)(5).GT.44.)) IBAU=11
      IF ((DAI(1)(4).LT.1.) OH. (DAI(1)(5).LT.1.)) 16AD=11
      IF ((DAI(1)(4).LT.1.) OH. (DAI(1)(5).LT.1.)) GO TO 545
      IF ((DAI(1)(7).LE.0.) OH. (DAI(1)(8).LE.0.)) OH. (DAI(1)(9).LE.0.)) IBAU=121
      IF ((DAI(1)(7).LE.0.) OH. (DAI(1)(8).LE.0.)) OH. (DAI(1)(9).LE.0.)) GO TO 51N
      IF ((DAI(1)(7).LE.0.) OH. (DAI(1)(8).LE.0.)) OH. (DAI(1)(9).LE.0.)) GO TO 51N
      IF ((EX.LT.0.) OH. (DAI(1)(10).LT.0.)) IBAU=13
      IF ((EX.LT.0.) OH. (DAI(1)(10).LT.0.)) GO TO 545
      IF ((DAI(1)(9).EQ.0.) AND. (EX.NE.0.)) IBAU=14
      IF ((DAI(1)(9).EQ.0.) AND. (EX.NE.0.)) GO TO 545
      IF ((DAI(1)(10).NE.0.) AND. (EX.EQ.0.)) IBAU=15
      IF ((DAI(1)(10).NE.0.) AND. (EX.EQ.0.)) GO TO 545
      IF ((INSEG.LT.1.) OR. (INSEG.GT.50)) IBAU=16
      IF ((INSEG.LT.1.) OR. (INSEG.GT.50)) GO TO 545
      280
      275
      285
  
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## SUBROUTINE INPUT

74/74 OPT=1

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      IF ((ICAB(INDEX).NE.0) GO TO 555
      ICAB(INDEX)=1
      INDEX=DATA(5)
      IF ((CHECK(INDEX).NE.0) IBAD=31
      IF ((CHECK(INDEX).NE.0) GO TO 550
      ICHECK(INDEX)=1
      GET HERE IF DATA CK
      C
      C INDEX=DATA(3)
      ZJUNC(LINDEX)=DATA(4)
      LJUNC(INDEX)=DATA(5)
      125 NODE((INDEX))=SEG+1
      *CAB(INDEX)=DATA(6)
      CDCAB(INDEX)=DATA(7)
      DCAB(INDEX)=DATA(8)
      H(INDEX)=DATA(9)/SEG
      ECICAB(INDEX)=DATA(10)
      EXP CAB(INDEX)=EX
      GC TO 500
      C
      C GET HERE IF UEN CARD READ
      C
      130 IF ((DATA(13).LE.0*) IBAD=25
      IF ((DATA(13).LE.0*) GO TO 545
      IF (FH=0*)+1
      IF (FH=0*.G1*.1) IBAD=36
      IF (FH=G1*.1) GO TO 565
      FH=DATA(13)
      GC TO 50
      C
      C GET HERE IF EOD CARD READ
      C
      135 IF EOF=1 FEGU+1
      UC 140 J=1,10
      140 DATA((INDO,J)=DATA(J)
      INDO=10
      IF ((ATE.NE.0*) GC TO 450
      IF (TPLF.EQ.1) GO 10 145
      GC TO 335
      145 IF READ=1 SAV1
      IF LG=0
      GC TO 335
      C
      C GET HERE IF NNC CARD READ
      C
      150 IF ((DATA(3).LT.2*.0*.0*.DATA(3)*.67*.44*)) IHAD=5
      IF ((DATA(3).LT.2*.0*.0*.DATA(3)*.67*.44*)) GO TO 545
      IF (JNC=IF JNC+1
      IF (IF JNC.G1*.1) IBAD=25
      IF (IF JNC.G1*.1) GO TO 565
      NNC=DATA(3)
      GC TO 50
      C
      C GET HERE IF NCAT CARD READ
      C
      155 NCATC=NCATC+1

```

SUBROUTINE INPUT 74/74 OPT=1

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FIN 4.6.433E

C DEFINE CURRENT UNITS OPTION AND CONVERSION FACTOR

INP 343

345 C UNIT=DAT(1)(1)+1.E-9

INP 344

CUNITS=1

INP 345

IF (IUNIT.EQ.1) CUNITS=0.01943

INP 346

IF (IUNIT.EQ.2) CUNITS=0.5921

INP 347

DEVMEDAT(1)(8)

INP 348

NSTEPS=1

INP 349

ISTEP=1

INP 350

PERCENT=0.

INP 351

INCPLNT=0

INP 352

IF (EX.NE.0.0) NSTEPS=EX

INP 353

IF (FLDA(INSTEPS).NE.0.0.AND.NSTEPS.GT.1) INCPLNT=1

INP 354

IF (DAT(1)(1).NE.0.0) IFUNCT=8H

INP 355

NCCUR=DAT(1)(5)

INP 356

HEAD(LHEAD,620) TITLE

INP 357

SAVE INPUT ON TAPE

INP 358

C IBAD=0

INP 359

IFORMM=1

INP 360

WRITE (15CH) IFOV,IBAU

INP 361

\*WRITE (15CH,020) TITLE

INP 362

IF (IWAU.EQ.0) GO TO 615

INP 363

READ ANGLE IN DEGREES BETWEEN MAGNETIC NORTH AXIS AND X-AXIS OF

INP 364

ARRAY REFERENCED COORDINATE SYSTEM. ANGLE IS POSITIVE CLOCKWISE

INP 365

AND IS REFERENCED WITH RESPECT TO THE MAGNETIC NORTH AXIS.

INP 366

C PHI=DAT(1)(6)

INP 367

6C 10 45

INP 368

IFCMM=0

INP 369

INDAT=C

INP 370

IFVEL=0

INP 371

IFANG=C

INP 372

IF ((DAT(1)(3).LT.0.0).OR.(DAT(1)(3).GT.3.)) IBAD=26

INP 373

IF ((DAT(1)(3).LT.0.0).OR.(DAT(1)(3).GT.3.)) GO TO 545

INP 374

IVUPDUA(1)(3)

INP 375

IF (IVOPT.EQ.1) NSIA=DAU(4)

INP 376

IF (INDAT.EQ.1) GC 10 165

INP 381

IF (IVOPT.EC.0) GC 10 180

INP 382

IF (KFLG.EQ.0) GO TO 170

INP 383

IF (IVOPT.EC.KCUR) GO TO 180

INP 384

GC 10 610

INP 385

165 IF (IVOPT.EC.0) GO 10 175

INP 386

170 KFLG=1

INP 387

KCUR=IVOPT

INP 388

UC 10 180

INP 389

175 KFLG=0

INP 390

C READ ONE INPUT RECORD FROM PARAMETRIC STUDY SOURCE DECK

INP 391

IF (FOF(LHEAD,620)) 185,190

INP 392

185 CALL MAIN

INP 393

190 STOP

INP 394

195,196

INP 395

SUBROUTINE INPUT

74/14 OPT=1

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PAGE

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400 C SAVE INPUT ON TAPE  
C  
C 190 1BAUEJ  
IF(IHM=2  
WHITE((I\$CH)) IF(OR,IBAD  
WHITE((I\$CH,62)) STORE  
DECONE((I\$0,630,SI\$HE)) DATN,EXX>NNSEG  
UC 195 I=1,I4  
IF(DATN(2)\*EC,TEST(1)) GO TO (615,255,255,255,615,230,225,315)  
IF(DATN(2)\*EG,4MCPL) GO TO 235  
IF(DATN(2)\*EG,4HPLT) GO TO 245  
195 CONTINUE  
CALL SWITCH  
GO TO 540  
C  
C GET HERE IF VEL CALL READ  
C 200 IF VEL=IFVEL+1  
IF((IVOP1\*EG\*3)) CALL REDVEL (IREAD,IPHNL)  
CALL SW1C  
IF((IVOP1\*EG\*3)) GC TO 1H0  
IF((IVOP1\*EG\*0)) GC TO 615  
IF((IVOP1\*NL\*1)) GC TO 210  
NVSEG=0  
DC 205 I=1,25  
VEL(1)=0.  
205 VEL(1)=6.  
210 NVSEG=NVSEG+1  
IF((NVSEG\*61\*25)) IBAD=3H  
IF((NVSEG\*61\*25)) GO TO 565  
ZVFL(NVSEG)=DAT1(3)  
UC 215 K#1 NVSEG  
IF((ZVEL(NVSEG).EQ.ZVEL(K)).AND.(K.NE.NVSEG)) IBAD=39  
IF((ZVEL(NVSEG).EQ.ZVEL(K)).AND.(K.NE.NVSEG)) GO TO 565  
215 CONTINUE  
IF((IVOP1\*EG\*2)) GC TO 220  
VEL(NVSEG)=DAT1(4)  
GO TO 180  
220 VELX(NVSEG)=DAT1(5)  
VELY(NVSEG)=DAT1(5)  
GO TO 180  
C  
C GET HERE IF AND CAND RTAU  
C 225 IF(AN=IFAN)+1  
CALL SWITCH  
IF((IVOP1\*EG\*0)) GO TO 615  
IF((IFAN=IFAN+1)) HANG=0  
IF((DAT1(4)\*L\*0\*)) IMAH=28  
IF((DAT1(4)\*L\*0\*)) GO TO 545  
IF((DAT1(5)\*L\*0\*)) DAT1(3) IMAU=29  
IF((DAT1(5)\*L\*0\*)) DAT1(3) IMAU=29  
THETAH=DAT1(3)  
THETAS=DAT1(4)  
THETAE=DAT1(5)

SUBROUTINE INPUT 74/74 OPT=1

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119  
HANG=HANG+1  
IF (HANG.GT.1) IBAU=40  
IF (HANG.GT.1) GU(0,505  
GO TO 180  
C  
C GET HERE IF LCMP CARD READ  
C  
230 IF(COMP=IFCOMP+1  
CALL SWITCH  
IF (IFCOMP.EQ.1) NCOMP=0  
IF (DATI(3).LE.0.) IBAD=27  
IF (DATI(3).LE.0.) GU TU 545  
NCOMP=NCOMP+1  
IF (INCOMP.GT.1) IBAD=37  
IF (INCOMP.GT.1) GU TU 565  
N1=200  
IF (DATI(4).NE.0.0) N1=DATI(4)  
MAXIEH=1000  
IF (DATI(5).NE.0.0) MAXIEH=DATI(5)  
GO TO 180  
C  
C GET HERE TO PLUT VELOCITY FIELD  
C  
235 IF (KPLI.EQ.0) CALL PLOTS(0,0,6LNPFIL)  
KPLI=1  
KCHLIA=1  
CALL SWITCH  
ZUP=DATI(3)  
ZDN=DATI(4)  
DZ=DATI(5)  
Y1=DATI(6)  
X1N=DATI(17)  
XMAX=DATI(18)  
YMIN=DATI(19)  
YMAX=DATI(20)  
ANG=EXX  
IF (ANG.LE.C\*0.0R.ANG.GE.180.) ANG=90.  
NY=MSEG  
IF (NY.LE.0) NY=6  
C  
C FIND MAX AND MIN FOR DEFAULT  
C  
500 DEFAULT=XMIN+YMIN+XMAX+YMAX  
IF (DEFAULT.NE.0.) GO TO 180  
C  
C  
505 YMAX=RIG  
DC 240 ISF=1,ISAC  
ISAF=ANJU(C1,ISF)  
> XMIN=XMIN(XMIN,PJUJC(1+1SA))  
> XMAX=XMAX(XMAX,PJUJC(2+1SA))  
241 YMAX=AMAX(XMAX,PJUJC(2+1SA))  
HY=AMIN(XMAX-XMIN)

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515 PY=AHS(YMAX-YMIN)  
IF (RY.EQ.0.) YMIN=YMIN-0.15\*RY  
IF (RY.EQ.0.) YMAX=YMAX-0.15\*RY  
IF (RX.EQ.0.) XMIN=XMIN-0.15\*RY  
IF (RX.EQ.0.) XMAX=XMAX+0.15\*RY  
GC TO 180

C GET HERE FOR PERSPECTIVE PLOTTING  
C 245 CALL SWITCH  
IPOPT=DAT1(3)+01  
SIZE=DAT1(4)  
IH(1)=DAT1(5)  
IH(2)=DAT1(6)  
IH(3)=DAT1(7)  
DEFAULT=IH(1)+TH(2)\*TH(3)  
IF (DEFAULT.NE.0.0) GC TO 250  
TH(1)=30.  
TH(2)=120.  
TH(3)=90.

250 IF (KPL1.EQ.0) CALL PLOTS (0,0,6LNFILE)  
KPL1=1  
GC TO 180

C SET HERE IF PARAMETERS ARE BEING CHANGED  
C EXECUTE RECORD TO BE CHANGED AND BRANCH  
C 255 IF (INDAT1.NE.0) GC TO 260  
READ (INFILE,660) (DAT1(I,J),I=1,10),J=1,IRMAX  
REWIND INFILE

120 540  
545 IRATE1  
260 IRATE2  
0.265 I=1,IRMAX  
IROW=1  
IF ((DATIN1).EQ.DAT1(IROW,1)).AND.(DATN(2).EQ.DAT1(IROW,2)) GO  
110 270  
IF (DAT1(IROW,2).EQ.1E51) 191 GO TO 605  
265 CONTINUE  
270 J=1,10  
275 DAT1(J)=DAT1(IROW,J)

120 550  
280 J=1,10  
IF (DAT(2).EQ.TEST(1)) GO TO 285+290+295+305), 1  
280 CONTINUE

C GET HERE IF ANC CARL READ  
C 285 IF (DAT(3).NE.DATN(3)) GO TO 605  
CALL SWITCH  
INUT=DAT1(3)  
GO TO 90

560  
565 C GET HERE IF DUNC CARL READ  
C 290 IF (DAT(3).NE.DATN(3)) GO TO 605  
CALL SWITCH  
DAT1(4)=2  
IF ((DAT1(7).LT.0.).OR.((DAT1(8).LT.0.)) INAU=24

570

SUBROUTINE INPUT      74/74    OPT=1

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      IF ((DAT1(7).LT.0.) .OR. (DAT1(8).LT.0.)) GO TO 545  
      GC TO 500

      C     GET HERE IF ICAB CARD READ

      575    C     245 IF ((DAT1(3).NE.DAT1(3)) GO TO 695  
         1BDA(B1KU)=1XX  
         IF (((DAT1(4).EQ.1.) .OR. (DAT1(4).EQ.2.)) .AND. ((DAT1(4).EQ.1.) .OR. (DAT1(4).EQ.2.)) GO TO 300  
         GC TO 605

      580    C     305 CALL SWITCH  
         IF ((DAT1(4).LT.0.2.) .AND. (DAT1(9).NE.0.)) IHAD=21  
         IF ((DAT1(4).EQ.2.) .AND. (DAT1(9).NE.0.)) GO TO 545  
         IF ((DAT1(7).LT.0.) .OR. (DAT1(8).LT.0.)) IBAD=22  
         IF ((DAT1(7).LT.0.1.) .OR. (DAT1(8).LT.0.1.)) IBAD=22  
         IF ((DAT1(7).LT.0.2.) .OR. (DAT1(8).LT.0.2.)) GO TO 545  
         IF ((DAT1(4).EQ.1.) .AND. (DAT1(9).LE.0.)) IHAD=20  
         IF ((DAT1(4).EQ.1.) .AND. (DAT1(9).LE.0.)) IHAD=20  
         IF ((DAT1(4).EQ.1.) .AND. (DAT1(9).LE.0.)) GO TO 545  
         IF ((DAT1(4).LT.0.) .LT.0.) IBAC=20  
         IF ((DAT1(10).LT.0.)) GO TO 545  
         GC TO 500

      590    C     581 HERE IF CAB CARD READ  
      310    C     310 I=3+5  
      595    C     IF ((DAT1(1).NE.DATN(1)) GO TO 605  
         310 CONTINUE  
         CALL SWITCH  
         EX=EXX  
         INSEG=MSEG  
         IAD=EXDAT(3)  
         HEAD (IREAD+620) STOP

      600    C     SAVE INPUT IN TAPE  
      605    C     1BAA=0  
         IFORM=3  
         WHITE (ISCH) IFOHM IBAD  
         WRITE (ISCH+620) \$10E  
         DECWE (10,6,0,SICK) IFCAN(INDEX)  
         IF ((DAT1(7).LE.0.) .OR. (DAT1(8).LE.0.)) OH. (DAT1(9).LE.0.) IAD=121  
         IF ((DAT1(7).LE.0.) .OR. (DAT1(8).LE.0.)) OH. (DAT1(9).LE.0.) GO TO 511  
         145    C     ((EX+L1+0.) .OR. (DAT1(10).LT.0.)) IHAD=13  
         IF ((DAT1(11).LT.0.) .OR. (DAT1(12).LT.0.)) GO TO 545  
         IF ((DAT1(11).LT.0.) .OR. (DAT1(12).LT.0.)) IHAD=14  
         IF ((DAT1(10).LT.0.) .OR. (DAT1(11).LT.0.)) ANL (FX,NE,0.) GO TO 545  
         IF ((DAT1(10).LT.0.) .OR. (DAT1(11).LT.0.)) AND (FX,NE,0.) IHAD=15  
         IF ((INSEG+1).LT.0.) OH. INSEG=0  
         IF ((INSEG+1).LT.0.) OH. INSEG=10  
         IF ((INSEG+1).LT.0.) OH. INSEG=501  
         IF ((INSEG+1).LT.501) GO TO 545  
         GO TO 125

      615    C     615 HERE IF F1(F1)+1  
         IF ((F1(F1)+1).NE.0.) GC TO 45.  
         IF ((F1(F1)+1).NE.0.) GC TO 45.  
         C     615 HERE IF F1(F1)+1  
         IF ((F1(F1)+1).NE.0.) GC TO 45.  
         C     615 HERE IF F1(F1)+1  
         IF ((F1(F1)+1).NE.0.) GC TO 45.  
         C     615 HERE IF F1(F1)+1  
         IF ((F1(F1)+1).NE.0.) GC TO 45.

## SUBROUTINE INPUT

PRINT 4,6\*433F

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```

C GET HERE IF LUN CARD READ           INP 626
C
630   C 320 INTAPE=DATI(5)           INP 629
      C 1FLG=DATI(6)           INP 630
      C ((1FLG.L.0).OR.(1FLG.GT.1)) 1BAD=2   INP 631
      C ((1FLG.L.0).OR.(1FLG.GT.1)) 60 TO 545   INP 632
      C ISAV=DATI(3)           INP 633
      C IF ((1FLG.EU.0) .INREAD=DATI(3)   INP 634
      C IF ((1FLG.EU.0) .INREAD=DATI(7)   INP 635
      C OFLG=DATI(4)
      C IF ((OFLG.L.0) .OR. (OFLG.GT.2)) 1BAD=3   INP 636
      C IF ((OFLG.L.0) .OR. (OFLG.GT.2)) 60 TO 545   INP 637
      C IF ((OFLG.EU.0) .OUTAPE=DATI(4)   INP 638
      C IF ((OFLG.NE.0) .OUTAPE=DATI(9)   INP 639
      C IF ((IPRINT.EU.IREAD) .OR. (IPRINT.EQ.IREAD)) .OR. ((IPRINT.EQ.OUTAPE) .OR. ((IREAINP 640
      C INTAPE.QUITAPE) .OR. ((INTAPE.EQ.IREAD) .OR. ((IREAINP 641
      C 2D.EQ.QUITAPE) .OR. ((IFLG.EQ.1).AND.((IREAD.EQ.ISAV))) 1BAD=4   INP 642
      C IF ((IPRINT.EU.IREAD) .OR. (IPRINT.EQ.INTAPE) .OR. ((IREAINP 643
      C INTAPE.QUITAPE) .OR. ((INTAPE.EQ.IREAD) .OR. ((IREAINP 644
      C 2D.EQ.QUITAPE) .OR. ((INTAPE.EQ.OUTAPE) .OR. ((IREAINP 645
      C 2D.EQ.QUITAPE) .OR. ((IPRINT.EU.IREAD) .OR. ((IPRINT.EQ.0) .AND. ((IREAINP 646
      C INTAPE.QUITAPE) .OR. ((INTAPE.EQ.IREAD) .OR. ((IREAINP 647
      C 2D.EQ.QUITAPE) .OR. ((INTAPE.EQ.OUTAPE) .OR. ((IREAINP 648
      C 2D.EQ.QUITAPE) .OR. ((IPRINT.EU.1).AND.((IREAD.EQ.ISAV))) GO TO 545   INP 649
      C 2D.EQ.QUITAPE) .OR. ((IPRINT.EU.1).AND.((IREAD.EQ.ISAV))) GO TO 545   INP 650
      C
      C GET HERE FOR EOP
      C
640   C 325 IF (FATE.NE.0) CALL BADATA   INP 651
      C IF (OFLG.EU.0) GO TO 330   INP 652
      C WRITE (OUTAPE,650) TEST(16)   INP 653
      C IF (FATE.EU.0) WRITE (IPRN,1655)   INP 654
      C IF (KPLT.NE.0) CALL PLOT (1•1•999)   INP 655
      C FATE=1.   INP 656
      C RETURN   INP 657
      C
645   C CHECK TO SEE IF SUSPENDED ARRAY SOURCE DECK COMPLETE   INP 658
      C
      C 335 IF ((IFINC.EU.0) .OR. ((FFHU,LQ.0) .OR. (INAC,EQ.0)) GO TO 570   INP 659
      C 60 TO 395   INP 660
      C
655   C CHECK TO SEE IF PARAMETRIC STUDY SOURCE DECK COMPLETE   INP 661
      C
      C 340 IF ((IVOPT.EU.0) .OR. ((IVUP1,LQ.3)) GO TO 390   INP 662
      C N2L$N
      C IF ((IVSEG.EC.0) 1BAD=54   INP 663
      C IF ((IVSEG.EC.0) UC TO 575   INP 664
      C IF ((IVEL.EC.0) UC TO 370   INP 665
      C IF ((IVOPT.EC.2) GO TO 355   INP 666
      C
660   C SCR7 VELOCITY PROFILE HY Z-COORDINATE   INP 667
      C
      C 345 I=1,AVSEG   INP 668
      K=1
      C 345 J=K,AVSEG   INP 669
      C IF ((ZVCL(1),LE.ZVFL(J)) ,0 TO 345   INP 670
      C IF ((ZVEL(1)=ZVEL(1))   INP 671
      C ZVEL(1)=ZVEL(1)   INP 672
      C ZVEL(1)=ZVEL(1)   INP 673
      C TEMP=ZVEL(1)   INP 674
      C
670   C
680   C
685   C

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## SUBROUTINE INPUT

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685      VELZ(I)=VELZ(J)
          VELZ(J)=VELZ(I)
          345  CCONTINUE
          C   UNITS CONVERSION
          C
          C   DO 350 I=1,INVSEG
          VELXP(I)=VELZ(I)
          VELYP(I)=0
          VELZ(I)=VELZ(I)*CUNITS
          VELX(I)=VELZ(I)
          350  VELY(I)=0.
          GO TO 370
          C   SORT VELOCITY FOR CURRENT OPTION 2
          C
          C   355  DO 360 I=1,INVSEG
          K=1
          DO 360 J=K,INVSEG
          IF (ZVEL(I).LE.ZVEL(J)) GO TO 360
          ZVEL(I)=ZVEL(J)
          ZVEL(J)=ZVEL(I)
          IEMP=ZVEL(I)
          IVMF=ZVEL(J)
          TVX=VELX(I)
          TVY=VELY(I)
          VELX(I)=VELX(J)
          VELY(I)=VELY(J)
          VELX(J)=TVX
          VELY(J)=TVY
          360  CCONTINUE
          C   UNITS CONVERSION
          C
          C   DO 365 I=1,INVSEG
          VELXP(I)=VELX(I)
          VELYP(I)=VELY(I)
          AMAG=VELX(I)
          DIR=360.-VELY(I)*PHI
          VELX(I)=COS(DIR*PI)*AMAG*CUNITS
          VELY(I)=SIN(DIR*PI)*AMAG*CUNITS
          365  INDEX=ANJUNC(1)
          ANCH=PJUNC(3,INDEX)
          IF (NANC.EQ.1) GO TO 380
          DC 375  N=NANC
          INDEX=ANJUNC(N)
          IF (PJUNC(3,INDEX).LT.ZANCH) ZANCH=PJUNC(3,INDEX)
          375  CCONTINUE
          380  IF ((VOPT.EQ.1) .AND. (VEL(I).EQ.0)) IHAO=54
          IF ((VZL.EQ.0).OR.(VANG.EQ.0)) GO TO 575
          IF ((VCP.EQ.0).OR.(VAD=53))
          IF ((VCP.EQ.0)) GC 10 575
          IF ((VCA1.EQ.0)) GC 10 415
          RETURN
          INP 685
          INP 686
          INP 687
          INP 688
          INP 689
          INP 690
          INP 691
          INP 692
          INP 693
          INP 694
          INP 695
          INP 696
          INP 697
          INP 698
          INP 699
          INP 700
          INP 701
          INP 702
          INP 703
          INP 704
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          INP 710
          INP 711
          INP 712
          INP 713
          INP 714
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          INP 720
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          INP 723
          INP 724
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          INP 726
          INP 727
          INP 728
          INP 729
          INP 730
          INP 731
          INP 732
          INP 733
          INP 734
          INP 735
          INP 736
          INP 737
          INP 738
          INP 739
          INP 740
          INP 741

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SUBROUTINE INPUT — 7474 OPT=1

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C CHECK ON CONTINUITY OF CABLE NUMBERING AND COUNT CABLES  
C  
C 395 NCAB=ICAB(22)  
UC 400 N=1,21  
NCAB=NCAB+ICAB(N)  
J=1 CAB(N)-ICAB(N+1)  
IF (J.L1.G) GO TO 580  
400 CONTINUE  
IF (INCAB.EQ.0) GO TO 580  
C  
C CHECK ON CONTINUITY OF JUNCTION NUMBERING AND COUNT JUNCTIONS  
C  
C NJUNC=ICHECK(44)  
UC 405 N=1,43  
NJUNC=NJUNC+ICHECK(N)  
JEICHECK(N)-ICHECK(N+1)  
IF (J.L1.G) GO TO 585  
405 CONTINUE  
C  
C SORT DEVICES ON CABLE NO. (DATI(3))  
AND DISTANCE FROM 0 JUNCTION (DATI(10))  
C  
C NDEV=INDEV  
CALL SORT (INDEV,INTAPE)  
IF (FATE.EQ.0.) GO 10 410  
GC TO 530  
C  
C GET MIRE IF ARRAY NUMBERED CORRECTLY  
C  
C 410 NIRC=NCAB+NANC-NOJUNC  
IF (NIR.NE.NIRC) GO TO 590  
C  
C GET HERE TO MAKE FINAL CHECK ON INTAPE  
C  
C 415 I=1  
420 DO 425 J=1,10  
425 DATI(J)=DATI(11,J)  
I=I+1  
IF (DATI(2).EQ.TEST(1)) GO TO 430  
IF (DATI(2).EQ.TEST(3)) GO TO 435  
IF (DATI(2).EQ.TEST(4)) GO TO 440  
IF (DATI(2).EQ.TEST(5)) GO TO 445  
IF (DATI(2).EQ.TEST(9)) GO TO 450  
GO TO 420  
C  
C GET HERE FOR IR  
C  
C 430 IN1=DATI(3)  
IN2=DATI(4)  
IF (IN1.LE.NOJUNC) BAU=43  
IF (IN1.LE.NOJUNC) GO TO 505  
IF (IN2.GT.NOJUNC) BAU=46  
IF (IN2.GT.NOJUNC) GO TO 545  
IF (IN1.GT.NOJUNC) BAU=47  
IF (IN1.GT.NOJUNC) GO TO 595  
INP 742  
INP 743  
INP 744  
INP 745  
INP 746  
INP 747  
INP 748  
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INP 797  
INP 798

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800      C   GO TO 420
C   GET HERE FOR CJNC
C   435  ID=DATI(3)
        IF (IU.GT.NJUNC) IBAD=51
        IF (IU.GT.NJUNC) GO TO 545
        GO TO 420
C   GET HERE FOR UCAB
C   440  ID=DATI(4)
        IF (IU.GT.NCAB) IBAD=49
        IF (IU.GT.NCAR) GC 10 595
        PL=M(IID)*(NAODE(IC)-1)
        IF (DATI(IID).GE.PL) IBAD=50
        IF (DATI(IID).GE.RL) GC 10 595
        GO TO 420
C   GET HERE FOR CAB
C   445  ID=DATI(4)
        IF (IU.GT.NJUNC) IBAD=48
        IF (IU.GT.NJUNC) GO 10 595
        GO TO 420
C   GET HERE FOR EOD
C   450  WRITE (NINTAPE,660) ((DATI((I,J),J=1,10),I=1,6MAX)
        REWIND INTAPE
        IF (NJNC.NE.0.AND.FATE.EQ.0.) RETURN
        IF (FATE.EQ.0.) GO 10 455
        GO TO 50
C   GET HERE IF ALL OK AND CALCULATE PATH
C   K IS CABLE COUNTER
835      C   455  K=0
C   LOOP=1 LOOKING FOR CABLES LEAVING ANCHORS
C   JMAX REMEMBERS FIRST VALUE OF K ON A LEVEL OF TREE
C   JMAX=1
840      C   MAX MEMBERS NUMBER OF LINES ON A LEVEL OF ICPGRAPHIC TREE
C   JMAX
        IF (LCIP.EQ.1) GO TO 455
        IF (JMAX.EQ.1).AND.(K.NE.1) GO TO 660
        IF (LCIP.EQ.2).AND.(JMAX.EQ.1) GO 10 660
        IF (LCIP.EQ.2)
        LCIP=2
        JMAX=JMAX+1
850

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SUBROUTINE INPUT

74/74 OPT=1

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FIN 4.6433F

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1C 495 J=JMIN,JMAX          INP 656
C LOOKING FOR CABLES LEAVING A JUNCTION          INP 657
C                                               INP 658
C                                               INP 659
C                                               INP 660
C                                               INP 661
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C                                               INP 911
C                                               INP 912
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SUBROUTINE INPUT

IFORM

IBAD

PAGE

17

DATE

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555 IER=3  
IBAU=32  
UC TU 530  
IER=4  
GC TU 534  
565 IER=6  
GC TU 530  
570 IER=7  
FA1=1  
IFORM=5  
IBAU=41  
WHITE (ISCR) IFORM IBAD  
WHITE (ISCR) IFJNC, IFHO, NANC  
GC TU 535  
575 IER=14  
FATE=1  
IFORM=6  
WHITE (ISCR) IFORM IBAD  
WHITE (ISCR) ACUMP, IVOP1, NVSEG, NZL, NANG  
GC TU 535  
580 IER=8  
FATE=1  
IBAU=42  
IFORM=7  
WHITE (ISCR) IFORM IBAD  
WHITE (ISCR) ICAB(I), I=1\*22  
GC TU 535  
585 IER=9  
FATE=1  
IBAU=43  
IFORM=8  
WHITE (ISCR) IFORM IBAD  
WHITE (ISCR) IHECK(I), I=1\*44  
GC TU 535  
590 IER=11  
FATE=1  
IBAU=44  
IFORM=9  
WHITE (ISCR) IFORM IBAD  
WHITE (ISCR) ACAB,NANC,NIJINC,NIRC,NIM  
GC TU 535  
595 IFR=12  
GC TU 530  
600 IER=13  
FATE=1  
IBAU=52  
GC TU 530  
605 DATA(1)=DATA(1)  
DATA(2)=DATA(2)  
010 IER=15  
IBAU=55  
GC TU 530  
615 IER=16  
BAU=56  
DATA(1)=DATA(1)  
DATA(2)=DATA(2)

SHROUTINE INPUT 74/74 OPT=1

FIN 4.6.435

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```
970      60 10 530          INP 970
          C   620 FORMAT (HALG)    INP 971
          C   625 FORMAT (A5,A3)    INP 972
          C   630 FORMAT (F4.0,A4,BF8.0,F5.0)  INP 973
          C   635 FORMAT (F4.0,A4,AE15.8,/E12.5,I3) INP 974
          C   640 FORMAT (I14F5.0)    INP 975
          C   645 FORMAT (B8E5.0)    INP 976
          C   650 FORMAT (1H4.14*3E15.8)  INP 977
          C   655 FORMAT (1H1.18HANALYSIS COMPLETED) INP 978
          C   660 FORMAT (F4.0,A4,AE15.8)  INP 979
          C   665 FORMAT (8X,2H17,18X*45HCOMMON/BL/ BOUND EXCEEDED. SEE USERS MANUAL INP 980
          C           1L0)          INP 981
          C           END          INP 982
                                INP 983-

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CARD NR. SEVERITY DETAILS - DIAGNOSIS OF PROBLEM

861 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
872 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

SUBROUTINE PRSOUT      74/74      UPT=1

FIN 4.6433E      03/07/80      11.41.06      PAGE 1

•UECK PRSOUT  
SUBROUTINE PRSOUT

C THIS ROUTINE GENERATES INFORMATION CONCERNING THE PHYSICAL  
C CHARACTERISTICS OF THE STRUCTURAL CABLE ARRAY.  
C  
COMMON /B2/ VEL(25),VELY(25)  
COMMON /H1/ FT,JUNC,IR,DELT,IAS,TJ,JUNC,F,ES,FCAB,HCAB,JUMP,PHS  
IJUNC,PCAB,PCAH,RCAB,THETA,TJUNCO  
COMMON /B2/ NCAB,ANODE,ERJUNC,IJUNC,DAIL,DATN,PJUNC,CUCAB,DCAB,PHS  
IFATE,AN,ANJUNC,IHEAD,IPN,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THEPHS  
2IAS,THEIA,COMP,THAB,INJUNC,RCAB,TEST,NSFG,ZVEL,VELZ,P1P,ECICAB,PHS  
3ECICAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,MCAB,IDEV,ICHECK,NEDEV,NDATC  
COMMON /TANG/ ICAB(22),INDAB(100)  
COMMON /TITLE/ TITLE(8) OF HI  
COMMON /PL/ IFUCH,IP,CH,TITLEM(B),DEVWT  
DIMENSION IJUNC(13,44), IR(3,44), IRS(3,44), TJ,JUNC(3,44), PJJUNC(3,44),  
13,44)  
DIMENSION FCAB(3,5,1,22), HCAB(3,5,1,22), PJJUNC(3,44), PCA8(3,5,1,22)  
1)  
20 DIMENSION ICA8(3,5,1,22), PCA8(3,5,1,22), RCABU(3,5,1,22)  
DIMENSION INODE(22), ERJUNC(44), IRJUNC(44), UATI(10), DATN(10),  
14,22)  
14,22)  
25 DIMENSION PJUNC(3,44), DCAB(22), DCAB(22), ANJUNC(44), TEST(14)  
DIMENSION ZJUNC(25), VEL(25), ECICAB(22), EXP CAB(22), ZJUNC(22),  
DIMENSION EJUNC(22), PATH(22), ICAB(22), WCAB(22), IDE8(1000)  
DIMENSION ICHECK(44)  
INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,IFLG  
INTEGER PAIR  
REAL IR,IF,  
WRITE (IPRN,40) TITLEM  
IF (INDA8,NE,0) WRITE (IPRN,45) TITLE  
40 WRITE (IPRN,50)  
WRITE (IPRN,55) PHI  
IF (PHI,LT,0) WRITE (IPRN,60)  
IF (PHI,LC,0) WRITE (IPRN,65)  
WRITE (IPRN,70)  
WRITE (IPRN,75) ANC  
UC 5 N=1,ANC  
INDEX=ANJUNC(N)  
5 WRITE (IPRN,80) INDEX, (PJUNC(I,INDEX), I=1,3)  
NCJUNC=NC+NAIC-NH  
WRITE (IPRN,85) NJUNC  
WRITE (IPRN,90) NF  
IF (NF,IR,FC,0) GO TO 15  
45 DC 10 N=1,NH  
10 WRITE (IPRN,95) NJUNC(N),ERJUNC(N)  
15 WRITE (IPRN,100) NCAB  
UC 2C N=1,NC  
NSEGMODE(N)=1  
HEM(N)\*NSEG(C)  
26 \*ELEIF (IPRN,105) NJUNC(N),LJUNC(N),PL,ICAB(N),CAH(N),CDCAH(N)  
JFICAB(N)+XP CAB(N),MSEL,ICAH(N)  
SITE (IPR,1,110)  
ECAU (IPR,1,115) (DATI(1),1,1,10)  
IF (DATI(2).EQ.1) TEST(3) GO TO 30  
IF (DATI(2).EQ.2) TEST(9) GO TO 35

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60      GC TO 25          PHS 58
35      JUNCTDATI(3)   PHS 59
      WRITE (11PFN,120) JUNCT • (DATI(K),K=6,8) PHS 60
      GC TO 25          PHS 61
      35 REWIND INTAPE    PHS 62
      WRITE (11PN,125) NCEV PHS 63
      WRITE (11PN,130) CONED PHS 64
      IF (LG.EQ.0) WRITE (11PN,135) NDAIC PHS 65
      RETURN             PHS 66
      PHS 67
      PHS 68
      PHS 69
      PHS 70
      PHS 71
      PHS 72
      PHS 73
      PHS 74
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      PHS 103
      PHS 104
      PHS 105
      PHS 106

60      GC TO 25          PHS 58
35      JUNCTDATI(3)   PHS 59
      WRITE (11PFN,120) JUNCT • (DATI(K),K=6,8) PHS 60
      GC TO 25          PHS 61
      35 REWIND INTAPE    PHS 62
      WRITE (11PN,125) NCEV PHS 63
      WRITE (11PN,130) CONED PHS 64
      IF (LG.EQ.0) WRITE (11PN,135) NDAIC PHS 65
      RETURN             PHS 66
      PHS 67
      PHS 68
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60      GC TO 25          PHS 58
35      JUNCTDATI(3)   PHS 59
      WRITE (11PFN,120) JUNCT • (DATI(K),K=6,8) PHS 60
      GC TO 25          PHS 61
      35 REWIND INTAPE    PHS 62
      WRITE (11PN,125) NCEV PHS 63
      WRITE (11PN,130) CONED PHS 64
      IF (LG.EQ.0) WRITE (11PN,135) NDAIC PHS 65
      RETURN             PHS 66
      PHS 67
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60      GC TO 25          PHS 58
35      JUNCTDATI(3)   PHS 59
      WRITE (11PFN,120) JUNCT • (DATI(K),K=6,8) PHS 60
      GC TO 25          PHS 61
      35 REWIND INTAPE    PHS 62
      WRITE (11PN,125) NCEV PHS 63
      WRITE (11PN,130) CONED PHS 64
      IF (LG.EQ.0) WRITE (11PN,135) NDAIC PHS 65
      RETURN             PHS 66
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60      GC TO 25          PHS 58
35      JUNCTDATI(3)   PHS 59
      WRITE (11PFN,120) JUNCT • (DATI(K),K=6,8) PHS 60
      GC TO 25          PHS 61
      35 REWIND INTAPE    PHS 62
      WRITE (11PN,125) NCEV PHS 63
      WRITE (11PN,130) CONED PHS 64
      IF (LG.EQ.0) WRITE (11PN,135) NDAIC PHS 65
      RETURN             PHS 66
      PHS 67
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      PHS 106

60      GC TO 25          PHS 58
35      JUNCTDATI(3)   PHS 59
      WRITE (11PFN,120) JUNCT • (DATI(K),K=6,8) PHS 60
      GC TO 25          PHS 61
      35 REWIND INTAPE    PHS 62
      WRITE (11PN,125) NCEV PHS 63
      WRITE (11PN,130) CONED PHS 64
      IF (LG.EQ.0) WRITE (11PN,135) NDAIC PHS 65
      RETURN             PHS 66
      PHS 67
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SUBROUTINE HPC1Y 74/74 0P1=1

FTN 4.6+433E 03/07/80 11.41.06

PAGE 1

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1      *SUBROUTINE HPC1Y (C,HK,H1)
2
3      C THIS ROUTINE FINDS REAL ROOTS OF POLYNOMIAL EQUATIONS UP TO
4      C (4)*(X**2) + C(3)*(X**2) + C(2)*X + C(1) = 0 FOR USE IN
5      C EVALUATING MAXIMUM CABLE DISPLACEMENTS AND TENSION EXTREMA
6
7      C HEAL PARTS OF ROOTS ARE PLACED IN RR. IMAGINARY PARTS IN RI
8      C SINCE ONLY REAL ROOTS ARE OF INTEREST, ALL NON-REAL OR
9      C NON-EXISTING ROOTS RETURN RR=0, RI=1
10
11      C DIMENSION C(4), HK(3), H1(3)
12      C
13      IF (C(4))=0.0 GC TO 40
14      IF (C(3))=0.0 GC TO 30
15      IF (C(2))=0.0 GC TO 15
16
17      C GET HERE IF EQUATION IDENTICALLY SATISFIED
18
19      C 5 UC 1C 1I=1,3
20      HK(1)=0.
21      HK(2)=1.
22      RETURN
23
24      C GET HERE IF EQUATION LINEAR
25
26      C 15 HK(1)=-C(1)/C(2)
27      HK(1)=0.
28      UC 25 I=2,3
29      HK(I)=0.
30      25 HK(I)=1.
31      RETURN
32
33      C GET HERE IF EQUATION CUBIC
34
35      C 36 DISC=C(2)**2-C(1)*C(3)
36      IF (DISC<=0.0) GC TO 35
37      GC TU 5
38      HK(1)=1.C(2)+SQR(DISC))/(2*C(3))
39      HK(1)=0.
40      HK(2)=(-C(2)-SQR(DISC))/(2*C(3))
41      HK(2)=0.
42      HK(3)=0.
43      HK(3)=1.
44      RETURN
45
46      C GET HERE IF EQUATION CUBIC
47
48      C 49 P=C(3)/C(4)
49      Q=C(2)/C(4)
50      K=C(1)/C(4)
51      A=(3.0*P+Q**2)/1.
52      H=(2.0*P+Q**2)*Q*(P+Q**2)**27.
53      DISC=(H**2/4.0+K**2/27.0)**27.
54      E (DISC) 51 45,45
55
55      C5 (DISC>=0.0) HK(1)=C(1)*
56      IF (H**2.0+(Q+DISC)) CAPA=1.0
57      IF (H**2.0+(Q+DISC)) CAPD=1.0-H/2.0*DISC
58      IF (H**2.0+(Q+DISC)) CAPB=(1.0-H/2.0*DISC)**4.0
59      IF (H**2.0+(Q+DISC)) CAPC=(1.0-H/2.0*DISC)
```

SUBROUTINE RPULY      74 / 14      OPT=1

F7N 4.6\*43JE

PAGE 2

```
      CAPHE=(((-H/2.+DISC)**6)*(1.+3.*))/(-H/2.-DISC)
      HK(1)=CAP*CAFU-P/3.
      K1(1)=0.
      IF (DISC*G1+0.) GO TO 20
      HK(2)=-CAFU-H/3.
      PI(2)=0.
      HK(3)=PH(12)
      PT(3)=0.
      RETURN
5C  DISC=2.*SCH((A/3.))
      PHI=ACOS((+3.*K1)/(A*DISC))/3.
      RF(1)=-P/3.*DISC*COS(PHI)
      HQ(12)=-P/3.*DISC*COS(PHI+3.14159265*(2./3.))
      HQ(3)=-P/3.*DISC*COS(PHI+3.14159265*(4./3.))
      PI(1)=0.
      PI(2)=0.
      PI(3)=0.
      RETURN
END
```

```
      HPO 58
      RPO 59
      HPO 60
      HPO 61
      HPO 62
      HPO 63
      HPO 63
      RPO 64
      RPO 65
      RPO 66
      RPO 66
      RPO 67
      RPO 67
      RPO 68
      RPO 69
      RPO 70
      RPO 71
      RPO 72
      RPO 73
      RPO 74
      RPO 75
      RPO 76-
```

FUNCTION SPACE 7474 INPUT

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```
1 *CHECK SPACE (1)
C THIS ROUTINE CALCULATES THE LOCATION IN SPACE
C OF ANY POINT ON THE ARRAY
C
COMMON /BJJ/ VELX(25),VELY(25)
COMMON /B1/ FEJUNC,IR,DELTA,IIRS,IFJUNC,E,ES,FCAB,HCAB,JUMP,SPA
IR,JUNC,P,CAB,PCAB,RCAB,Theta,P,JUNC
COMMON /B2/ NCAB,ANODE,LRJUNC,IRJUNC,DAI1,DELTA,IRS,IFJUNC,E,ES,FCAB,HCAB,JUMP,SPA
IATE,MANG,ANJUNC,IREAD,IPART,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THESPA
ZIAS,THETA,CORPD,THEIA,ANJUNC,RHU,TEST,AVSEG,ZVEL,VELZ,P,IP,ECICAB,SPA
3EXPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,W CAB,IDEV,ICHECK,NDDEV,NDATC
UDIMENSION FEJUNC(3,44), IRS(3,44), IRJUNC(3,44), P,JUNC(3,44), PJUNC(3,44)
13*44)
UDIMENSION FCAH(3,51,22), RCAAH(3,51,22), P,JUNC(3,44), PCAB(3,51,22)SPA
1) UDIMENSION PLANE(3,51,22), PCAHO(3,51,22), RCAAU(3,51,22), SPA
UDIMENSION IRJUNC(22), ERJUNC(44), DAII(10), DAII(10), HSPA
1(22)
UDIMENSION P,JUNC(3,44), CUCAB(22), DCAB(22), ANJUNC(44), TEST(14)
UDIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXP CAB(22), ZJUNC(22)
UDIMENSION LJUNC(22), PATH(22), WCAB(22), IDEV(1000)
UDIMENSION ICHECK(44)
INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
INTEGER PATH
PEAL IP,IFS
IF (DAT(1,2)*EG,TEST(3)) GO TO 5
IF (DAT(1,2)*EG,TEST(4)) GO TO 10
30   C GET HERE IF JUNCTION POINT
      C
      5 N=DAT(1,3)
      SPACE=P,JUNC(1,1,0)
      RETURN
35   C GET HERE IF POINT ON A CABLE
      C
      10 N=DAT(1,3)
      M=(DAT(1,0)/H(N))+1
      C CALCULATE DISTANCE, SIGMA, OF POINT FROM NODE N
      C
      SIGMA=DAT(1,0)-(M-1)*H(N)
      C
      40   C CALCULATE EXTRAPOLATION QUANTITIES
      C
      E=EX CAB(M,N)*HCAB(M,N)/TCAB(M,N)
      F=FE CAB(M,N)*FCAB(M,N+1,N)/TCAB(M+1,N)
      C
      45   C CALCULATE LOCATION
      C
      50   C CALCULATE LOCATION
      C
      55   C RETURN
```

STARTUP LINE START 76/74 OPT=1

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1 \*CHECK START  
SUBROUTINE START

C THIS ROUTINE CALCULATES THE INITIAL GUESSES AT THE IMAGINARY  
C AND EQUIILIBRATING REACTIONS AND THE INITIAL DELTA BASED ON  
C THE TOTAL WEIGHT OF THE ARRAY

C COMMON /B3/ VEL(25),VELY(25)

COMMON /B1/ FEJUNC,IRJUNC,IHS,IFJUNC,E,ESS,FCAB,RCAH,JUMP,STA

IPJUNC,PCAB,PCABH,RCABH,RCABO,TMTHO,TRJUNC,IRJUNC

CCAMON /B2/ NCAB,NCABO,PCAB,PCABH,RCABH,RCABO,TMTHO,TRJUNC,IRJUNC,THJUNC,DATN,DATN+,PJUNC,CUCAB,DCAB,STA

IFATE,NANC,ANJUNC,IREAD,IPRN1,INIAPE,OUTAPE,ITIME,IFLG,OFLG,NINH,THESTA

21 AS,THEIA,COMP,THFLB,IRJUNC,PHOT,TEST,NSF6,ZVEL,VELZ,PIP,ECICAB,STA

3EXPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,ICAB,10EV,ICHECK,NUEV,NUATC,STA

DIMENSION FEJUNC(3,44),IR(3,44),IRS(3,44),PJUNC(3,44),PJUNC0(3,44)

13,44)

01MENSION ICAB(3,51,22),RCABH(3,51,22),PJUNC(3,51,22),PCAHC(3,51,22)

14,22),DIMENSION IRJUNC(22),ERJUNC(44),IRJUNC(44),DATN(10),DATN(10),HSTA

14,22).

DIMENSION PJUNC(3,51,44),CUCAB(22),DCAB(22),ANJUNC(44),TEST(14)

15 DIMENSION ZVEL(25),VELZ(25),ECICAB(22),EXP CAB(22),ZJUNC(22)

16 DIMENSION LJUNC(22),PAIH(22),ICAB(22),WCAH(22),IUEV(1000)

17 DIMENSION OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG

18 INTEGER PATH,IR,IS,STA

19 REAL IR,IS,STA

20 WEIGHT=0,STA

21 DO 5 J=1,IRJUNC,STA

22 S WEIGHT=WEIGHT+FEJUNC(3,0,J)

23 UC10,N=1,NCAB,STA

24 INNAME(N)=IRJUNC(1)-1,STA

25 IC10,M=1,INNN,STA

26 WEIGHT=WEIGHT+FCAB(3,0,M,N)

27 DC15,N#=1,NINH,STA

28 KER=ERJUNC(1),STA

29 DC15,1#1,J,STA

30 IS IR(1,KER)=0,STA

31 DC20,N=1,NIR,STA

32 KER=IRJUNC(1),STA

33 KER=ERJUNC(1),STA

34 IR(1,KER)=0,STA

35 IR(2,KER)=0,STA

36 IR(3,KER)=WEIGHT/(NIR+1),STA

37 IR(3,KER)=IR(3,KER)-IR(3,KER)

38 DELTA=AH5(WEIGHT)/(NIR+1),STA

39 RETURN,STA

40 END

41 IR(3,KER)=0,STA

42 IR(3,KER)=IR(3,KER)-IR(3,KER)

43 DELTA=AH5(WEIGHT)/(NIR+1),STA

44 IR(3,KER)=0,STA

45 IR(3,KER)=IR(3,KER)-IR(3,KER)

46 DELTA=AH5(WEIGHT)/(NIR+1),STA

47 RETURN,STA

48 END

49 END

134

40

35

30

20

15

10

5

0

-5

-10

-15

-20

-25

-30

-35

-40

-45

-50

-55

-60

-65

-70

-75

-80

-85

-90

-95

-100

SUBROUTINE SROUT 7474 OPT=1

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1         SUBROUTINE SROUT  
C  
C THIS ROUTINE GENERATES THE ARRAY STRUCTURAL OUTPUT  
C  
5  
COMMON /B1/ VELX(25),VELY(25)  
COMMON /B1/ FEJUNC,IR,DELTA,IHS,TJUNC,E,ES,FCAB,RCA,B,JUMP,STR  
IPJUNC,PCAB,PCAB,RCAB,PCAB,RCAB,THETA,P JUNCO  
CMHUN /B2/ HCAH,NODE,ERJUNC,IRJUNC,DATI,DAIN,I,PJUNC,CUCAB,DCAB,STR  
IATE,NAHC,ANJUNC,IREAC,IPNT,INTAPE,OUTAPE,ITME,IFLG,NR,THESTR  
21AS,THETE,CUPU,THEIAH,NJUNC,WHOTEST,NSEG,VEL,VELZ,PIP,ECICAB,STR  
3E\*PCAH,ZJUNC,LJUNC,FATH,ICAH,IVOPT,WCAH,IDEV,ICHECK,NDATC,STR  
12  
COMMON /CVEL/ VMAG(25,4),VDIR(25,4),ZPT(25,4),XPT(4),NPPS(4)  
1) \*USTA  
COMMON /LEVEL/ ILEVEL  
COMMON /PCAB/ XNP1(4),YNP1(4)  
COMMON /TIAH/ ICAB(22),TDCAB(1000)  
COMMON /TITLE/ ITITLE(8),PHI,CURITS,IUNIT,VELXP(25),VELYP(25)  
COMMON /PU/ IPUNCH,IPATCH,ITLEM(8),DEVW  
COMMON /KILMH/ KOUNTH,NIT,MAITER,NSTEPS,ISTEP,PERCENTV,INCPRINT  
DIMENSION FEJUNC(3,44),IR(3,44),IJUNC(3,44),PJUNC,STR  
13\*44)  
DIMENSION FCAH(3,51,22),RCAB(3,51,22),PJUNC(3,44),PCAH(3,51,22)  
STR  
15  
DIMENSION PCAB(3,51,22),PCABU(3,51,22),RCABU(3,51,22)  
DIMENSION IR(3,51,22),ERJUNC(44),IRJUNC(44),DATI(10),DAIN(10),STR  
16  
11(22)  
DIMENSION PJUNC(3,44),CUCAB(22),DCAB(22),ANJUNC(44),TEST(14)  
DIMENSION AVEL(25),VEL(25),ECICAB(22),EXPBAR(22),LJUNC(22)  
30  
DIMENSION LJUNC(22),PAIH(22),ICAB(22),WCAB(22),IDEV(1000),  
DIMENSION ICHECK(44)  
DIMENSION SPACE0(3,1010),PJORIG(3,44),DISPO(3)  
DIMENSION NSEW(4)  
DIMENSION UJITS(3)  
35  
INTEGER OUTAP,LJUNC,ERJUNC,ANJUNC,OFLG  
INTEGER PATH  
REAL IRHS  
DIMENSION TEMP(3),TEMP(3,3),TEMP(3,3),PSPACE(3)  
DIMENSION A(3),H(3),D(3),U(3),V(3),W(3),C(4),RQ(3),RI(3)  
DATA NSEW/SW,NORTH,SE,SOUTH/EAST,SW,WEST/  
DATA UNIT/SH (KNOTS).8/(CM/SEC)/RH(F1/SEC)/  
NCJUNC=NCAH+NANC-NIR  
JLM=JUMP+1  
FACTORS#1  
PCTPERCH=100.  
IF (INCPRINT.EQ.1) FACTOR=PERCENTV  
GC TO (5,10),JUM  
5 WRITE (IPRN,465) TITLER  
IF (IPUNCH.EQ.8H YES) WRITE (IPNCH+470) TITLER  
GC TO 55  
50  
5C WRITE (IPNCH+475) TITLER,111E  
5 WRITE (IPRN,480) ROUNT  
IV=IVOPT+1  
5C TO (15,20,30,40),IV  
55  
5C CURRENT OPTION 0  
5C

SUBROUTINE SHOUT 74/74 OPT=1

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15 WRITE (IPRN1,485) IVOPT1
    IF (IPUNCH.EQ.8H) YES) WRITE (IPNCH,490) TITLE
    IF (IPUNCH.EQ.BH) YES) WRITE (IPNCH,495) IVOPT1
    GC TO 55

C CURRENT OPTION 1
C
C 20 WRITE (IPRN1,500) IVOPT1
    WRITE (IPRN1,505) UNITS(UNIT1+1)
    DC 25 N=L,IVSEG
    VLFACT=VELP(M)*FACTOR
    25 WRITE (IPRN1,510) ZVEL(M)*VLFACT,VELYP(M)
    IF (INCPRN.EQ.1) WRITE (IPRN1,515) PCT
    WRITE (IPRN1,520)
    THETA=THETA
    IF (THETAX.GE.360.) THETAX=THETAX-360.
    IF (THETAN.GE.360.) THETAN=PHI
    IF (THETA.EG.360.) THETA=0.
    IF (THETAN.EG.360.) THETAN=0.
    WRITE (IPRN1,525) THETA,THETAX,THETAN
    IF (IPUNCH.EQ.8H) YES) WRITE (IPNCH,490) TITLE
    IF (IPUNCH.EQ.BH) YES) WRITE (IPNCH,530) THETA
    GC TO 55

C CURRENT OPTION 2
C
C 30 WRITE (IPRN1,500) IVOPT1
    WRITE (IPRN1,505) UNITS(UNIT1+1)
    DC 35 N=L,IVSEG
    VLFACT=VELP(M)*FACTOR
    35 WRITE (IPRN1,510) ZVEL(M)*VLFACT,VELYP(M)
    IF (INCPRN.EQ.1) WRITE (IPRN1,515) PCT
    WRITE (IPRN1,520)
    IF (IPUNCH.EQ.BH) YES) WRITE (IPNCH,490) TITLE
    IF (IPUNCH.EQ.8H) YES) WRITE (IPNCH,530) THETA
    GC TO 55

C CURRENT OPTION 3
C
C 40 WRITE (IPRN1,500) IVOPT1
    DC 50 L=L,NSIA
    IF S=1
    IF (XNP(L).EQ.0) INSE=2
    IE=4
    IF (YNP(L).EQ.0) IEW=3
    AXNP=ABS(XNP(L))
    AYNP=ABS(YNP(L))
    ATNP=ABS(ATNP(L))
    WRITE (IPRN1,535) L*AXNP*INSE*(INS),AYNP*NSE*(IEW)*XPT(L)*YPT(L)
    WRITE (IPRN1,540) UNITS(UNIT1+1)
    NS=IPPS(L)
    DC 45 L=L+1,NS
    VU=VUDR(L)+360.+P+1
    YU=VUDR(L)
    IF (VX.GE.360.) VX=VX-360.
    VAGP=VAG(L)+CUNIS
    WRITE (IPRN1,549) (ZP(L,L)+VAGP,VN,VX)
    50 CONTINUE

```

SUBROUTINE SJROUT 74/74 OPR#1

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FN 4.6+433E

115 WRITE (IPNCH,545)  
IF (IPNCH.EQ.0) YES) WRITE (IPNCH,490) TITLE  
IF (IPNCH.EQ.8H YES) WRITE (IPNCH,495) IYOPT

C GENERATE ANCHOR HEADERS

120 C 55 WRITE (IPR41,550)  
WRITE (IPRN1,555)  
WRITE (IPRN1,555)  
WRITE (IPRN1,560)  
WRITE (IPRN1,565)  
C THIS SECTION CALCULATES FORCES AND ANGLES AT ANCHORS  
DO 110 J1=1,NANC  
J3=0  
J2=1  
DU IF (ANJUNC(J1)).EQ.0.ZJUNC(J2)). GO TO 100  
65 J2=J2+1  
TF (J2).LE..NCAJ) GO TO 60  
TF (INR.EQ.0) GO TO 110  
70 J3=1  
75 IF (ANJUNC(J1)).EQ.ERJUNC(J3)) GO TO 85  
90 J3=J3+1  
IF (J3.LE..MIN) GO TO 75  
IF (J3.LE..MIN) GO TO 110  
GC TO 110  
85 INDEX=IRJUNC(J3)  
UC 90 J4=1,NCAU  
IF (INDEX.EQ.LJUNC(J4)) GO TO 95  
93 CONTINUE  
95 GO TO 110  
95 MN=J4  
MX=NNODE(J4)  
1=TCAB(MX,MN)  
RX=-RCAB(1,MX,MM)  
HY=-RCAB(2,MX,MM)  
HZ=-RCAB(3,MX,MM)  
UC TO 105  
MN=J2  
105  
I=TCAB(1,MN)  
WX=RCAB(2,1,MM)  
HY=RCAB(3,1,MM)  
HZ=SQR((KX\*\*2+HY\*\*2))  
HZ=HH  
IF (KX\*\*2+HY\*\*2) RHM=1.  
A1=ASIN(HY/KX)/PIP  
IF (RM2.EG.0\*) RHM=0\*  
A2=ASIN(HZ/1)/PIP  
IF ((HX.LT.0\*).AND.(HY.GE.0\*)) A1=180.-A1  
IF ((HX.LT.0\*).AND.(HY.LT.0\*)) A1=-180.-A1  
IF (IPNCH.EQ.70) ANJUNC(J1),NM,T,PX,RY,RZ,RH,A1,A2  
IF ((JP,L).EQ.0) GC TO 65  
IF ((J2.EQ.NCAU).AND.(J3.EQ.0)) GO TO 70  
IF ((J2.EQ.NCAU).AND.(J3.NF.NJUNC)) GO TO 80  
C GENERATE CABLE HEADERS  
137  
138  
139  
140  
141  
142  
143  
144  
145  
146  
147  
148  
149  
150  
151  
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171

```

C          WRITE (IPRINT,575)
      WRITE (IPRINT,580)
      IF (IOMN.GT.1) GO TO 115
      WRITE (IPRINT,595)
      GC TO 120
      115 WRITE (IPRINT,590)
      WRITE (IPRINT,595)

180    120  CONTINUE
      C          THIS SECTION CALCULATES MAXIMUM AND MINIMUM CABLE TENSIONS
      C          AND MAXIMUM CABLE DISPLACEMENTS FROM NO CURRENT LOCATION
      C          BY EXTRAPOLATION BETWEEN CABLE NODES
      C          INITIALIZE EXTREMA
      C
      DO 295 MN=1,NCAB
      N=NN
      TMAX=TCAB(1,MN)
      SMAX=0,
      IMAX=IMAX
      SIMIN=0.
      125  UMAX=0.
      DC 10  (135,125)* JUM
      DC 120  I=1,3
      130  DC 130  I=1,3
      131  DC 140  I=1,3
      132  DC 150  I=1,3
      133  DC 160  I=1,3
      134  DC 170  I=1,3
      135  MY=NODUE(MN)-1
      DC 245  MM=1,MM
      MM=MM
      M1=MM+1
      C          CALCULATE EXTRAPOLATION QUANTITIES
      C
      RR=0.
      MU=0.
      DC=0
      DC 156  I=1,3
      140  DC 157  I=1,3
      DC 158  I=1,3
      DC 159  I=1,3
      DC 160  I=1,3
      DC 161  I=1,3
      DC 162  I=1,3
      DC 163  I=1,3
      DC 164  I=1,3
      DC 165  I=1,3
      DC 166  I=1,3
      DC 167  I=1,3
      DC 168  I=1,3
      DC 169  I=1,3
      DC 170  I=1,3
      DC 171  I=1,3
      DC 172  I=1,3
      DC 173  I=1,3
      DC 174  I=1,3
      DC 175  I=1,3
      DC 176  I=1,3
      DC 177  I=1,3
      DC 178  I=1,3
      DC 179  I=1,3
      DC 180  I=1,3
      DC 181  I=1,3
      DC 182  I=1,3
      DC 183  I=1,3
      DC 184  I=1,3
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      DC 187  I=1,3
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      DC 198  I=1,3
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      DC 221  I=1,3
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      DC 225  I=1,3
      DC 226  I=1,3
      DC 227  I=1,3
      DC 228  I=1,3
      DC 229  I=1,3
      DC 230  I=1,3
      DC 231  I=1,3
      DC 232  I=1,3
      DC 233  I=1,3
      DC 234  I=1,3
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      DC 255  I=1,3
      DC 256  I=1,3
      DC 257  I=1,3
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      DC 262  I=1,3
      DC 263  I=1,3
      DC 264  I=1,3
      DC 265  I=1,3
      DC 266  I=1,3
      DC 267  I=1,3
      DC 268  I=1,3
      DC 269  I=1,3
      DC 270  I=1,3
      DC 271  I=1,3
      DC 272  I=1,3
      DC 273  I=1,3
      DC 274  I=1,3
      DC 275  I=1,3
      DC 276  I=1,3
      DC 277  I=1,3
      DC 278  I=1,3
      DC 279  I=1,3
      DC 280  I=1,3
      DC 281  I=1,3
      DC 282  I=1,3
      DC 283  I=1,3
      DC 284  I=1,3
      DC 285  I=1,3
      DC 286  I=1,3
      DC 287  I=1,3
      DC 288  I=1,3
      DC 289  I=1,3
      DC 290  I=1,3
      DC 291  I=1,3
      DC 292  I=1,3
      DC 293  I=1,3
      DC 294  I=1,3
      DC 295  I=1,3
      C
      138
  
```

```

      NW=0.
      DC 165 I=1,3
      V(1)=EXCAB(M,N)*RCAB(I,M,N)/TCAB(M,N)
      W(1)=EXCAB(M,N)*RCAB(I,M,N)/TCAB(M,N)-V(1))/H(N)
      V(1)=P(1)-V(1)
      W(1)=(P(1)-W(1))/2.
      UL=U(1)*L(1)
      UV=U(1)*V(1)
      UV=UVW*2.*U(1)*W(1)*V(1)*V(1)
      VH=V(1)*W(1)*W(1)
      DC 170 I=1,3
      HCAB(1,M,N)=TEMP1(I)
      HCAB(1,M,N)=TEMP2(I)
      C(4)=U.
      C(3)=0.
      C(2)=DD
      C(1)=HO
      CALL RPOLY (C,HO,RI).
      C CALCULATE TENSION EXTREMA IN SEGMENT
      C JTIME=0
      180 CCNTNU
      DC 205 I=1,3
      IF (JTIME.EQ.1) GC TO 185
      IF ((W(1)).NE.C(.)) GU TO 205
      IF ((R(1)).LE.0.).OR.(R(1)).GE.H(N))) GU TO 205
      SIG=AL(I)
      185 TE=SIGHT(WA*2.*HU*S16*DU*SIG**2)
      IF ((E.GT.TMAX)) GC TO 195
      IF ((E.LT.JMIN)) GC TO 200
      IF ((E.LT.JMAX).OR.(E.GT.H(N))) GC TO 205
      GC TO 210
      195 TMAX=E
      SHMAXH(N)*(M-1)+S16
      GC TO 90
      200 TR1=TR1
      S14=(I-1)*(M-1)+S16
      GC TO 190
      205 CCNTNU
      SJ=SH(N)
      GC TO 186
      GC TO 186 (245,215)+ JUM
      215 C(4)=2.*VN
      C(3)=3.*VN
      C(2)=UVW
      C(1)=V
      CLL RPOLY (C,HO,RI)
      C CALCULATE MAXIMUM DISPLACEMENT IN SEGMENT
      C JTIME=0
      220 CCNTNU
      DC 204 I=1,3
      IF (JTIME.EQ.1) GU TO 225
      225
      260
      265
      270
      275
      280
      285

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IF (R1(1).LE.0.) GO TO 240
IF ((R0(1)).LE.0.).OR.(H(1).GE.H(N)) GO TO 240
SIG=H(1)
225 ZARG=U*2.0*VW*SIG**2.0*VW*SIG**3.0*WW*SIG**4
C THESE STATEMENTS CHECK ZARG FOR ZERO AND NEGATIVE VALUES
C ZARG SHOULD BE POSITIVE, IF IT IS NOT IT IS COMPARED TO H(N).
C THE LENGTH OF ONE CABLE SEGMENT, IF IT IS SMALL BY COMPARISSON, IT
C IS SET TO A SMALL POSITIVE VALUE
C IF (ZARG.LT.0.0.AND.ABS(ZARG/H(N)).LT.0.0001) ZARG=ABS(ZARG)
C IF (ZARG.EQ.0.) ZARG=0.000001*H(N)
DE=SQR(1.0/ZARG)
230 IF (DE.GT.DMAX) GO TO 235
IF (JTYPE.EQ.0) GO TO 245
235 DMAX=DE
SDMAX=H(N)*(N-1)*SIG
GO TO 230
240 CONTINUE
JTIME=1
SIGM(H(N))
GO TO 220
245 CONTINUE
C EXTHEMA ALONG A CABLE NOW DETERMINED
C CALCULATE FINAL AND INITIAL COORDINATES OF MAXIMALLY DISPLACED POINTS
C
250 HL=H(N)*MAX
IF (SDMAX.LT.HL) GO TO 260
K=LJUNC(N)
DO 255 I=1,3
A(I)=PJUNC(I,K)
255 H(I)=PJUNC(I,K)
256 GC TO 285
260 DATA(I2)=FES/(4)
DATA(I3)=SDMAX
J=(SDMAX/F(N))+1
J1=J+1
DC 265 I1=1,3
I=1,I
265 A(I)=SPACE(I)
DC 271 I=1,3
TEMP1(I)=HCAB(I,J,N)
TEMP2(I)=HCAB(I,J+1,N)
TEMP3(I)=PCAB(I,J,N)
PCAB(I,J,N)=HCAB(I,J,N)
HCAB(I,J+1,N)=HCAB(I,J,N)
270 PCAB(I,J+1,N)=PCAB(I,J,N)
UC 275 I1=1,3
I=1,I
275 H(I)=SFAC(I)
DC 279 I=1,3
HCAB(I,J,K)=TEMP1(I)
HCAB(I,J+1,N)=TEMP2(I)
HCAB(I,J+1,N)=TEMP3(I)
280 PCAB(I,J+1,N)=TEMP3(I)
285 CONTINUE

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140

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      WRITE (IPRNT,600) N,IMAX,SMAX,TMIN,SMIN,DMAX,SDMAX,(AI(I),I=1,3)*STR 343
      11B(I,I),I=1,3)
      345   GC TU 295
      295   WRITE (IPRNT,CU0) N,IMAX,SMAX,TMIN,SMIN
      295   CONTINUE

C   GENERATE JUNCTION HEADERS
C
      C   WRITE (IPRNT,605)
      C   WRITE (IPRNT,610)
      C   LF (JUM,91,1) GO TO 300
      C   WRITE (IPRNT,615)
      C   WRITE (IPRNT,620)
      C   GO TO 305
      C   360   CONTINUE
      C   WRITE (IPRNT,625)
      C   WRITE (IPRNT,630)
      C   365   CONTINUE

C   THIS SECTION CALCULATES JUNCTION FORCES, LOCATIONS AND DISPLACEMENTS
C
      C   IF =0
      C   UC 395 J1=1,NCJUNC
      C   DC 310 K=1,RA,C
      C   IF (AJUNC(K).EQ.J1) GU TU 395
      C   310   CONTINUE

      C   GC TU (325,315)* JUM
      C   315   DO 320 J2=1,3
      C   320   UISP(J2)=PJUNC(U2,J2)-PJURIG(U2,J1)
      C   320   UISP(J2)=PJUNC(U2,J1)-PJUNC(U2,J1)
      C   325   J6=1
      C   IF (INDIC,61,0,0,JUM,61,1) GU TU 395
      C   375   DC 330 J2=1,3
      C   330   PJORIG(U2,J1)=PJURIG(U2,J1)
      C   335   COUNTNIE
      C   340   IF (J1.EQ.ZJUNC(J6)) GU TU 360
      C   345   IF (J1.EQ.LJUNC(J6)) GU TU 386
      C   350   IF (J6,1,E,NCAR) GC TU 340
      C   355   IF (J1.EQ.FKJUNC(J7)) GU TU 365
      C   360   IF (J7,LE,NIM) GO TU 355
      C   360   GU TU 295
      C   360   MM=J6
      C
      C   390   I=CAH(1,MM)
      C   H=RCAB(1,1,MM)
      C   W=RCAH(2,1,MM)
      C   HZ=HCAB(3,1,MM)
      C   UC TU 395
      C   365   INDEX=(JJUNC(-7)
      C   UC 370 JDE=J+CAH
      C   F (INDEX,E,LJUNC(JH)) GU TU 375
      C   375   MM=JH
      C   UC TU 395
      C

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400      361  MW=J1
        385  MXNODNE (P1)
        1=LCM (X,MM)
        HX=RCAH (1,P,MM)
        HY=RCAH (2,P,MM)
        HZ=RCAH (3,P,MM)
        H7=SIGHT (HX,0,2*RY**2)
        IF (HN.EW.J1) H7=1.
        A1=ASIN (HY/P1)/P1
        A2=ASIN (HZ/P1)/P1
        J1=(HX,L1,0)*AND. (RY,GE,0.)
        A1=180.-A1
        IF ((HX,L1,0)*AND. (RY,LT,0.)) A1=-180.-A1
        IF ((IF,EG,0.)*AND. (JW,EU,1)) WRITE (IPHNT,635) J1,MM,T,A1,A2,(PJUSTR
        413  IC,(K,J1),K=1,3)
        IF ((IF,EG,0.)*AND. (JW,EU,1)) WRITE (IPHNT,635) J1,MM,T,A1,A2,(PJUSTR
        INC(K,J1),K=1,3),(DISP,(1),I=1,31,DISP,(1),I=1,3)
        IF ((IF,EW,1)) WRITE (IPRNT,635) J1,MM,T,A1,A2
        IF ((JW,6,L1,NCAB)*AND. (J1,EG,ZJUN(C,J6))) GO TO 345
        IF ((JW,6,L1,NCAB)*AND. (J1,EG,LJUN(C,J6))) GO TO 350
        395 IF=0
        C  GENERATE INDEXED DEVICE HEADERS
        C
        C  WRITE (IPRNT,640)
        C  WRITE (IPRNT,645)
        C  IF (JUM,61,1) GO TO 400
        C  WRITE (IPHNT,650)
        C  WRITE (IPHNT,655)
        C  GO TO 405
        C  WRITE (IPHNT,660)
        C  WRITE (IPHNT,665)
        C  405 CONTINUE
        C
        C  THIS SECTION CALCULATES TENSIONS AT INDEXED DEVICES,
        C  DEVICE LOCATIONS, AND DEVICE DISPLACEMENTS
        C
        425
        C
        C  IF (INDEV,EG,0) GO TO 460
        C  IF (IPUNCH,NE,0) YES, GO TO 420
        C  IF (INDATC,0,1) GO TO 415
        C  NCPUDEV=0
        C  NO 410 RELATED DEV
        C  HEAD (INIAPI,675), (INIL(1),I=1,10)
        C  IF (IUA(1)(2).NE.FSI(3)) AND. (INATC,EG,0)) AND. (INDATC,EG,0))
        C  INCPUNEV=NCPUDEV+1
        C
        435
        C  410 CONTINUE
        C  NEWIND 1MATE
        C  415  WRITE (IPACT,670) NCPUDEV
        C  420  INC 455 N=1,1,DEV
        C  READ (INTARE,C75) (INIL(I),I=1,10)
        C  INEX=X=N
        C  430
        C  501 FORMAT (14.84,HE15.8)
        C  IF (DAT(1)(2).NE.TEST(3)) GO TO 455
        C  K=DAT(1)(3)
        C  M=DAT(1)(4)/((K)+1)
        C  SIGMA=DAT(1)(1)-(M-1)*PK
        C  IF N2=0.

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SIAMHOLINE SIRUOI

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DO 425 II=1,3
 1=II
  PSPACE(1)=SPACE(1)
  IF (NUAIC.EQ.1) JUN=JUN+EQ(1)
  SPACE(0),INDEX)=SPACE(1)
  425 TE=2*1CN2*(KCAB(1,M,K)+KCAB(1,M+1,K))*SIGMA/H(K))**2 STR 461
  TENSUR(1EN2)
  30 10 (430*4 35)  JUR
  430 IF ((IPUNCH.EQ.8H YES).AND. (DAT(6).EQ.DEVWT)) WRITE (IPNCH,6BSTR 464
  19 INDEX,K,DAT(10),OFSpace(1),I=1,3) STR 465
  IF (DAT(5).EQ.0) WRITE (IPNCH,6B5) INDEX*K,DAT(10),LEN, (PSPACE(1STR 466
  1),LEN,3),DAT(6),DAT(9),DAT(7),TDOCAB(INDEX) STR 467
  UC TU 455
  435 DC 440 I=1,3
  TEMP(1)=PCAB(1,M,K)
  TEMP(2)=PCAB(1,M+1,K)
  TEMP(3)=PCAB(1,M,K)
  RCAB(1,M,K)=RCAB(1,M,K)
  RCAB(1,M+1,K)=RCAB(1,M+1,K)
  PCAB(1,M,K)=PCAB(1,M,K)
  PCAB(1,M+1,K)=PCAB(1,M+1,K)
  DC 445 II=1,3
  1=II
  DISPO(I)=PSPACE(1)-SPACE(1,INDEX)
  DISPO(I)=PSPACE(1)-SPACE(1)
  DC 450 II=1,3
  HCAB(1,M,K)=TEMP1(1)
  HCAB(1,M+1,K)=TEMP2(1)
  450 PCAB(1,M,K)=TEMP3(1)
  IF ((IPUNCH.EG.8H YES).AND. (DAT(6).EQ.DEVWT)) WRITE (IPNCH,6BSTR 483
  10 INDEX,K,DAT(10),OFSpace(1),I=1,3) STR 484
  IF (DAT(5).NE.0.) GO TO 455
  IF (IPN(1).NE.0.) GO TO 455
  WRITE (IPN(1),690) INDEX,K,DAT(10),LEN, (PSPACE(1),I=1,3), (DISP(1),I=1,3)
  455 CONTINUE
  460 RETURN INTAPE
  460 RETURN
  460
  465 FORMAT (//1*8A10//,34H ARRAY EQUILIBRIUM WITH NO CURRENT//)
  470 FORMAT (BA)C,35H ARRAY EQUILIBRIUM WITH NO CURRENT ) STR 493
  475 FORMAT (1M1,M10/1X,8A10//) STR 494
  480 FORMAT (/1X,3YNHNUMBER OF ITERATIONS FOR CONVERGENCE - *15/) STR 495
  485 FORMAT (3BH ARRAY EQUILIBRIUM WITH CURRENT UP1ION,13//) STR 496
  490 FORMAT (8A10) STR 497
  495 FORMAT (3BH ARRAY EQUILIBRIUM WITH CURRENT OPTION,13) STR 498
  500 FORMATT (25H CURRENT FIELD OPTION IS *11) STR 500
  505 FORMATT (//7X,12HZ*COORDINATE*6X,12HZ*ANGLE OF *7X,12HDIRECTION OF/SIR 501
  1.8X*16HCF CURRENT,7X,12HCURRENT AT 2,7X,12HCURRENT AT Z/44X,11HFROSTR 502
  2H N-AXIS*,/10X,6H(FEET),11A,A8,10X,9H(WEEHEES))
  510 FORMAT (1X,F10.2*10*X*F8.3*10*X,F8.3*1X*F8.3) STR 503
  515 FORMAT (F10.1*24+ PERCENT OF FULL CURRENT) STR 504
  520 FORMAT (//1X*7A10***CURRENT DIRECTION IS POSITIVE IN THE CLOCKWISSTR 505
  525 IE SENSE FROM THE N-AXIS***//) STR 507
  530 FORMAT (24H ARRAY EQUILIBRIUM WITH *FH.2,1SH DEGREE CURRENT //1X*4STR 508
  10H ARRAY EQUILIBRIUM WITH CURRENT DIRECTION ,/F10.2*2X*42DEGREES FRSIR 509
  2H X-AXIS(* IS COUNTERCLOCKWISE)/F10.2*2X*35HDEGREES FROM N-AXIS(*STR 510
  535 FORMAT (24+ ARRAY EQUILIBRIUM WITH *F8.2*1SH DEGREE CURRENT) STR 511
  540 FORMAT (//1X*26HLOCATION OF STRING NUMBER-,J1/1X,F8.0*1X*4HFEET,1XSIR 512
  545 FORMAT (//1X*26HLOCATION OF STRING NUMBER-,J1/1X,F8.0*1X*4HFEET,1XSIR 513

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STRUCTUREN STRUCTURE 7A/74 OF 1

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1. A5.24.2197.2X.F9.0.1X.4HFEET.1X.A5.10X.2HXR.1UX.2HXR.0.4HFEET.STR 514  
 25.2Y=10.0.4HFEET)

549 FORMAT 1/44X,12MH CURRENT OF .7X,12HDIRECTION OF .7X,12HDIRECTION OF /7X,12HZ-COORDINATE STR 515  
 1.6X,12MH CURRENT OF .7X,12HZ CURRENT AT Z.7X,12HZCURRENT AT 2.ZX,12HZCURRENT AT 2.ZX,10HDF STR 516  
 2 CURRENT 7BX,10HDF CURRENT 7BX,13HZ-AXIS SYSTEM,6X,13HZ-AXIS SYSTEM/STR 518  
 310X,6H(FTE),11XAH,10X,9H(DEGREES),10X,9H(DEGREES)

545 FORMAT //1X,7RH\*\*\*CURRENT DIRECTION IS POSITIVE IN THE CLOCKWISE STR 519  
 1E SENSE FROM THE N-AXIS\*\*\*/1X,85H\*\*\*CURRENT DIRECTION IS POSITISTR 520  
 21E IN THE COUNTERCLOCKWISE SENSE FROM THE X-AXIS\*\*\*\*//) STR 521

550 FORMAT (1H,13HARRAY ANCHORS)  
 555 FORMAT (1H,13H-----/)

560 FCHMAT (1H,32HJUNC. NO. CARLE AT TENSION A1,14X,26HFORCE COMPOSTR 525  
 1MENTS AT ANCHOR,13X,16HANGLE WRT,ANCHOR ANCHOR,6HX-COMP,6X,6HY-COSTA STR 526  
 565 FORMAT (1H,30HANCHOR ANCHOR ANCHOR,6HX-COMP,6X,6HY-COSTA STR 527  
 1MF,6X,6L-COMP,3X,9HHR,-COMP,5X,16HZ-AXIS XY-PLANE)  
 570 FORMAT (1H,3X,12,9X,12,5X,F10,2,3X,4(F10,2,2X),2(2X,F7,2,1X)) STR 528  
 575 FORMAT (1H,3X,12,9X,12,5X,F10,2,3X,4(F10,2,2X),2(2X,F7,2,1X)) STR 529  
 580 FORMAT (1H,3X,12M-----/)

595 FORMAT (1H,41H) MAXIMUM S-COORD MINIMUM S-COORD STR 530  
 1. TENSION OF TENSION OF 0F) S-COORD MINIMUM S-COORD MAXIMUM STR 531  
 597 FORMAT (1H,12MH,12MH) LOCATION OF THIS POINT NO CURRENT LOC. OF THIS PSTR 532  
 1-S-COORD 20INT) 1-S-COORD Y-COORD TENSION OF X-COORD Y-COORD DISP STR 533  
 598 FORMAT (1H,12MH NO. TENSION OF X-COORD Y-COORD Y-COORD Z-COORD STR 534  
 1 OF 20RD )  
 600 FORMAT (1H,14.01X,6F9.2\*610\*2)  
 610 FORMAT (1H,11H,15HARFAY JUNCTIONS).  
 611 FORMAT (1H,15H-----/)

612 FORMAT (1H,27HJUNC. CABLE AT TENSION A1,3X,16HZANGLE WRT,STR 542  
 613 FORMAT (1H,27HJUNC. CABLE AT TENSION A1,3X,16HZANGLE WRT,STR 543  
 16A17HJUNCTION LOCATION)

622 FORMAT (1H,15H NC. JUNCTION 3X,8HJUNCTION X,16HZ-AXIS XY-PLANE STR 544  
 12.025H-X-COORD Y-COORD Z-COORD)  
 625 FORMAT (1H,27HJUNC. CABLE AT TENSION A1,3X,16HZANGLE WRT,STR 545  
 1X,17HJUNCTION LOCATION,9X,21HDISP FROM A1 CURRENT,4X,25HDISP FROSTR 546  
 2M ORIG NO CURRENT)  
 630 FORMAT (1H,15H NC. JUNCTION 3X,8HJUNC.110H4X,16HZ-AXIS XY-PLANE STR 549  
 12.025H-X-COORD Y-COORD Z-COORD,3X,24HX-UISP Y-OISP Z-DISP,3X,STR 550  
 22.4HX-UISP Y-OISP Z-DISP /-LISP)

635 FORMAT (1H,14.06X,12,4X,F10\*2\*2(3X,F7,2)\*4F9,2)  
 1LOCATION,13X,6HDEVICE,4X,6DEVICE,4X,6NORMAL,6X,4HTANG)  
 635 FCHMAT (1H,34HINCEX NO. COORDINATE DEVICE,5X,25HZ-COORD YSTR 556  
 1-COORD 2-COORD,8X,6H,8IGHT,4X,6LENGTH,3X,7HDRAUG CO,3X,7HDRAUG CO,STR 549  
 630 FORMAT (1H,7HDEVICE,5HCARL,6X,11H5,7X,10HTENSION AT 10X,15HDEVICESTR 560  
 1E LOCATION,12X,21HISP FROM NO CURRENT,8X,25HDISP FROM ORIG NO CUSTR 561  
 2HENT)  
 645 FORMAT (1H,34HINCEX NO. COORDINATE DEVICE,7X,25HZ-CUORD YSTR 563  
 1-CUGRU /-CCUHD,6X,24HX-UISP Y-OISP Z-DISP,6X,24HX-DISP Y-OISP Y-DISP STR 564  
 2SP Z-OISP)  
 670 FCHMAT (110) STR 565  
 675 FCHMAT (F4..A4,RE15.H) STR 567  
 680 FCHMAT (210,4E15.6) STR 568  
 685 FCHMAT (1H,14.04X,12,4X,F9,2\*1X,3F9,2\*4X,2F10,2,2F10,3) STR 569  
 690 FCHMAT (1H,14.04X,12,4X,F9,2\*3X,F9,2\*1X,3(3X,356,2) STR 570

SUBROUTINE SHROUT 74/74 OPT#1

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END

STR 571-

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

47 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
19 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
212 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
219 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
219 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
27 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
312 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
309 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.  
463 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

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SUBROUTINE SWITCH

74/74

OPT=1

03/07/80

11.41.06

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1      *UECK SWITCH
      SUBROUTINE SWITCH
      C
      C THIS ROUTINE SWITCHES INPUT DATA
      C
      COMMON /B1/ FEJUNC,IR,DELT1,DELT2,IJS,TFJUNC,E,ES,FCAB,RCAB,JUMP,SWT
      1PJUNC,PCABH,PCABE,PCABO,RCABH,RCABE,RCABO,TETA,PJUNC
      2COMMON /B2/ NCAB,NODE,ERJUNC,IRJUNC,DATN,M,PJUNC,DCAB,DCABH,SWT
      3 1FATE,NANG,ARJUNC,THEAD,IPRNT,INTAPE,OUTAPE,ITIME,IRLG,OFLG,NIR,THESWT
      4 2IAS,THETAE,CUMPD,THEIA,B,NJUNC,IRNO,TEST,ONYSEG,ZVEL,ZVELZ,PIPE,CICAB,SWT
      5 3EXP CAB,ZJUNC,IRJUNC,PATH,ICAB,IVOPT,W CAB,IDEV,ICHECK,NDATC,SWT
      6 4DIMENSION PJUNC(3,44), IR(3,44), IR(3,44), TFJUNC(3,44), PJUNC0(SWT
      7 5DIMENSION F CAB(3,51,22), RCAB(3,51,22)SWT
      8 6DIMENSION P CAB(3,51,22), PCAB(3,44), PJUNC(44), RCAB0(3,51,22)SWT
      9 7DIMENSION P JUNC(22), DCAB(22), ANJUNC(44), TEST(14)
      10 8DIMENSION ZVEL(25), CDCAB(22), DCAB(22), ANJUNC(44), TEST(14)
      11 9DIMENSION ZVEL(25), E,ES,FCAB(22), DCAB(22), ANJUNC(44), TEST(14)
      12 10DIMENSION L JUNC(22), EXP CAB(22), E,ES,FCAB(22), DCAB(22), ANJUNC(44)
      13 11DIMENSION ICHECK(44), PATH(22), ICAB(22), NCAB(22), 10EV(1000)
      14 12INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OF LG
      15 13REAL IR,IJS
      16 14DC 5 I=1,10
      17 15S DATI(1)=DATN(1)
      18 16RETURN
      19 17END
      20 18
      21 19
      22 20
      23 21
      24 22
      25 23
      26 24
      27 25
      28 26
      29 27
      30 28
      31 29
      32 30

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FUNCTION TANG 74/74 OPT=1

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1      *DECK TANG
2      FUNCTION TANG (I)
3
4      C THIS ROUTINE CALCULATES THE UNIT TANGENT TO A CABLE AT ANY POINT
5
6      COMMON /B3/ VELX(125),VELY(125)
7      COMMON /B1/ FEJUNC,IR,DELTA,IIRS,IFJUNC,E,ES,FCAB,RCAB,JUMP,TAN
8      COMMON /B2/ NCAB,NODE,ERJUNC,IR,DELTA,PCAB,RCAB,PIJUNC
9      COMMON /B2/ NCAB,NODE,ERJUNC,IR,JUNC,DATN,M,PJUNC,CDCAB,DCAB,TAN
10     JFATE,MANC,ANJUNC,READ,IPRINT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THEtan
11     ZTAS,THEJAE,COMPDTHETAB,MJUNC,RH0,TEST,MYSEG,ZVEL,VELZ,PIPECAB,TAN
12     3EXP,CAB,2JUNC,PATH,ICAB,IVOP,NCAB,IREV,ICHECK,IDEV,NDATC
13     DIMENSION FEJUNC(13,44), IRS(3,44), ITERS(3,44), PJUNC(13,44), PJUNC0(13,44)
14     13,44)
15     DIMENSION FCAB(3,51,22), RCAB(3,51,22), PJUNC(3,44), PCAB(3,51,22), TAN
16     1) DIMENSION PCABE(3,51,22), PCABO(3,51,22), RCABO(3,51,22)
17     DIMENSION NNODE(22), ERJUNC(44), IRJUNC(44), DATN(10), DATN(10), MTRAN
18     1(22)
19     1(22) DIMENSION PJUNC(13,44), DCAB(22), DCAB(22), ANJUNC(44), TEST(14)
20     20 DIMENSION ZVEL(125), VEL2(25), ECICAB(22), EXP CAB(22), ZJUNC(22)
21     21 DIMENSION LJUNC(22), PATH(22), ICAB(22), NCAB(22), IDEV(1000),
22     22 IDEV(1000), TAN
23     23 DIMENSION ICHECK(44)
24     24 INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
25     25 REAL IR,IIRS
26     26
27     27      N=DAT(1)
28     28      M=(DAT(10)/H(N))+1
29     29
30     30      C CALCULATE DISTANCE, SIGMA, OF POINT FROM NODE M
31     31      C SIGMA=DAT(10)-(M-1)*H(N)
32     32
33     33      C CALCULATE EXTRAPOLATION QUANTITIES
34     34
35     35      C EM=RCARI(1,M,N)/TCAB(M,N)
36     36      C EM1=RCAB(1,M+1,N)/TCAB(M+1,N)
37     37
38     38      C CALCULATE TANGENT
39     39
40     40      C TANG=EM*((EM1-EM)/H(N))*SIGMA
41     41      C RETURN
42     42
43     43-
```

SUBROUTINE TAPOUT 74/74 OPT=1

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1    \*DECK TAPOUT  
C    SUBROUTINE TAPOUT

C    THIS ROUTINE GENERATES THE TAPE OR CARDS GIVING  
C    THE LOCATIONS OF THE INDEXED DEVICES

C    COMMON /B3/ VELX(25),VELY(25)

C    COMMON /B1/ FEJUNC,IR,DELTAI,IRS,TFJUNC,E,ES,FCAB,RCAB,JUMP,TAP

C    1PJUNC,PCAB,PCABE,PCABO,RCABO,RCAB,PJUNC

C    COMMON /B2/ NCAB,ANODE,ERJUNC,IRJUNC,PJUNC

C    COMMON /B3/ NCAB,ANODE,ERJUNC,IRJUNC,PJUNC,DCAB,DCAB,TAP

C    IFATE,IVAN,ANJUNC,IREAD,IPRNT,INATE,OUTAPE,TIME,IFLG,NIR,THE,TAP

C    2TAS,THETAECOMP,DTHETAB,NJUNC,RHO,TEST,MSEG,ZVEL,VELZ,PIP,ECICAB,TAP

C    3EXP,CAB,LJUNC,PATH,ICAB,IVOP,WCAB,IDEV,ICHECK,NDEV,TAP

C    DIMENSION FEJUNC(3+44),IR(3+44),IRS(3+44),TFJUNC(3+44),PJUNC(3+44),TAP

C    15 DIMENSION FCAB(3+51+22),RCAB(3+51+22),PJUNC(3+51+22) TAP

C    16 PCAB(3+51+22),PCABO(3+51+22),RCABO(3+51+22) TAP

C    17 DIMENSION NNODE(22),ERJUNC(44),IRJUNC(44),DATN(10),DATN(10),HTAP

C    18 1(22) DIMENSION PJUNC(3+44),DCAB(22),ANJUNC(44),TEST(14) TAP

C    19 DIMENSION ZVEL(25),VELZ(25),ECICAB(22),EXPCAB(22),ZJUNC(22) TAP

C    20 DIMENSION LJUNC(22),PATH(22),ICAB(22),WCAB(22),IDEV(1000) TAP

C    21 DIMENSION ICHECK(44),DIMENSION PSPACE(13) TAP

C    22 INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG TAP

C    23 INTEGER PATH,PEAL,TIRS TAP

C    24 101=4 CUR TAP

C    25 102=AM DEV TAP

C    26 ID3=4H REC TAP

C    27 JUM=JUMP+1 TAP

C    28 GO TO (5+10),JUM TAP

C    29 5 WRITE (OUTAPE,35) 103,MDATC TAP

C    30 WRITE (OUTAPE,35) 101,JUMP,THTA TAP

C    31 GO TO 15 TAP

C    32 10 WRITE (OUTAPE,35) 101,JUMP,THTA TAP

C    33 15 IF (IDEV.EQ.0) GO TO 30 TAP

C    34 DO 25 NN=1,IDEV TAP

C    35 READ (INATE,40) (DATN(K),K=1,10) TAP

C    36 INDEX=DATN(5) TAP

C    37 CALCULATE LOCATION OF DEVICE IN SPACE TAP

C    38 DO 20 J=1,3 TAP

C    39 45 I=J TAP

C    40 PSPACE(I)=SPACE(I) TAP

C    41 WHILE (OUTAPE,35) ID2,INDEX,(PSPACE(I),I=1,3) TAP

C    42 25 CONTINUE TAP

C    43 30 CONTINUE TAP

C    44 REWIND INTAPE TAP

C    45 RETURN TAP

C    46 35 FORMAT (A4+14,A4+8,F15.8) TAP

C    47 END TAP

C    48 55 FORMAT (F4.0,A4+8,F15.8) TAP

C    49 56 TAP

	SUBROUTINE	TAPOUT	74/74	OPT <sub>1</sub>	FTN 4.6+433E	03/07/80	11.41.06	PAGE	2
CARD	NR.	SEVERITY	DETAILS	DIAGNOSIS OF PROBLEM					
33	1			AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.					

FUNCTION ICAB      74/74      OPT=1

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PAGE 1

```
*DECK ICAB
FUNCTION ICAB (M,K)
C THIS ROUTINE CALCULATES THE TENSION AT NODE M OF CABLE K
      COMMON /B3/ VELX(25),VELY(25)
      COMMON /B1/ FEJUNC,R,DELTA,IJS,TFJUNC,E,ES,FCAB,RCAB,JUMP,TCA
      1PJUNC,PCAB,PCABE,PCABU,RCABO,THETA,PJUNC,TCA
      2COMMON /B2/ NCAB,ANDE,ERJUNC,IRJUNC,DAIS,DATAH,PJUNC,DCAB,DCABO,TCA
      3IFATE,NANG,ANJUNC,IREAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THETCA
      42IAS,THETAL,CUNPD,IMTAB,NJUNC,RHO,TEST,NSSEG,ZVEL,VELZ,P,P,ECICAB,TCA
      53EXP CAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,NCAB,IDEV,ICHECK,NOEV,TCA
      6DIMENSION FEJUNC(3*44),IR(3*44),IR5(3*44),TFJUNC(3*44),PJUNC(1ICA
      713*44)
      8DIMENSION FCAB(3,51,22),RCAH(3,51,22),PJUNC(3,44),PCAB(3,51,22)ICA
      91)DIMENSION PCAB(3,51,22),RCAB(3,51,22),RCABO(3,51,22)
      10DIMENSION NJUNC(22),ERJUNC(44),TRJUNC(44),DATI(10),DATIN(10),HICA
      111(22)
      12DIMENSION PJUNC(3,44),CDCAB(22),DCAB(22),ANJUNC(44),TEST(14)
      131(22),ECICAB(22),EXPCAB(22),ZJUNC(22)
      14DIMENSION ZVEL(25),VELZ(25),ICAB(22),PATH(22),W CAB(22),IEVE(1000)
      151(22)
      16DIMENSION ICHECK(44)
      17INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
      18INTFGER PATH
      19REAL IJS,IJS
      20ICAB=SQRT((RCAH(1,M,K)*42+RCAB(2,M,K)**2+RCAB(3,M,K)**2)
      21
      22      RETURN
      23      END
```

FUNCTION VELOC 74/14 OPT=1

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```

1      *DECK VELOC (1,PSPACE)
C THIS ROUTINE SPECIFIES THE I COMPONENT OF THE CURRENT FIELD
C AT AN ARBITRARY POINT IN SPACE, PSPACE(1)
C
COMMON /B3/ VELX(25),VELY(25),
COMMON /B1/ REJUNC,IR,DELTA,IIRS,TJUNC,E,ES,FCAB,RCAB,JUMP,VEL
1P JUNC,PCAB,PLABE,PCAB0,RCAB0,THETA,PJUNC0
COMMON /B2/ NCAB,NODE,ERJUNC,TJUNC,DATI,DATN,M,PJUNC,CUCAB,DCAB,VEL
IFACE,MANC,ANJUNC,IREAD,IPHN,INTAPE,ITIME,IFLG,OFLG,NIR,TIMEV
ZIAS,THETAE,COMPD,THETAB,NJUNC,RHO,TEST,NSSEG,ZVEL,VELZ,PIP,ECICAB,VEL
3EXPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,NCAB,IDEV,ICHECK,NDATC,VEL
COMMON /PIBLK/ PI
COMMON /KITER/ KOUNTR,NIT,MAXITER,IARS(3,44),TJUNC(3,44),PJUNC0(VEL
DIMENSION FCA(13,51,22),RCAB(13,51,22),PJUNC(13,44),FCAB(3,51,22)VEL
1) DIMENSION PCAB(3,51,22),RCABU(3,51,22),PJUNC(44),TJUNC(44),PJUNC(10),VEL
1) DIMENSION MNUDE(24),ERJUNC(44),DATN(10),MVAL(10),VEL
1) DIMENSION PJUNC(3,44),CUCAB(22),DCAB(22),ANJUNC(44),TEST(14),
1) DIMENSION ZVEL(25),VEL2(25),ECICAB(22),EXP CAB(22),ZJUNC(22),VEL
1) DIMENSION LJUNC(22),PATH(22),ICAB(22),MCAB(22),IDEV(1000),VEL
1) DIMENSION ICHECK(44),VEL
1) DIMENSION PSPACE(3),VEL
1) INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG,VEL
1) INTEGER PATH,VEL
1) REAL IR,IRS,VEL
1) DIR=PI/180,VEL
1) PERCENTV=FLG,IINSTEP)/FLGA,IINSTEPS,VEL
1) T=THE(TAU)H,VEL
1) GO TO (5,5,40),1,VEL
1) 5 L=PSPACE(13),VEL
1) DC 10 KKK1,NSSEG,VEL
1) K=KK,VEL
1) IF (L.GT.ZVEL(K)) GO TO 10,VEL
1) GC TO 15,VEL
1) CONTINUE,VEL
1) VFPSSX=1.0E78*VELX(K),VEL
1) VFPSSY=1.0E78*VELY(K),VEL
1) GC TO 25,VEL
1) 15 IF (K.NE.1) GO TO 20,VEL
1) VFPSSX=1.0E78*VELX(K),VEL
1) VFPSSY=1.0E78*VELY(K),VEL
1) GC TO 15,VEL
1) SIGMA=2/ZVEL(K-1),VEL
1) SLOPXE=(VELX(K)-VELX(K-1))/(ZVEL(K)-ZVEL(K-1)),VEL
1) SLOPY=(VELY(K)-VELY(K-1))/(ZVEL(K)-ZVEL(K-1)),VEL
1) VFPSSX=1.0E78*(VELX(K-1)+SLOPXE*SIGMA),VEL
1) VFPSSY=1.0E78*(VELY(K-1)+SLOPY*SIGMA),VEL
1) 25 VNP=Sqrt(VFPSSX**2+VFPSSY**2),VEL
1) IF (VNP.SGT.0.0) VFI SX=0.000001,VEL
1) VELA14=N1(VFPSSX,VFPSSY)+1,VEL
1) GC TO 13,VEL
1) VFLUX=VPA(15,1)*FEMNTV,VEL

```

FUNCTION vFLOC	74/74	OPTR1	F1N 4.6.433E	03/07/80	11.41.06	PAGE
						2
60	RETUN					
	35 VELOC=VW*SIN(AN)*PEMCH1V					
	RETUN					
	64 VELUC=0.					
	RETUN					
	END					
	VEL 58					
	VEL 59					
	VEL 60					
	VEL 61					
	VEL 62					
	VEL 63-					

## CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

34	1	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
56	1	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

SUBROUTINE RLEVEL      74/74      UPT#1      F7N 4.6+433E      03/07/80      11.41.06      PAGE 1

```

1   *UELK RLEVEL
      SUBROUTINE RLEVEL (IR,IRW)
      C
      C ROUTINE TO READ CURRENT DATA FOR CURRENT OPTION 3
      C
      5   COMMON /BIN/ ISCH
      COMMON /CYEL/ VMAG(25,4),VDIR(25,4),ZPT(25,4),XPT(4),YPT(4),NPPS(4)
      IJNSTA
      10  COMMON /PCUR/ XNP1(4),YWP1(4)
      COMMON /TITLE/ TITLE(8),PHI,CUNITS,IUNIT,VELXP(25),VELYP(25)
      COMMON /B2/ NCABINCODE,ERJUNC,DATN,R,PJUNG,DCAB,DCAB,R
      IFATE,NANC,ANJUNC,IREAD,IPRN1
      COMMON /PIBLK/ PI
      DIMENSION NS(4)
      DIMENSION STORE(8)
      DIMENSION NRUCE(22),ERJUNC(44),DATN(10),DATN(10),MRKD
      1(22)
      15  DIMENSION PJUNC(3,44),DCAB(22),ANJUNC(44)
      IBAU
      20  DTR=PI/180.
      DC 20 J=1,NS1 A
      HEAD (IH,30) STORE
      WRITE (ISCH,30) IFORM,IRAD
      25  WRITE (ISCH,30) SIGHL
      DECUE (30,35,STORE) NS(J),NPPS(J),XNP1(J),YWP1(J)
      IF (XNP1(J).NE.0.0.R.YWP1(J).NE.0.) GO TO 5
      XPT(J)=0.
      YPT(J)=0.
      GC TO 10
      30  S=SIGN(XNP1(J))*2*YWP1(J)**2
      A=ATAN2(YWP1(J),XNP1(J))
      H=A*PI/180
      XPT(J)=W*COS(H)
      YPT(J)=W*SIN(H)
      LU
      35  DO 15 I=1,INF
      HEAD (IH,30) STORE
      WRITE (ISCH,30) IFORM,LUAD
      40  DECUE (40,10,STORE) NS(J),ZP1(I,J),VMAG(I,J),VCIR(I,J)
      45  VMAG(I,J)=VMAG(I,J)*CUNITS
      50  CONTINUE
      DC 25 J=1,NS1 A
      NF=NPPS(J)
      DC 25 I=1,INF
      55  VDIR(I,J)=360.*PHI-VDIR(I,J)
      RETURN
      C
      30  FORMAT (H410)
      35  FORMAT (F12.2,F10.0)
      40  FORMAT (15,5X,310.0)
      END
  
```

```

1      *DECK INVEL
2      SUBROUTINE INVEL (NM,PSPACE)
3      COMMON /ACEL/ X,Y,UUMV(9),VDR(4),YMG(4),
4      COMMON /PIBLK/ PI
5      DIMENSION W(3), FSPACE(3),
6      DIMENSION V(4), V2(4),
7      STAI(Y1,Y2)=Y1+(Y2-Y1)*H
8      X=PSPACE(1)
9      Y=PSPACE(2)
10     L=PSPACE(3)
11     DC 20 J=N14
12     NP=NPPS(J)
13     DO 5 I=NP
14     ZDIF=Z-2P1(I,J)
15     IF (.SDIF.GT.0.) GO TO 5
16     I2=I
17     I1=I-1
18     GC 10 10
19     5 CCNINUE
20     IF ((I.EQ.0) .OR. I.GT.15)
21     P=(Z-ZP1(I-1,J))/(ZP1(I,J)-ZP1(I-1,J))
22     VRG(J)=S1AT(VMAG(I-1,J)*MAG(I2,J))
23     VDR(J)=S1AT(VCR(I-1,J)/VIR(I-1,J))
24     60 TO 20
25     VRG(J)=VMAG(I2,J)
26     VDR(J)=VDRH(I2,J)
27     20 CCNINUE
28     NS=N1A-1
29     GC TU (25,45,50), NS
30     25 X1=XP1(1)
31     X2=XP1(2)
32     Y1=YP1(1)
33     Y2=YP1(2)
34     IF ((X1-X2.NE.0.0) .OR. Y1-Y2.NE.0.0) GO TO 30
35     X3=X
36     X3=X1
37     Y3=Y
38     GO TO 40
39     30 IF ((Y1-Y2.NE.0.0) .OR. Y3.Y1)
40     X3=X
41     SW2=-1./SW1
42     IF (SW2.LT.-5.0)
43     GC TU 40
44     35 SW1=(Y2-Y1)/(X2-X1)
45     SP1=(X2-Y1)/(X2-X1)
46     SW2=-1./SW1
47     SC5=SC5/S1
48     Y3=(X1+X2*Y1)*(X+SM1*Y1)/US
49     S1=SINT((X2-X1)**2*(Y2-Y1)**2)
50     S2=SINT((X3-X1)**2*(Y3-Y1)**2)
51     SC5=SC5/(VMG(2)-VMG(1)+VCR(1)+VUR(1))
52     V1(1)=S05*(VMG(2)-VMG(1)+VCR(1)+VUR(1))
53     V2(1)=S05*(VUR(2)-VCR(1)+VUR(1))
54     GC TU 55
55     45 CALL SET (1)
56     CALL CHAMEP (V(1))

```

2

PAGE

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SUBROUTINE LEVEL      74/74      OPT#1

```

      CALL SET (2)
      CALL CRAMER (V2(1))
      GC 10 55
      55 CALL SFT (1)
      CALL CRAMER (V1(1))
      CALL SET (2)
      CALL CRAMER (V2(1))
      CALL SET (3)
      CALL CRAMER (V2(2))
      CALL SET (4)
      CALL CRAMER (V1(2))
      CALL SET (5)
      CALL CRAMER (V1(3))
      CALL SET (6)
      CALL CRAMER (V2(3))
      CALL SET (7)
      CALL CRAMER (V2(4))
      CALL SFT (8)
      CALL CRAMER (V1(4))
      V1(1)=.25*(V1(1)+V1(2)+V1(3)+V1(4))
      V2(1)=.25*(V2(1)+V2(2)+V2(3)+V2(4))
      55 DIR=P1/180.
      TH=V2(1)*UH
      WH(1)=V1(1)*COS(TH)*1.688
      WH(2)=V1(1)*SIN(TH)*1.688
      WH(3)=0.0
      RETURN
      END

```

CAHN R. SEVERITY DETAILS      DIAGNOSIS OF PROBLEM

AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

31    1

SUBROUTINE SET 74/74 OPT=1

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1 CALL SET  
SUBROUTINE SET 11  
COMM1, /LEVEL, VMAG(25,4), VDIR(25,4), ZPT(25,4), XPT(4), YPT(4), NPPS(4)  
SET 2  
SET 3  
SET 4  
SET 5  
SET 6  
SET 7  
SET 8  
SET 9  
SET 10  
SET 11  
SET 12  
SET 13  
SET 14  
SET 15  
SET 16  
SET 17  
SET 18  
SET 19  
SET 20  
SET 21  
SET 22  
SET 23  
SET 24  
SET 25  
SET 26  
SET 27  
SET 28  
SET 29  
SET 30  
SET 31  
SET 32  
SET 33  
SET 34  
SET 35  
SET 36  
SET 37  
SET 38  
SET 39  
SET 40  
SET 41  
SET 42  
SET 43  
SET 44  
SET 45  
SET 46  
SET 47  
SET 48  
SET 49  
SET 50  
SET 51  
SET 52  
SET 53-

1, NSIA  
COMM1 /CLEAR / X1=Y1, X2=X3, Y1=Y2, X3, Y2=Y3, Z1,Z2,Z3, VDR(4), VMG(4)  
GO TO 15,10,20,25,30,35,40,1  
5 CONTINUE  
X1=XPT(1)  
X2=XPT(2)  
X3=XPT(3)  
Y1=YPT(1)  
Y2=YPT(2)  
Y3=YPT(3)  
Z1=VMG(1)  
Z2=VDR(2)  
Z3=VMG(3)  
RETURN  
10 CONTINUE  
Z1=VDR(1)  
Z2=VDR(2)  
Z3=VDR(3)  
RETURN  
15 CONTINUE  
X3=XPT(4)  
Y2=YPT(4)  
Z2=VDR(4)  
RETURN  
20 CONTINUE  
Z1=VMG(1)  
Z2=VMG(2)  
Z3=VMG(4)  
RETURN  
25 CONTINUE  
X1=XPT(3)  
Y1=YPT(3)  
Z1=VMG(3)  
Z2=VDR(2)  
Z3=VDR(4)  
RETURN  
30 CONTINUE  
X2=XPT(1)  
Y2=YPT(1)  
Z2=VDR(1)  
Z3=VDR(3)  
RETURN  
35 CONTINUE  
X2=XPT(1)  
Y2=YPT(1)  
Z2=VDR(1)  
Z3=VDR(3)  
RETURN  
40 CONTINUE  
Z1=VDR(4)  
Z2=VDR(1)  
Z3=VDR(3)  
RETURN  
45 CONTINUE  
Z1=VDR(4)  
Z2=VDR(1)  
Z3=VDR(3)  
RETURN  
50 CONTINUE  
Z1=VDR(4)  
Z2=VDR(1)  
Z3=VDR(3)  
RETURN  
END

SUBROUTINE CHAMER 74/74 (PPI=1

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```
1      *DECK CHAMER (ANS)
      SUBROUTINE CHAMER (ANS)
      COMMUN /CLEI/, X1, Y1, X2, Y2, X3, Y3, Z1, Z2, Z3, VMG(4)
      D=X1*(Y2*Z3-Z1*Z2)-Y1*(X2*Z3-X3*Z2)+Z1*(X2*Y3-Y2*X3)
      A1=(Y2*Z3-Y3*Z2)-Y1*(Z2-Z3)-Z1*(Y3-Y2)
      HN=X1*(Z2-Z3)+(X2*Z3-X3*Z2)/2/Z1*(X3-X2)
      CN=X1*(Y3-Z2)-Y1*(X3-X2)-(X2*Y3-Y2*X3)
      IF (A1.NE.0) GO 10
      A1=S=-14*X*Y/NCN
      RETURN
  5      S A1=1/1
      H=HN/0
      C=CN/D
      ANS=(1./C)*(1.+A*X+B*Y)
      RETURN
 10     FTN
```

```
15      CRA 1
      CRA 2
      CHA 3
      CRA 4
      CRA 5
      CRA 6
      CRA 7
      CRA 8
      CRA 9
      CHA 10
      CRA 11
      CRA 12
      CHA 13
      CRA 14
      CHA 15
      CHA 16-
```

ROUTINE SORT      74/74      OPT#1

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```
1      *DECK SCRT
      SLRQUTINE SORT (NUEV, INTAPE)
      SCMMUN /81/ FE_JUNC
      COMMUN /ANDG/ TCCAB(22)*TUDCAB(1000)
      DIMENSION DATIT(2150*10), FE_JUNC(3,44)
      EQUIVALENCE (DATIT(1),FE_JUNC(1))
      HEAD (INTAPE,70) (DATIT(1,1),J=1,10),I=1,NDEV
      C COUNT NUMBER OF DCAB CARDS
      C
10     K=0
      UO 5 I=1,NUEV
      IF (NUEV .EQ. 1) GO TO 40
      K=MDCAB+1
      5 CONTINUE
      NCABEK
      C
      C PLT JUNC CARDS AFTER DCAB CARDS
      C
      NCJNC=NDEV+NDCAB
      IF (INDJNC.EQ.0) GC 10 40
      K=MDCAB+1
      UC 20 I=1,NCAB
      UC (DATIT(1,2).NE.*HDJNC) GO 10 20
      10 IF (DATIT(K,2).NE.*HDJNC) GO 10 15
      15 IF (DATIT(K,2).NE.*HDJNC) GO 10 15
      K=K+1
      20 IF (K.EQ.NDEV) GO 10 25
      25 CONTINUE
      GC 10 10
      15 CALL SWAP (1,K)
      20 CONTINUE
      25 CONTINUE
      C SORT JUNC CARDS BY JUNCTION NUMBERS
      C
      IF (NUJNC.EQ.1) GC 10 40
      NS=NDCAB+1
      NC1=NUJNC-1
      UC 35 I=NS,ND1
      11=I+1
      UC 30 K=11,NUEV
      IF (DATIT(1,3).LE.DATIT(K,3)) GO TO 30
      CALL SWAP (1,K)
      30 CONTINUE
      35 CONTINUE
      40 CONTINUE
      IF (INDCAB.LE.1) RETURN
      C SORT DCAB CARDS BY CABLE NUMBER
      C
      NCABIT=NDCAIT
      UC 50 I=1,NCABIT
      11=I+1
      UC 45 K=11,NDCAIT
      IF (DATIT(1,3).LE.DATIT(K,3)) GC 10 45
      CALL SWAP (1,K)
      45 CONTINUE
      50 CONTINUE
      55 CONTINUE
      59 CONTINUE
```

SUBROUTINE SURT 74/14 UPI=1

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C SCR1 BY UNSTRIPPED VISITANCE FORM S=0 JUNCTION OF CABLE

```
60 DO 65 I=1,NDCAB1          SUR 58
      KSI=1                      SOR 59
      65 IF (UAR1(I,3).NE.DAT1(K,3)) GO TO 65
          IF (UAR1(I,10).LE.DAT1(K,10)) GO TO 69
          CALL SWAP (I,K)
66 K=K+1                      SUR 61
67 IF (K.GT.NDCAB) GC 10 65    SUR 62
       GC TO 55                  SUR 63
68 CONTINUE                     SUR 64
69 RETURN                       SUR 65
70 C 70 FORMAT (F4.0,A4,BFB,0)  SUR 66
    END                         SOR 67
                                SOR 68
                                SOR 69
                                SOR 70
                                SOR 71
                                SOR 72-
```

SUBROUTINE SWAP   74/74   OPT1=1

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```
*LECK SWAP
      SUBROUTINE SWAP (I,J,K)
      COMMON /B1/ FEJUNC
      COMMON /LANDCH/ TCCAB(22),TDDCAB(1000)
      DIMENSION DATIT(2150,10),TUDATA(10),FEJUNC(3,44)
      EQUIVALENCE (DATIT(1),FEJUNC(1))
      DC 5 J=1,10
      TDATA(J)=LATIT(I,J)
      LATIT(I,J)=DATIT(K,J)
      5 DATIT(K,J)=TUDATA(J)
      TEMP=TUDATA(I)
      TDDCAB(I)=TCCAB(K)
      TDDCAB(K)=TEMP
      RETURN
      END
```

15

```
      SWA 1
      SWA 2
      SWA 3
      SWA 4
      SWA 5
      SWA 6
      SWA 7
      SWA 8
      SWA 9
      SWA 10
      SWA 11
      SWA 12
      SWA 13
      SWA 14
      SWA 15-
```

SUBROUTINE UALATA 74/74 OPT=1

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```
1      *CHECK BADATA  
C  
C THIS SUBROUTINE PRINTS OUT THE INPUT DECK IF  
C AN ERROR HAS BEEN DETECTED. NOTES THE ERRORS  
C AND PRINTS THE TEXT DESCRIBING THE ERRORS  
C  
C DIMENSION IERR(58), TYPE(58), CARD(58)  
C DIMENSION ICAB(22), ICHECK(44), IRJUNC(44), DATIL(10), DAIN(10), HAD  
C 1(22)  
C DIMENSION PJUNC(3,44), DCAB(22), UCAB(22), ANJUNC(44)  
C COMMON /BLK/ ISCH  
C COMMON /B2/ NCABINODE, ERJUNC, RJUNC, DATN, PJPUNC, DCAB, HAD  
C IFATE, NAKC, ANJUNC, IREAD, IPNT  
C  
C DATA STATEMENTS  
C  
C DATA TYPE/3r 0,3r 1A,3H 1B,3H 1C,3H 1A,3H 1B,3H 1A,3H  
C 1 1B,3H 1C,3H 1E,3H 1F,3H 1G,3H 1A,3H 1B,3H 1C,3H 1C,3H  
C 2 1E,3H 1C,3H 1E,3H 1F,3H 1A,3H 1A,3H 1B,3H 1B,3H 1D,3H  
C 3 3,3H "A,3H 4B,3H 6A,3H 6A,3H 6A,3H 6B,3H 6A,3H 7,3H 2A,3H  
C 4 9,3H 11,3H 12A,3R 12B,3H 12C,3H 12A,3H 12B,3R 12A,3H 13,3H  
C 5 14B,3H 15,3H 16,3R 17,3H 18/  
C  
C DATA CARUN/4H 0H LUN/4H LUN/4H MNJNC/4H ANC/4H IR/4H IR/4H  
C 14P CAH/4H CAH/4H CAB/4H CAB/4H CAB/4H CAB/4H CAB/4H CAB/4H  
C 2CAH/4HUCAB/4HDCAB/4HUCAB/4HUCAB/4HDCAB/4HDCAB/4HDCAB/4H  
C 3,4H ANG/4H ANG/4H ANG/4H ANG/4H ANG/4H ANG/4H ANG/4H ANG/4H  
C 4CMB/4H VEL/4H VEL/4H VEL/4H VEL/4H VEL/4H VEL/4H VEL/4H  
C 5K,4H 1R/4H CAB/4HUCAB/4HDCAB/4HDCAB/4HDCAB/4HDCAB/4H  
C 6H 4P  
C  
C WRITE END OF FILE AND REWIND UNIT ISCH  
C  
C END FILE ISCH  
C  
C INITIALIZE ARRAY INDICATING ERROR TYPES  
C  
C NEWEST  
C DC 5 J=1,NER  
C S TERR(1)=0  
C  
C PRINT HEADER FOR ERRORS  
C  
C WRITE (IPRN1+365)  
C READ +0H(M) AND ERROR CODE FOR SUBSEQUENT CARD  
C  
C 1, PFLD (ISCH) 1FH(M),1HAU  
C 1F (ECF (ISCH)) 55,15  
C 15 IF ((HAU.M=1) TERMINAL)=1  
C 10 (20*20*20*25*30*35*40*45*50) . 1FH(M)  
C  
C 55 C 2, AND PRINT INPUT CARD TAGFS  
C 2, READ (ISCH,355) 1FH(M)
```

```
      WRITE (IPHNT,360) TITLE  
      GC TO 10  
  
C HEAD AND PRINT ERROR TYPES AND OTHER INFORMATION  
C  
25  WRITE (IPRNT,375) TYPE (IBAD)  
C  
30  READ (ISCR) IFJNC,IFRH0,NANC  
     WRITE (IPRNT,375) TYPE (IBAD),IFJNC,IFRH0,NANC  
      GC TO 10  
  
35  READ (ISCR) NCNM,IVOP1,NVSEG,NZL,NANG  
     WRITE (IPRNT,375) TYPE (IBAD),NCNM,IVOP1,NVSEG,NZL,NANG  
      GC TO 10  
  
40  REAU (ISCR) (ICAB(1),I=1,22)  
     WRITE (IPRNT,380) TYPE (IBAD),(ICAB(1),I=1,22)  
      GC TO 10  
  
45  READ (ISCR) (ICHECK(1),I=1,44)  
     WRITE (IPRNT,380) TYPE (IBAD),(ICHECK(1),I=1,44)  
      GC TO 10  
  
50  READ (ISCR) NCAB,NANC,NOJUNC,NIRC,NIR  
     WRITE (IPRNT,375) TYPE (IBAD),NCAB,NANC,NOJUNC,NIRC,NIR  
      GC TO 10  
  
C PRINT TEXT OF ERRORS  
C  
55  WRITE (IPRNT,370)  
      DC 350 L1,NH  
      IF (IERR(1).EQ.0) GO TO 350  
      WRITE (IPRNT,385) RPT(1),CARD(1)  
      GO TU 60,65,70,75,80,85,90,95,100,105,110,115,120,125,130,135,140  
      1,145,150,155,160,165,170,175,180,185,190,195,200,205,210,215,220,230  
      225,230,235,240,245,250,255,260,275,280,285,290,295,300,305  
      310,315,320,325,330,335,340,345), 1  
      60  WRITE (IPRNT,340)  
      GC TU 350  
      65  WRITE (IPRNT,345)  
      70  WRITE (IPRNT,400)  
      GC TU 350  
      75  WRITE (IPRNT,405)  
      GC TU 350  
      80  WRITE (IPRNT,410)  
      GC TU 350  
      85  WRITE (IPRNT,415)  
      GC TU 350  
      90  WRITE (IPRNT,420)  
      GC TU 350  
      95  WRITE (IPRNT,425)  
      GC TU 250  
      100  WRITE (IPRNT,430)  
      GC TU 250  
      105  WRITE (IPRNT,435)  
      GC TU 350  
      110  WRITE (IPRNT,440)  
      GC TU 350  
      115  WRITE (IPRNT,445)  
      GC TU 350  
  
      HAD 58  
      HAD 59  
      HAD 60  
      HAD 61  
      HAD 62  
      HAD 63  
      HAD 64  
      HAD 65  
      HAD 66  
      HAD 67  
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      HAD 69  
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      HAD 71  
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      HAD 103  
      HAD 104  
      HAD 105  
      HAD 106  
      HAD 107  
      HAD 108  
      HAD 109  
      HAD 110  
      HAD 111  
      HAD 112  
      HAD 113  
      HAD 114
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115	120	WHITE (IPRNI,450)	BAD 115
	GC TO 350		BAD 116
125	WHITE (IPRNI,455)		BAD 117
	GO TO 350		BAD 118
130	WHITE (IPRNI,460)		BAD 119
	GC TO 350		BAD 120
120	135 WHITE (IPRNI,465)		BAD 121
	GC TO 350		BAD 122
140	WHITE (IPRNI,470)		BAD 123
	GC TO 350		BAD 124
145	WHITE (IPRNI,475)		BAD 125
	GO TO 350		BAD 126
150	WHITE (IPRNI,480)		BAD 127
	GO TO 350		BAD 128
155	WHITE (IPRNI,485)		BAD 129
	GC TO 350		BAD 130
160	WHITE (IPRNI,490)		BAD 131
	GC TO 350		BAD 132
165	WHITE (IPRNI,495)		BAD 133
	GO TO 350		BAD 134
170	WHITE (IPRNI,500)		BAD 135
	GC TO 350		BAD 136
175	WHITE (IPRNI,505)		BAD 137
	GC TO 350		BAD 138
180	WHITE (IPRNI,510)		BAD 139
	GC TO 350		BAD 140
185	WHITE (IPRNI,515)		BAD 141
	GC TO 350		BAD 142
190	WHITE (IPRNI,520)		BAD 143
	GC TO 350		BAD 144
195	WHITE (IPRNI,525)		BAD 145
	GC TO 350		BAD 146
200	WHITE (IPRNI,530)		BAD 147
	GC TO 350		BAD 148
205	WHITE (IPRNI,535)		BAD 149
	GC TO 350		BAD 150
210	WHITE (IPRNI,540)		BAD 151
	GO TO 350		BAD 152
215	WHITE (IPRNI,545)		BAD 153
	GC TO 350		BAD 154
220	WHITE (IPRNI,550)		BAD 155
	GO TO 350		BAD 156
225	WHITE (IPRNI,555)		BAD 157
	GO TO 350		BAD 158
230	WHITE (IPRNI,560)		BAD 159
	GC TO 350		BAD 160
235	WHITE (IPRNI,565)		BAD 161
	GC TO 350		BAD 162
240	WHITE (IPRNI,570)		BAD 163
	GC TO 350		BAD 164
245	WHITE (IPRNI,575)		BAD 165
	GC TO 350		BAD 166
250	WHITE (IPRNI,580)		BAD 167
	GC TO 350		BAD 168
255	WHITE (IPRNI,585)		BAD 169
	GC TO 350		BAD 170
260	WHITE (IPRNI,590)		BAD 171

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164  
175  
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220  
225

3511  
265 WHITE (IPRNT,695)  
GC TO 350  
270 WHITE (IPRNT,630)  
275 WRITE (IPRNT,605)  
GC TO 350  
280 WRITE (IPRNT,610)  
GC TO 350  
285 WHITE (IPRNT,615)  
GC TO 350  
290 WRITE (IPRNT,620)  
GC TO 350  
295 WHITE (IPRNT,625)  
GC TO 350  
300 WRITE (IPRNT,630)  
GC TO 350  
305 WRITE (IPRNT,635)  
GC TO 350  
310 WRITE (IPRNT,640)  
GC TO 350  
315 WRITE (IPRNT,645)  
GC TO 350  
320 WRITE (IPRNT,650)  
GC TO 350  
325 WRITE (IPRNT,655)  
GC TO 350  
330 WRITE (IPRNT,660)  
GC TO 350  
335 WRITE (IPRNT,665)  
GC TO 350  
340 WRITE (IPRNT,670)  
GC TO 350  
345 WRITE (IPRNT,675)  
350 CONTINUE

C FORMATS

C RETURN

C  
355 FCHMAT (BA10)  
360 FCHMAT (1H\*1X,BA10)  
365 FCHMAT (1H\*1X,11H\*1H) CAHD\$ 35X\*5M6RUR,13X\*5M6RUR INFORMATION BAD 214  
370 FCHMAT (1H\*1X,4H\*1H) CAHD\$ 35X\*5M6RUR,13X\*5M6RUR INFORMATION BAD 215  
375 FCHMAT (1H\*1X,4H\*1H) CAHD\$ 35X\*5M6RUR,13X\*5M6RUR INFORMATION BAD 216  
380 FCHMAT (1H\*1X,4H\*1H) CAHD\$ 35X\*5M6RUR,13X\*5M6RUR INFORMATION BAD 217  
385 FCHMAT (1H\*1X,20H\*1F) IN10N OF ERRORS / HAD 218  
390 FCHMAT (1H\*1X,20H\*1F) IN10N OF ERRORS / HAD 219  
395 FCHMAT (1H\*1X,20H\*1F) IN10N OF ERRORS / HAD 220  
400 FCHMAT (5X,23H\*1ELU 6 NOT EQUAL 0 0H 1) HAD 221  
405 FCHMAT (5X,49H\*1ELU 8 NOT EQUAL 0 0H 1) HAD 222  
410 FCHMAT (5X,39H\*1ELU 3 UNQUOTED NUMBERS ASSIGNED TO EQUIPPED I/O UNITS) HAD 223  
415 FCHMAT (5X,39H\*1ELU 3 GREATER THAN 44 OR LESS THAN 20) HAD 224  
420 FCHMAT (5X,39H\*1ELU 3 GREATER THAN 44 OR LESS THAN 10) HAD 225  
425 FCHMAT (5X,39H\*1ELU 3 GREATER THAN 44 OR LESS THAN 10) HAD 226  
430 FCHMAT (5X,39H\*1ELU 3 GREATER THAN 44 OR LESS THAN 10) HAD 227  
435 FCHMAT (5X,39H\*1ELU 3 GREATER THAN 44 OR LESS THAN 10) HAD 228

420 FCHM41 (5X,17F FIELD 3 = FIELD 4) BAD 229  
 425 FORMAT (5X,45RFIELDS 3 OR 4 GREATER THAN 44 OR LESS THAN 1 ) BAD 230  
 430 FCHM41 (5X,38RFIELD 3 GREATER THAN 22 OR LESS THAN 1 ) BAD 231  
 435 FCHM41 (5X,17F FIELD 4 = FIELD 5) BAD 232  
 440 FCHM41 (5X,44RFIELDS 4 OR 5 GREATER THAN 44 OR LESS THAN 1 ) BAD 233  
 445 FCHM41 (5X,39RFIELD 7,8 OR 9 LESS THAN OR EQUAL TO 0) BAD 234  
 450 FCHM41 (5X,27RFIELD 10 OR 11 LESS THAN 0) BAD 235  
 455 FCHM41 (5X,35RFIELD 10=0 AND FIELD 11 NOT EQUAL 0 AND FIELD 11=0) BAD 236  
 460 FCHM41 (5X,35RFIELD 10 NOT EQUAL 0 AND FIELD 11=0) BAD 237  
 465 FORMAT (5X,39F FIELD 12 GREATER THAN 50 OR LESS THAN 1) BAD 238  
 470 FCHM41 (5X,38RFIELD 3 GREATER THAN 22 OR LESS THAN 1 ) BAD 239  
 475 FORMAT (5X,37F FIELD 4 GREATER THAN 2 OR LESS THAN 1) BAD 240  
 480 FCHM41 (5X,40F FIELD 5 GREATER THAN 1000 OR LESS THAN 1) BAD 241  
 485 FCHM41 (5X,46F FIELD 4=1 AND FIELD 9 LESS THAN OR EQUAL TO 0) BAD 242  
 490 FCHM41 (5X,33F FIELD 4=2 AND FIELD 9 NOT EQUAL 0) BAD 243  
 495 FCHM41 (5X,28RFIELDS 7,8 OR 10 LESS THAN 0) BAD 244  
 500 FCHM41 (5X,38RFIELD 3 GREATER THAN 44 OR LESS THAN 1 ) BAD 245  
 505 FCHM41 (5X,24F FIELD 7 OH 8 LESS THAN 0) BAD 246  
 510 FCHM41 (5A,19F FIELD 3 LESS THAN 0) BAD 247  
 515 FORMAT (5A,27F FIELD 3 NOT EQUAL 0.1\* OR 2) BAD 248  
 520 FCHM41 (5A,28RFIELD 3 LESS THAN OR EQUAL 0) BAD 249  
 525 FORMAT (5A,25F FIELD 5 LESS THAN FIELD 3) BAD 250  
 530 FORMAT (5X,30THE JUNCTION NUMBER ASSIGNED TO THE ANCHOR(FIELD 3) BAD 251  
 535 FORMAT (5X,30THE JUNCTION NUMBER ASSIGNED TO THE SEL JUNCTION (FIELD 3) BAD 252  
 540 FCHM41 (5A,19A TYPE 1 FIELD 5) ON A PRECEDING CAB CARD) BAD 253  
 541 HAS BEEN ASSIGNED TO A PRECEDING ANC CARD OR 5A,52HIO AN SEL JUNCTBAD 253  
 542 FCHM41 (5X,28F FIELD 4 LESS THAN OR EQUAL 0) BAD 254  
 543 FCHM41 (5X,30THE JUNCTION NUMBER ASSIGNED TO THE SEL JUNCTION (FIELD 3) BAD 254  
 544 FCHM41 (5A,19A TYPE 1 FIELD 5) ON A PRECEDING ANC CARD) BAD 255  
 545 FCHM41 (5X,82A TYPE 2 ERROR APPEARS ONLY IN CONJUNCTION WITH A CABAD 256  
 546 FCHM41 (5A,19A AND INDICATES THAT THE 5A,80HNUMBER ASSIGNED TO THE CABLE BAD 256  
 550 FCHM41 (5X,37THE JUNCTION NUMBER ASSIGNED IN FIELD 3 HAS BEEN ASSHAD 261  
 551 LIGNED IN FIELDS 3 OH 4 OF A PRECEDING IR CARD) BAD 262  
 555 FCHM41 (5A,31THE JUNCTION NUMBER ASSIGNED IN FIELD 4 HAS BEEN ASSBAD 263  
 556 FCHM41 (5A,31THE JUNCTION NUMBER ASSIGNED IN FIELD 3 OF A PRECEDING IR CARD) BAD 264  
 560 FCHM41 (5X,60R SOURCE UCK) BAD 265  
 565 FCHM41 (5X,64R DEM CARD HAS PREVIOUSLY APPEARED IN THE PARTICULARHAD 267  
 570 FCHM41 (5A,64R SOURCE UCK) BAD 268  
 575 FCHM41 (5A,64R CCMP CARD HAS PREVIOUSLY APPEARED IN THE PARTICULARHAD 269  
 580 FCHM41 (5A,65R SOURCE UCK) BAD 270  
 585 FCHM41 (5A,65R SOURCE UCK) BAD 271  
 590 FCHM41 (5X,77THE TWENTY FIVE VEL CARDS HAVE PREVIOUSLY APPEARED IN THE PARTICULARHAD 271  
 595 FCHM41 (5X,74THE 2 COORDINATE AT WHICH THE CURRENT VELOCITY IS SPHAD 272  
 600 FCHM41 (FIELD 3) HAS /5K,63HFEEN USED ON A PRECEDING VEL CARD IN HAD 274  
 605 FCHM41 (5A,65R SOURCE UCK) BAD 275  
 610 FCHM41 (5A,65R SOURCE UCK) BAD 276  
 615 FCHM41 (5A,65R SOURCE UCK) BAD 277  
 620 FCHM41 (5X,119COLUN UNDER THE CABLE AWAY SOURCE UCK(UR TAP). THE OTHER INFORMATION/BAD 278  
 625 ELEMENTS OF WHICH GIVE RESPECTIVELY THE NUMBER OF NJNC CARDS/5X,12HAD 281  
 630 FCHM41 (THE NUMBER OF OPEN CARDS READ, AND THE NUMBER OF ANC CARDS BAD 282  
 635 FCHM41 A ZERO ELEMENT IS AN EOFH(SEE CABLE AWAY SOURCE UCK) BAD 283  
 640 FCHM41 (5X,119TYPE B ERROR INDICATES A DISCONTINUITY IN NUMERIBAD 284  
 645 FCHM41 (5A,65R SOURCE UCK) THE OTHER INFORMATION COLUMN UNDER /5XHAN 285

6.121 THE ERROR MEADING CONTAINS A 1X22 MATRIX, THE ELEMENTS OF WHICH  
 EACH CONTAIN ONE OR ZERO INDICATING, RESPECTIVELY, THE USE OR /SX, 12HAD 286  
 47-NON-USE OF THE CORRESPONDING COLUMN NUMBER AS A CABLE NUMBER. ZEHAD 288  
 600S INSTEAD OF THE CORRESPONDING COLUMN NUMBER. ZEHAD 289  
 600S FORMAT (5X,11H) TYPE 9 ERROR INDICATES A DISCONTINUITY IN NUMBERHAD 290  
 600S UNDER THE ERROR MEADING CONTAINS A X44 MATRIX, THE ELEMENTS OF WHICH  
 WHICH CONTAIN ONE OR ZERO INDICATING RESPECTIVELY. THE /SX,113MUSHAD 292  
 \*E OR NON-USE OF THE CORRESPONDING COLUMN NUMBER AS A JUNCTION NUMBERHAD 293  
 SER. ZEROS INTERFACED WITH ONES ARE IN LFIUS/SX,72H(SEE ARRAY DESBAD 295  
 DESCRIPTION AND REDUCTION TO A STATICALLY DETERMINATE ARRAY.) HAD 296  
 605 FORMAT (5X,11H) TYPE 11 ERROR INDICATES AN IMPROPER REDUCTION OF HAD 297  
 THE ORIGINAL CABLE ARRAY TO A STATICALLY UNTERMINATE ARRAY ON AN /HAD 298  
 25X,124ABSENCE OF CERTAIN INPUT CARDS IN THE CABLE ARRAY SOURCE DESBAD 299  
 JCK (HR TAPE). THE OTHER INFORMATION COLUMNS UNDER THE ERROR MEADING/HAD 300  
 45X,122HCOUNTS A 1X5 MATRIX. THE ELEMENTS OF WHICH GIVE, RESPECHAD 301  
 SIVELY, THE NUMBER OF CARDS READ. THE NUMBER OF ANC CARDS /SAHAI 302  
 6.121MREAL. THE NUMBER OF JUNCTIONS IN THE ORIGINAL CABLE ARRAYS (FIEHAD 303  
 TLU 3 OF THE NWC CARD), THE NUMBER OF REQUIRED CUTS (EQ.(11))/SX,11HAD 304  
 BY CALCULATED FROM THE PRECEDING INFORMATION, AND THE NUMBER OF IR HAD 305  
 SCADS HEAD. COLUMN 5 NOT EQUAL TO COLUMN 4 IS AN EPROM /SA,5HISTEHAD 306  
 S REDUCTION TO A STATICALLY DETERMINATE ARRAY.)  
 610 FORMAT (5X,11H) THE JUNCTION NUMBER ASSIGNED IN FIELD 3 IS LESS THANAD 307  
 IN OR EQUAL TO THE NUMBER OF JUNCTIONS IN THE ORIGINAL /SX,43HUNHEBAD 309  
 DUCED) ARRAY (FIELD 3 OF THE NWC CARD)) HAD 310  
 615 FORMAT (5X,11H) THE JUNCTION NUMBER ASSIGNED IN FIELD 3 IS GREATER HAD 311  
 IN OR EQUAL TO THE NUMBER OF JUNCTIONS IN THE ORIGINAL (REDUCED) ARRAYS/X,BAN 312  
 259MPLUS THE NUMBER OF CUTS MADE IN REDUCING THE ARRAY (EQ.(11)) HAD 313  
 624 FORMAT (5X,11H) THE JUNCTION NUMBER ASSIGNED IN FIELD 4 IS GREATER HAD 314  
 IN OR EQUAL TO THE NUMBER OF JUNCTIONS IN THE ORIGINAL (REDUCED) ARRAYS HAD 315  
 625 FORMAT (5X,12H) THE JUNCTION NUMBER ASSIGNED IN FIELD 4 IS GREATER HAD 319  
 IN OR EQUAL TO THE NUMBER OF CUTS MADE IN REDUCED /SX,92PRAHAD 317  
 DAY (FIELD 3 OF THE NWC CARD) PLUS THE NUMBER OF CUTS MADE IN REDUHAD 318  
 SCING THE ARRAY (EQ.(11)) HAD 319  
 630 FORMAT (5X,12H) THE CABLE NUMBER ASSIGNED IN FIELD 3 DOES NOT CORREBAD 320  
 SPOND TO A CABLE NUMBER ASSIGNED TO A CABLE (FIELD 3 OF THE CAR CABAD 321  
 PHCS)) HAD 322  
 635 FORMAT (5X,11H) THE DISTANCE OF THE DISCRETE DEVICE FROM THE S=0 JUHAD 323  
 LOCATION OF THE CABLE (FIELD 10) IS GREATER THAN OR EQUAL TO /SX,6JHAD 324  
 2THE LENGTH OF THE CABLE PENDING CABLE (FIELD 9 OF THE CAB CARD) HAD 325  
 649 FORMAT (5X,11H) THE JUNCTION NUMBER ASSIGNED IN FIELD 3 DOES NOT CUHAD 326  
 RESPOND TO EITHER A JUNCTION NUMBER ASSIGNED IN AN ANCHOR/SX,114HAD 327  
 C(FIELD 3 OF THE ANC CABLES) OR A JUNCTION NUMBER ASSIGNED TO AN SELHAD 328  
 3 JUNCTIONS OF A CABLE (FIELD 4 OF THE CAB CABNS).) HAD 329  
 645 FORMAT (5X,11H) TYPE 13 ERROR INDICATES THAT THE ORIGINAL CABLE AHAD 330  
 IPPEY HAS BEEN PROBABLY REFLECTED TO A STATICALLY /SX,10,114TEWMHAD 331  
 STATIC ARRAY SUCH THAT JUNCTIONS HAVE BEEN INAPPROPRIATELY NUMBERED. THE ORHAD 332  
 3THE INFORMATION, COLUMN NUMBER /SX, YPH THE FINE PRINT READING CONTAIHS THEHAD 333  
 MESSAGE, "IN PAPER ARRAY CONNECTION OR JUNCTION NUMBERING". CHUCK THEHAD 334  
 SE/SX,114HAD 335  
 659S MANTAB AGAINST JUNCTION NUMBERING IN AND ANC CAB CABNS.) HAD 336  
 659 FORMAT (5X,112H) TYPE 14 ERROR INDICATES AN INAPPROPRIACY OF INFORMATION HAD 337  
 LICH IN A STATICALLY STATIC SOURCE DECK. THE /S THE INFORMATION /SX,BAD 338  
 222COLUMN. WHETHER IT FOLLOWS IN THIS CONTAINS A 1 X NARROW. THE ELHAD 339  
 340 ELEMENTS OF WHICH MUST BE IDENTICAL. THE LENGTH OF CABLES/SX,121HAD 340  
 4HEDAD, THE CABLES PENDING CABLES, THE NUMBER OF VIL CARDS/WAD, THEHAD 341  
 S NUMBER OF VIL CARDS CURTAINS. A /COPROCESSOR (TRFL 3) /S,114TEWMHAD 342

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- LESS THAN OR EQUAL TO THE MINIMUM Z COORDINATE TRANSMITTED BY THE ANBAD 343  
TC CARDS (IFL1 6 OF THE AVE CARD), AND THE /5X.125HUMMER OF ANG CABAD 344  
THAT READING /5X.125HUMMER COLUMN 3 CONTAINS A ZERO. THEN A CMMY CALU MASHAD 345  
9 NOT APPEARED IN THE FIRST FEAT. AND USES PARAMETRIC STUDY SOURHAD 346  
SCE DECKS.)  
655 FORMAT (5X.1125HA TYPE 14 ERROR INDICATES AN INADEQUACY OF INFORMATION HAD 348  
LIGN IN A PARAMETRIC STUDY SOURCE DECK. THE OTHER INFORMATION /5X.1BAD 349  
5MNCOLUMN UNDER THE ENBLU READING CONTAINS A 1 X 5 MATRIX. THE ELLBAD 350  
5MENTS OF WHICH GIVE, RESPECTIVELY, THE NUMBER OF CAMP CARS /5X.121HAD 351  
4HREAD. THE CURRENT FIELD POSITION. THE NUMBER OF VEL CARUS HEAD. THE BAD 352  
5 NUMBER OF VEL CARS OF LENGTH A Z COORDINATE (IFLU 3) /5X.111HAD 353  
LESS THAN OR EQUAL TO THE MINIMUM Z COORDINATE TRANSMITTED BY THE ANBAD 354  
7C CARDS (IFL1 6 OF THE AVE CARD), AND THE /5X.125HUMMER OF ANG CABAD 355  
BICS READ./5X.1125HA TYPE 2 CONTAINS A ONE AND ANY OF COLUMNS 3,4HAD 356  
9.0 UN'S CULTAIN A ZERO. WITH THE STANDARD CURRENT FIELD HAS NOT HELBAD 357  
IN /5X.125HUMMER FORMULATED (SEE PARAMETRIC STUDY SOURCE DECKS ANBAD 358  
SU STANDARD CURRENT FIELD).  
660 FCHM1 (5X.106HA TYPE 15 ERROR INDICATES THAT AN UNPERMITTED CHANGBAD 360  
1E HAS BEEN ATTEMPTED IN A PARAMETRIC STUDY SOURCE DECK. /5X.136H(STERHAD 361  
2 PARAMETRIC STUDY SOURCE DECKS.)  
665 FCHM1 (5X.114HA TYPE 16 ERROR INDICATES AN IMPROPER DECK STRUCTUREHAD 363  
1E. SEE CABLE ARRAY SOURCE DECK, PARAMETRIC STUDY SOURCE DECKS./5XBAD 364  
670 FCHM1 (5X.101HA TYPE 17 ERROR INDICATES THAT THE CABLE ARRAYS HAD 365  
ACE DECK (CW TAPE) CONTAINS MORE THAN 400 RECORDS./5X.19 THE OTHERHAD 366  
2H INFORMATION COLUMN UNDERR THE ERROR READINGS CONTAINS THE MESSAGE HAD 368  
3CCM1 (5X.114HA TYPE 18) MOUTH EXCEEDED. SEE USERS MANUAL./5X.125HA TYPE 17 EHBBAD 369  
4UR IS READILY CORRECTABLE IF THE MACHINE BEING USED HAS SUFFICIENTHAD 370  
5 CORT STURGE. THIS CUMULATON IS ACHIEVED BY /5X.124HCHANGING THEBAD 371  
6 HUN DIMENSION OF DATA ON CARDS DE025 AND INP022 FROM 2150 TO A BAD 372  
7NUMBER EXCEEDING THE NUMBER OF RECORDS IN THE /5X.123HCARLLE ARRAYS HAD 373  
ESCAPE DECK (CW TAPE). SUPPLY TANDEMUSLY, THE COMPARISON VALUE ON CABAD 374  
9U INPUTS MUST BE CHANGED FROM 2150 TO THE NEW /5X.23HUN DIMENSION HAD 375  
8OF DATA.)  
675 FCHM1 (5X.108HA TYPE 18 ERROR INDICATES THAT THE ACCURACY REQUIREBAD 377  
1U FOR THE AVEAY EQUILIBRIUM CALCULATIONS (FIELD 3 OF THE /5X.9ACOBAD 378  
2MP CARD) HAS NOT BEEN OBTAINED DURING THE CALCULATIONS. THIS IS FOHAD 379  
3H ONE OF TWO POSSIBLE PROBLEMS./5X.114HA. SOME CABLE ELEMENTS MAYHAD 380  
4F GONE SLACK (THIS IS THE STEPPING HAVE MEAN ZERO TENSION. AN EXAMHAD 381  
5IATION OF THE TENSION /5X.1125PRINTED OUT IN CONJUNCTION WITH A BAD 382  
6FE 1A FEAT. WILL REVEAL IF THIS IS THE REASON. IF IT IS, SEE THAT HAD 383  
7SECTION OF /5X.91INSTANT CALL UNSTABLE CABLE ARRAYS IN HFT. 2 FOR HFTAN 384  
8HISSELF MEDICAL ACTIONS. IF IT IS NOT THEN /5X.125H. THE ACCURABAD 385  
9CY REQUESTED FOR THE EQUILIBRIUM CALCULATIONS IS SIMPLY TUU STRINGEBAD 386  
101 FHT THE COMPUTER TO PRINT (SEE COMP CARD)./5X.120HAN EXAMINAHAD 387  
11SU OF THE FINAL VALUE OF THE ACCURACY OBTAINED, PRINTED OUT IN COMBAD 388  
12JUNCTION WITH A TYPE 18 ENHGT. WILL HELBAD /5X.102H THE HFT ACCURACHAD 389  
13Y OHTAERLE. FIELD 3 OF THE CAMP CARD SHOULD BE MODIFIED TO REFLEHAD 390  
14U THIS INFORMATION.)  
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1      *ECK CPLT
      *ROUTINE CPLT (IVOPT,IPHNT,PJUNC,NANC,TITLE,ANJUNC)
      COMMON /CPT/ ZUP,ZDN,DZ,XMIN,XMAX,YMIN,YMAX,YIN,ANG,XY,
      CCHMNC/PIBLK/ PI
      DIMENSION PJUNC(3,44), ANJUNC(44)
      DIMENSION X(100), Y(100)
      DIMENSION PSPACE(3), W(3), TITLE(8)
      INTEGER ANJUNC
      C
      C SET UP PERSPECTIVE TRANSFORMATIONS
      C
      C UP(XP*YP)=XP+YP*EX
      C VP(TP)=YP*EX
      C
      C INITIALIZATION
      C
      C UTHEPI/180.
      C EX=COS(ANG*UTR),
      C EY=SIN(ANG*UTR),
      C HGT=0.07
      C
      C CALCULATE SPACE BETWEEN PLOTS
      C
      C NZ=(ZUP-ZDN)/DZ+1.00001
      C PIN=YIN
      C TY=NZ*PIN
      C SPACE=(10.-TY)/(NZ+1)
      C IF (SPACE.GT.0.) GO TO 5
      C WRITE (IPHNT,75)
      C RETURN
      C CONTINUE
      C GET COORDINATES
      C
      C NY1=NY-1
      C DEL1=YIN/NY1
      C DELU=(YPAK-YMIN)/NY1
      C NX=(XPAK-XMIN)/DELU+2.00001
      C IF (NX.GE.3) GO TO 10
      C WRITE (IPHNT,80)
      C RETURN
      C NX=NX-1
      C XIN=DELI*NX1
      C DC15=T=1.04X
      C 15 X((I)=XMIN+(T-1)*DELU
      C DC20 T=1.04Y
      C 20 Y((I)=YMIN+(T-1)*DELU
      C
      C OFF THE SCALE IN UNITS PTH INCH
      C
      C SCALE=DELL/ELI
      C
      C FIND NORMALIZATION FACTOR FOR CURRENT
      C
      C SMAX=0.
      C UC 40 K=1,42
      C PSPACE(3)=LN+(K-1)*UC
      C
      C FINISH DRAWING (DO NOT USE THIS LINE)
      C
      C

```

\*IN PLOT1 (24,45,46,47,48,49,50,51,52,53,54,55,56,57) IS UNPAGED FROM 44 IN LTSS (MAN 1)

MAP 228

SUBROUTINE CPL1

FIN 4.6\*433E

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60      C      LCOF ON X AND Y          CPL 58
      C      DC 35 I=2,NX1          CPL 59
      C      DC 35 J=2,NY1          CPL 60
      C      PSPACE(1)=X(1)          CPL 61
      C      PSPACE(2)=Y(J)          CPL 62
      C      IF ((IVOPTONE=3)) GO TO 25          CPL 63
      C      CALL INTVEL (NM,PSPACE)          CPL 64
      C      XA=MW(1)          CPL 65
      C      YA=MW(2)          CPL 66
      C      GC TO 30          CPL 67
      C      25 XA=VELOC(1,PSPACE)          CPL 68
      C      YA=VELOC(2,PSPACE)          CPL 69
      C      DC 70 K=1,MZ          CPL 70
      C      S=SQR((XA**2+YA**2)          CPL 71
      C      SMAX=AMAX1(SMAX,S)          CPL 72
      C      CCINUE          CPL 73
      C      SD=0.50*AEL1/SMAX          CPL 74
      C      GC TO 30          CPL 75
      C      70  C      INITIALIZE AND SET PEN POSITION          CPL 76
      C      YC=SPACE          CPL 77
      C      CALL PL01 (0.0,Y0,-3)          CPL 78
      C      DC 70 K=1,MZ          CPL 79
      C      LOOP ON DEPTH LEVELS          CPL 80
      C      PSPACE(3)=ZDN+(K-1)*DZ          CPL 81
      C      C      LABEL DEPTH LEVEL AND INDICATE X-AXIS          CPL 82
      C      IF (K*EG=1) GC TO 45          CPL 83
      C      YC=PIN*SPACE          CPL 84
      C      CALL PL01 (C.0,Y0,-3)          CPL 85
      C      DRAW BOY          CPL 86
      C      75  C      45 CALL PL01 (6.0,0.0,3)          CPL 87
      C      PX=UP(0,Y1N)          CPL 88
      C      PY=VP(Y1N)          CPL 89
      C      CALL PL01 (PX,PY,2)          CPL 90
      C      PX=UP(X1N,Y1N)          CPL 91
      C      CALL PL01 (PX,PY,2)          CPL 92
      C      CALL PL01 (X1N,0.0,2)          CPL 93
      C      CALL PL01 (0.0,Y1N)          CPL 94
      C      PY=VP(Y1N)          CPL 95
      C      CALL PL01 (0.0,0.0,2)          CPL 96
      C      XN=0.5*(X1N+PX)+0.025          CPL 97
      C      TN=0.5*(PI-PI1)          CPL 98
      C      CALL NUMHEH (XN,YN,PI1,(SPACF(3),0.0,0.0)          CPL 99
      C      CALL SYMBOL (X1N+0.25,(C.0,Y1N),1,MX,0.0,1)          CPL 100
      C      CALL SYMBOL (0.25,0.0,PI1,MX,0.0,1)          CPL 101
      C      80  C      PRINT SYMBOL AT EACH ARROW POINT          CPL 102
      C      XC = C.0, YC = 1.0,MX          CPL 103
      C      ZN=UP(C.0,Y1N)          CPL 104
      C      TN=(P.0,NC(1,0L))-YMIN/SCALE          CPL 105
      C      YDN=(P.0,NC(0,0L))-YMIN/SCALE          CPL 106
      C      PY=VP(Y1N)          CPL 107
      C      85  C      GC TO 30          CPL 108
      C      90  C      GC TO 30          CPL 109
      C      95  C      GC TO 30          CPL 110
      C      100  C      GC TO 30          CPL 111
      C      105  C      GC TO 30          CPL 112
      C      110  C      GC TO 30          CPL 113
      C      115  C      GC TO 30          CPL 114
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SUMMARY LINE CPLI 74/74 00121

FIN 4060433E

PAGE 3

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CPL 115
IF (XAN.GT.XIN.OH.XAN.LI.0.) GO TO 50
IF (YAN.LT.YIN.OH.YAN.LI.0.) GO TO 50
CALL SYMBOL (PAO,PYO,PGI,11,0,0,-1)
CONTINUE

120 C
C LOUP UN X AND Y
C
C DC 65 I=2,NX1
DC 65 J=2,NY1
PSPACE(I)=A(1)
PSPACE(I2)=Y(J)
IF (IVOF1*JLT3) GO TO 55
CALL NIVEL (NW,PSPACE)
XA=WW(1)*SU
YA=WW(2)*SU
UC TU 60
55 X=VELOC(I2,FSFACE)*SD
YA=VELOC(I2,FSFACE)*SD
CALL PLOT (FX1,FY1,3)
C
C DRAW ARROW
C
C CALCULATE DISTANCE FROM XMIN,YMIN TO TAIL OF ARROW (INCHES)
C
C DC X5=(X1)-XMIN)/SCALE
DC Y5=(Y1)-YMIN)/SCALE
P1=UP(X5,Y5)
PY1=VP(Y5)
CALL PLOT (FX1,FY1,3)
C
C CALCULATE DISTANCE FROM XMIN,YMIN TO HEAD OF ARROW (INCHES)
C
C XF=Y5+YA
YC=Y5+YA
YC=UP(XE,YF)
F1=VP(FY1)
CALL PLOT (FX2,PFY2,2)
C
C DRAW ARROW HEAD
C
C DC X=F1-X-FX1
DC Y=Y2-PY1
ARBLT=ATAN2(DY,DX)/DEG-90.
HCSE=0.2857431*(X**2+Y**2)
CALL SYMBOL (RAZ,RY2,HCSE,6,ANGLE,-1)
US CONTINUE
CONTINUE
C
C PLOT TITLE
C
C YC=INCR*SPACE
CALL SYMBOL (0,0,YC,11,LT,0,80)
C
C LEFT MIGHT FOR FXT PLOT
C
C XC=Z*W1
YC=(N2-1)*(1+SPACE)*SPACE
CPL 121
CPL 122
CPL 123
CPL 124
CPL 125
CPL 126
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CPL 128
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FIN 4.6431E

SUBROUTINE PLT 74/14 OPT#1

```
CALL PLT (X0,Y0,-3)
RETURN
C
175  IS FORMAT // / / X , 57H TOTAL HEIGHT OF PLOT EXCEEDS 10. INCHES. PLOT NOCPL
      IF CHEATED // / , NO PLOT NOCPL 175
      OR FORMAT // / / X , WANT NUMBER OF GRID POINTS IN THE X DIRECTION IS LCPL 177
      LESS THAN 3, TO CORRECT THIS INCREASE NY///). CPL 178
      FN4
176
177
178
179
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SOURCELINE #EPLI 74/74 OPI=1

TIN 4064334F 03/07/80 1104106

PAGE 1

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1      *11.C. EPLI
2      SUBROUTINE EPLI (IVOPT,NCAB,NNODE,PCAB,PCAHO,TITLE)
3      DIMENSION N(112), NPAK(114), X(2200), Y(2200), Z(2200),
4      DIMENSION PCAB(3,51,22), PCAHO(3,51,22), KNODE(22),
5      LC4RDN /PLT/, KPLI, SIZT, IH(3), IVOPT, KCP1,
6      DATA HED/0M ,6H ,6H ,6H ,6H ,6H ,6H ,6H ,6H ,6H ,
7      IVOPT=1 , 6H ,6H ,6H ,6H ,6H ,6H ,6H ,6H ,6H ,
8      IVOPT=2 , 6H ,6H ,6H ,6H ,6H ,6H ,6H ,6H ,6H ,
9      INITIAZT
10     C      ULMRYAN.
11     C      NELTYPE1
12     C      RTHELU
13     C      REWIND N1E
14
15     C      PUT UNREFINED COORDINATES FROM PCAB IN X,Y,Z
16     C      PUT UNREFINED COORDINATES FROM PCABO IN X,Y,Z
17     C      DEFINE NUMBER OF NODAL POINTS NUMNP
18     C      DEFINE NUMBER OF ELEMENTS NEL
19     C
20     C      HEL=0
21     C      IF (IVOPT.EQ.0) GC TO 5
22     C      IF (IVOPT.EQ.1) GC TO 20
23     C      UNREFINED
24     C      5  NC 15  N=1,1,CAH
25     C      MN=MNOUT(N)
26     C      NC 15  M=1,1,CAH
27     C      NMNP=NUMNP+1
28     C      X(NUMNP)=CAB(1,1,M,N)
29     C      Y(NUMNP)=CAB(2,1,M,N)
30     C      Z(NUMNP)=CAB(3,1,M,N)
31     C      IF (M>6) .OR. N>1,1,CAH(M,N)
32     C      MN=MNOUT(N+1)
33     C      X(NUMNP)=PLAB(1,1,M,N)
34     C      Y(NUMNP)=PLAB(2,1,M,N)
35     C      Z(NUMNP)=PLAB(3,1,M,N)
36     C      1L  IF (M>6 .OR. N>1,1,CAH(M,N))
37     C      MN=MNOUT(N+1)
38     C      1L  IF (M>6 .OR. N>1,1,CAH(M,N))
39     C      MN=MNOUT(N+1)
40     C      1L  IF (M>6 .OR. N>1,1,CAH(M,N))
41     C      MN=MNOUT(N+1)
42     C      1L  IF (M>6 .OR. N>1,1,CAH(M,N))
43     C      MN=MNOUT(N+1)
44     C      1L  IF (M>6 .OR. N>1,1,CAH(M,N))
45     C      MN=MNOUT(N+1)
46     C      UNREFINED
47     C      UN=M1,M,N
48     C      UN=M1,M,N
49     C      UN=M1,M,N
50     C      UN=M1,M,N
51     C      X(NUMNP)=CAB(1,1,M,N)
52     C      Y(NUMNP)=CAB(2,1,M,N)
53     C      Z(NUMNP)=CAB(3,1,M,N)
54     C      IF (M>6) .OR. N>1,1,CAH(M,N)
55     C      MN=MNOUT(N+1)
56     C      X(NUMNP)=PLAB(1,1,M,N)
57     C      Y(NUMNP)=PLAB(2,1,M,N)

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LINIE PEMP1

FIN 4.06.433E

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PAGE 2

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2 (N1,N2)=PCABU(3,0,N)
25 IF (N>CG+JNAN) GO TO 30
      NEL=TITLE+1
34 CONTINUE
35 CC+LINE

C GENERATE TAPE FILE
C
65 C
      WRITE (N1,E) (I+L1(K),K=1,12),NUMNP,NETLTP
      WRITE (N1,E) DUMMY
      WRITE (N1,E) (X(IK),K=1,NUMNP)
      WRITE (N1,E) (Y(IK),K=1,NUMNP)
      WRITE (N1,E) (Z(IK),K=1,NUMNP)
      WRITE (N1,E) DUMMY
END FILE N18
NPAR(1)=1
NPAR(2)=NEL
NPAR(3)=1
NPAR(4)=1
NPAR(5)=1
UC 40 I=6,14
40  (NPAR(1)=0
      WRITE (N1,E) (NPAR(K),K=1,14)
      WRITE (N1,E) DUMMY
      WRITE (N1,E) DUMMY
      WRITE (N1,E) DUMMY
      WRITE (N1,E) DUMMY
UC 45 I=1,NFL
      K1=2**1-1
      KJ=K1+1
45  WRITE (N1,E) I,K1,KJ
      FFIND NFL
      CALL SSF (TITLE)
      RETURN
END
```

SUBROUTINE SSP

74/14 OPT=1

F7W 4.6+433E

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PAGE 1

```
1      *BLOCK SSP           SSP 1
      C   SUBROUTINE SSP (MED)
      C
      C   DIMENSION MED(8), NF(18)
      C   DIMENSION REL(12), XX(6), KK(14)
      C   DIMENSION THIN(3), BUFF(60)
      C
      C   COMMON A(600)
      C   COMMON /FLIT/, KFFLT, SIZE, IH(3), IPOPT, KCPLT
      C
      C   DATA IBIN/3,4,8/
      C   I6=60
      C   IF=61
      C
      C   *** FTBIN (I,3,IBIN) ****
      C   *** CALL FTBIN (I,3,IBIN) ****
      C   *** ****C
      C
      C   CALL SYSTEM BLOCKING ROUTINES FOR TAPES 3 AND 4 *ONLY*
      C
      C   READ THE LINE FORTHOLE TAPE AND SET UP FILES FOR
      C   TAPE 3 - NODE COORDINATES
      C   TAPE 4 - ELEMENT CONNECTIVITIES
      C
      C   CALL PORT (NMM, NELTP, N1, N2, N3, N33, KTL)
      C
      C   READ MASTER CONTROL CARD
      C
      C   NVFW=1
      C   SAVSIZE
      C   IF (SIZE.LT.1.0) SIZE=10.0
      C   IF (SIZE.GT.1.3L0) SIZE=30.0
      C
      C   PERFORM PLOT INITIALIZATION
      C
      C   SET PLOT SIZE TO 30 INCHES (WITH 10 PERCENT REDUCTION)
      C
      C   SIZE=SIZE/1.1
      C   CALL FACTCH (SIZE)
      C
      C   SET PLOT LOWER PUNCTURATION LINE
      C
      C   CALL PLOT (200,0,0,-3)
      C   CALL PLOT (0,0,0,250,-3)
      C
      C   COUNT I=6
      C
      C   COUNT ON LOCAL NUMBER OF VIEWS
      C
      C   IF (COUNT.LT.1) STOP 20
      C   IF (COUNT.GT.NV=1) VIEWS
      C   COUNT J
      C
```

SUBROUTINE SSP 74/74 OPT=1

FTN 4.0.6+43DE 03/07/80 11.41.06 PAGE 2

C RESTORE GLOBAL COORDINATES

C CALL READS (3,A(N)),N33)

C HEAD VIEW CONTROL CARD

C NFR=1

XX(1)=0.

XX(2)=0.

XX(3)=0.

XX(4)=0.

XX(5)=0.

XX(6)=0.

C TEST ANGLES FOR ADMISSIBILITY

C L=0

DO 5 K=L,3

IF (ABS(IH(K)).LT.360.1) GO TO 5

L=L+1

S CONTINUE

IF (L(LI,2).GT.10)

WRITE (IP,160)

STOP 21

14 CONTINUE

C DEFINE PLG1 COORDINATES FOR THIS VIEW

C CALL PI (A(N1),A(N2),A(N3),NUMNP,TH,XX)

C PLG1 NFR NAMES IN THIS VIEW

C DO 90 N=1,11

REWIND 4

C READ FRAME DATA

C KTYPE=1

C HY-PASS HOUNDARY ELEMENT PLOTTING

C IF (KTYPE.EQ.7) GO TO 90

C TEST FOR ADMISSIBLE ELEMENT TYPE

C IF (KTYPE.GT.0.AND.KTYPE.LE.8) GO TO 15

C IF (KTYPE.EQ.12) GO TO 15

STOP 22

15 CONTINUE

C ADVANCE ELEMENTS TAP4 TO THIS ELEMENT TYPE

C DO 20 L=1,NELTP

C IF (KTYPE.LT.0.KTYPE) GO TO 25

21 CONTINUE

C N=N-1

C IF (N.EQ.1) GO TO 40

```

115      DC 35 J=1,M
          READ (4) LT1,TYP,NUMEL,LH2
          IF (LH2.EQ.0) GO TO 35
          DC 30 I1=1,NUMEL
          CALL REAUS (4,NP,LH2)
          30 CONTINUE
          35 CONTINUE
          *F REAU (*I,I1,TYP,NUMEL,LH2
          IF (TYP.NE.KTYPE) STOP 24
          C SHIFT PEN TO NEW ORIGIN
          C CALL PLOT (3.0,0,0,0,-3)
          NCOUNT=COUNT+1
          IF (NCOUNT.EQ.1) CALL PLOT (1.0,0,0,7,-3)
          130      C READ AN ELEMENT PLOT SEQUENCE CARD
          C
          NE=0
          KK(1)=1
          KK(2)=NUMEL
          DO 45 IJK=3,14
          45 K(IJK)=0
          IF (KK(1).LT.1) GO TO 65
          DC 50 L=1,7
          IF (KK(2*L).LT.1) KK(2*L)=KK(2*L-1)
          IF (KK(2*L).LT.KK(2*L-1)) GO TO 55
          50 CONTINUE
          GO TO 65
          C ELEMENT SEQUENCE NOT IN ORDER
          55 WRITE (15,1CS) L
          60 CONTINUE
          IF (KK(1).GT.NE) GO TO 60
          GO TO 85
          C CHECK FOR INCREASING SEQUENCE ELEMENT NUMBERS
          140      65 L=1
          IF (KK(1).LT.NE) GO TO 55
          DC 70 L=2,7
          IF (KK(2*L-1).LT.1) GO TO 70
          IF (KK(2*L-1).LT.1) GO TO 70
          IF (KK(2*L-1).LT.1) GO TO 70
          70 CONTINUE
          C PLOT THE RANGE OF ELEMENTS IN SEQUENCE L
          C
          UC 80 L=1,i
          L=KK(2*L-1)
          IF (L.LT.1) GO TO 85
          12=KK(2*L)
          IF (12.GT.NE) STOP 25
          DC 80 M=1,i
          165      C READ THE RANGE OF ELEMENTS FROM TAPE
          C 75 CALL REAUS (4,NP,LH2)
          NE=NE+1
          IF (M.GT.NE) GO TO 75
          170      C

```

SUBROUTINE SSP      7474      OPT=1      F7N 4.6•433E      03/07/80      11.41.06      PAGE 4  
 C PLOT THIS ELEMENT  
 C ILINE=0 • SOLID LINE • UNFORMED  
 C ILINE=5 • DASHED LINE • NO CURRENT  
 175    C ILINE=0  
 C IF (IPOP1.EQ.0) ILINE=5  
 C IF (IPOP1.EQ.2.AND.NE.GT.NUMEL/2).ILINE=5  
 C IF (IPOP1.EQ.2.AND.NE.GT.NUMEL/2).ILINE=5  
 C CALL P2 (A(1),A(2),NP(4),NP(5),NP(6),NP(9),NP(10),NP(11),LH2,ILINE)  
 C CONTINUE  
 C PLOT FRAME LABELS AND TITLE CARDS  
 C BS CALL P3 (MLL,1H)  
 185    C 9C CCJNTUE  
 C 95 CCJNTUE  
 C CLOSE THE PLUT FILE  
 190    C  
 C I1=11+10\*  
 C I2=12+10\*  
 C I3=13+10\*  
 C SIZE=SAYSIZ  
 C CALL PLUT (0.0,-0.95,-3)  
 C RETURN  
 C 10C 10CPLT (//23H SOLUTION TERMINATED\*\*\*,//20H TWO ANGLES .GT. 360)  
 C 10C 10CFORMAT (8X,10SEQUENCE =,12,26H ON CARD ABOVE IS IN ERROR.)  
 195    END  
 200    END

```

1      SUBROUTINE POINTS (NUMNP,NELTYP,N1,N2,N3,N33,KEL)
C
C      DIMENSION HEDT(12), L1(19), NP(18), LOUT(12), MPAR(14), KPAR(14)
C      NELTYP(12), AP(14),
C      COMMON A(6600)
C      EQUIVALENCE (L1(12),NP(11),AP(11))
C      DATA LIN/3,3,5,5,9,5,6,17,0,0,0,4/,LOUT/2,2,4,4,8,4,0,10,0,0,0,18/
C      IP=60
C      IP=61
C      NTA=10
C
C      READ AND RE-FORMAT THE PUNCHLINE TAPE - NTB
20     REWIND NTB
C
C      1 HEADING AND CONTROL INFORMATION
25     READ (NTB) (HEDT(K),K=1,12),NUMNP,NELTYP
C      2 EQUATION NUMBERS FOR RETAINED DEGREES OF FREEDOM
30     READ (NTB)
2      C      SET UP ARRAY SIZE FOR COORDINATES
30     C
35     N1=1
C      N1=NUMNP
C      N2=N1+NUMNP
C      N22=2*NUMNP
C      N3=N2+NUMNP
C      N33=3*NUMNP
C      N4=N3+NUMNP
C      N5=N4+NUMNP
C      I=LUCF (A(1,N4))
C
3      READ NODE COORDINATES
4      HEAD (N18) (A(IK)),K=1,N11
C      HEAD (NTB) (A(IK)),K=2,N22
C      HEAD (N18) (A(IK)),K=3,N33
3      C
4      C      PRINT FIRST AND LAST NODE COORDINATES
5      C
50     C
55     C      SAVE NODE COORDINATES ON TAPPF 3
56     C
57     C      REWIND 3
58     C      CALL WRITES (3,A(11),N33)
59     C      4      NODE TEMPERATURES

```

SUBROUTINE POINTS 74/74 OPT=1

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```
4 READ (NTB)          PUR 58
C   4 PUR 59
C   5 ENCLFILE MARK PUR 60
C   READ (NTB) NULM PUR 61
C   5 PUR 62
C   USE PREVIOUS CARD FOR RUN COMPILER PUR 63
C   IF (EOF(NTB)) 10,5 PUR 64
C   WRITE (IP,135) PUR 65
C   CALL EXIT PUR 66
C   10 CONTINUE PUR 67
C
C   PROCESS ELEMENT DATA AND SAVE CONNECTIVITIES ON TAPE 4 PUR 68
C
C   REWIND 4 PUR 69
C
C   75 C PUR 70
C   DO 130 M=1,NELTYP PUR 71
C
C   130 C PUR 72
C   ELEMENT CONTROL PARAMETERS PUR 73
C   READ (NTB) (NPAR(K),K=1,14) PUR 74
C   6 ELEMENT CONTROL PARAMETERS PUR 75
C   6 READ (NTB) (NPAR(K),K=1,14) PUR 76
C
C   IELTYP=NPAR(1) PUR 77
C   KEL(M)=IELTYP PUR 78
C   NCMEL=NPAR(2) PUR 79
C
C   LR=LIN(IELTYP) PUR 80
C   LQ2=LOU(IELTYP) PUR 81
C
C   WRITE (4) IELTYP,NCMEL,LH2 PUR 82
C
C   GC TO 15,25,35,40,50,55,65,70,75,85,90,95, IELTYP PUR 83
C
C   90 C PUR 84
C   PUR 85
C   PUR 86
C   PUR 87
C   PUR 88
C   PUR 89
C   PUR 90
C   PUR 91
C   PUR 92
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C   PUR 106
C   PUR 107
C   PUR 108
C   PUR 109
C   PUR 110
C   PUR 111
C   PUR 112
C   PUR 113
C   PUR 114
C
C   105 C
C   HEAD (NTB)
C   A LOAD MULTIPLIERS
C   PFILE (NTB)
C   GOTO 106
```

```

115      25 CONTINUE
          NLUMATERIAL(4)
          MATERIAL PROPERTIES
          C
          9 UC 30 ISKIP=1,NUMMAT
          READ (N18)
          9
          C LU
          READ (N18)
          30 CONTINUE
          10
          C LU
          READ (N18)
          11
          C LU
          READ (N18)
          12
          C LU
          IF (NLUMATERIAL.GT.0) READ (N18)
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```

SUBROUTINE PUNKT 74/74 OPT=1

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PAGE 4

IF(MMA1=NPAR(3))  
DC 6C ISKIP=1,NUMMAT

READ (NIB)

19

C 20

READ (NIB)

6C CONTINUE

20

LUAU MULTIPLIERS

CG TO 100

C 65 CONTINUE

21

READ (NIB)

21

C 6C TO 100

C 7L CONTINUE

NLD=NPAR(4)

C 22

HEAD (NIB)

195

C 22

HEAD (NIB)

23

IF (NLD.GT.0) READ (NIB)

C 23

HEAD (NIB)

24

READ (NIB)

C 24

CG TO 100

C 75 CONTINUE

C 6C WRITE (1P,140) IELTYP

205

C STOP

210

C 65 GO TO 80

C 90 CG TO 80

C 215

C SKIP PLOT PROPERTIES, SECTION, BRANCH PT NODES, MULTIPLIERS

95 IF(PRN=NPAR(6))

HEAD (NIB)

HEAD (NIB)

IF (NPRH.GT.0) HEAD (NIB)

HEAD (NIB)

C \* \* \* \* \*

C 1,\* CONTINUE

225

C PFAU ALL ELEMENTS OF TENS, TRUE

C

```

230      LHR2=LHR2
          IF (LIEL1F.EQ.12) LHR2=3
          UC 125 K=1,KUREL
          C CALL READS (N18,IX,LR)
          C
          C BY-PASS THE BOUNDARY ELEMENTS
          C IF (LIEL1F.EQ.7) GO TO 120
          C
          C CHECK FOR SEQUENTIAL INPUT ORDER
          C IF (IX(1).EQ.N) GC TO 105
          WRITE (IP,145) IX(1),K,1
          CALL EXIT
          C 105 CONTINUE
          C
          C TEST FOR FOURTH NODE ZERO
          C IF (LR2.NE.4) GO TO 110
          C IF (INP(4).LT.1) INP(4)=NP(3)
          C
          C 110 IF (IELYP.NE.12) GO TO 115
          C
          C READ RADIUS,KODE,X3P (BLND). OR JUNK (TANGENT)
          C
          C READ (INP(8)) AP(4)*NP(5),AP(6),AP(7)*AP(8)
          C IF (INP(1).EQ.1) GO TO 115
          C
          C HEND. READ THETA AND DC ARRAY
          C
          C HEAD (INP(1)) AP((JL)+JL+9,18)
          C
          C PIPE TAPE SAVE FORMATS (TAPE4)
          C TANGENT - 1*N1*N2*XLN*JUNK(5)-JUNK(14)
          C HEND - 2*N1*N2*RADIUS*KODE,X3P,SMETA,DC(1,1)-DC(3,3)
          C
          C 115 CALL WRITES (4*NP,LR2)
          C
          C PRINT FIRST AND LAST ELEMENT CONNECTIONS
          C
          C 120 CONTINUE
          C 125 CONTINUE
          C 130 CONTINUE
          C
          C RETURN
          C
          C 135 FORMAT (//,13H SOLUTION TERMINATED**,/39H NO END-OF-FILE ENCONTRD)
          C 140 IFRED ON TAPE RTB*)
          C 141 FORMAT (1/26H *ELEMENT TYPE (112-23H) ENCOUNTERED ON TAPE)
          C 142 */*X)
          C 143 *CHMAT (1/13H *CHMUR** ELEMENTS ON TAPE ARE NOT SEQUENTIAL,5X,3P)
          C 144 */*)
          C
          C 270
          C 275
          C
          C 280
          C
          C 285
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          C 5075
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          C 5080
          C
          C 
```

ROUTINE WRITES 74/7, OPT=1 FIN 4.6+33E 03/07/80 11.41.06 PAGE 1

1 \*UECK WRITES  
SUBROUTINE WRITES (ITAPE,A,LREC)  
DIMENSION A(LREC)  
WRITE (ITAPE) A  
RETURN  
END

5

SUBROUTINE HEADS 74/74 (P#1)

1 \*DECN HEADS  
SUBROUTINE HEADS (ITAPE, A, LREC)  
DIMENSION A(LREC),  
READ (ITAPE) A  
RETURN  
END

5

FIN 4.6\*433F

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PAGE 1

HEAD 1  
HEAD 2  
HEAD 3  
HEAD 4  
HEAD 5  
HEAD 6-

SUBROUTINE P1 74/74 OPT=1

FIN 4.6+433E.

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```
1      *SUBROUTINE P1 74/74  OPT=1
2
3      C
4      C PLOT VITW INITIALIZATION PROGRAM
5      C
6      DIMENSION U(1), V(1), W(1), TH(1), XM(1)
7      C
8      COMMON /MESH/ XX(12), YY(12), XLEN, YLEN, ALLEN, EX(3), EY(3), XMIN, YMIN
9      C
10     DATA RAD/0.01745329254/
11
12     C CONVERT COORDINATES TO A TWO-DIMENSIONAL PROJECTION
13
14     DC 5 I=1,3
15     EX(I)=SIN(TH(I)*RAD)
16     EX(I)=CCS(TH(I)*RAD)
17     IF (TH(I).LT.360.) GO TO 5
18     EX(I)=9.
19     EY(I)=0.
20
21     C DC 16 I=1,4,1,N
22     TEMP=U(I)*EX(I)+V(I)*EY(I)+W(I)*EY(I)
23     U(I)=U(I)*EX(I)+V(I)*EX(I)+W(I)*EX(I)
24     V(I)=TEMP
25
26     C CONTINUE
27
28     C CONVERT MAX/MIN CONTROL DIMENSIONS TO THE PLOT SYSTEM (U,V)
29
30     DC 15 K=1,6
31     DC 15 DUM=AHS(XM(K))
32     IS 15 JF (DUM.LT.-.0001) GO TO 25
33
34     C
35     U1=XM(1)*FX(1)
36     U2=XM(2)*FX(1)
37     U3=XM(1)*EY(1)
38     U4=XM(2)*EY(1)
39     U5=XM(3)*EX(1)
40     U6=XM(4)*EX(2)
41     U7=XM(3)*EY(2)
42     U8=XM(4)*EY(2)
43     U9=XM(5)*EX(3)
44     U10=XM(6)*EX(3)
45     U11=XM(5)*EY(3)
46     U12=XM(6)*EY(3)
47
48     C U = VALUES FROM MAX/MIN CONTROL POINTS
49
50     C
51     U(1)=U1+0.05*UX
52     U(2)=U1+0.06*UX
53     U(3)=U1+0.05*UY
54     U(4)=U1+0.06*UY
55     U(5)=U2+0.05*UX
56     U(6)=U2+0.06*UX
57     U(7)=U2+0.05*UY
58     U(8)=U2+0.06*UY
59
```

```

60      C   W(9)=0.3*U7*D11
       C   W(10)=0.3*U7*D11
       C   W(11)=0.3*U7*D12
       C   W(12)=0.3*U8*D12
       C   W(13)=0.4*U7*D11
       C   W(14)=0.4*U8*D11
       C   W(15)=0.4*U7*D12
       C   W(16)=0.4*U8*D12
70      C   FIND MAX-MIN DIMENSIONS IN THE CONTROLLED SCALE DIMENSIONS
       C
       C   X& Y(N=1) = 0.0
       C   XMAX=W(9)
       C   YMAX=W(9)
       C
       C   UC 20 1=2,8
       C   IF (XMIN>GT.W(1)) XMIN=W(1)
       C   IF ((W(1)+GI.XMAX) XMAX=W(1)
       C   IF (YMIN>GT.W(1+8)) YMIN=W(1+8)
       C   IF ((W(1+8)+GI.YMAX) YMAX=W(1+8)
       C
       C   2D CONTINUE
       C
       C   FIND MAX-MIN DIMENSIONS FROM NODAL POINT ARRAY (NO USER CONTROL)
       C
       C   25 XMIN=W(1)
       C   YMIN=W(1)
       C   XMAX=W(1)
       C   YMAX=W(1)
       C
       C   UC 30 1=2,NUMNP
       C   IF (XMIN>U(1)) XMIN=W(1)
       C   IF (U(1)>XMAX) XMAX=W(1)
       C   IF (YMIN>V(1)) YMIN=W(1)
       C   IF (V(1)>YMAX) YMAX=W(1)
       C
       C   30 CONTINUE
       C
       C   SHIFT PLOT NODLES FOR SYMBOL PLOT OF GLOBAL AXES
       C
       C   35 UC 4,0 T=1,3
       C   T-(1)=T-(1)-30.0
       C   4C 3C CONTINUE
       C
       C   FIND PROBLEM HORIZONTAL SCALE
       C
       C   YLEN=(YMAX-YMIN)/10.0
       C   IF (YLEN>0.0) GO TO 45
       C   ALEN=(XMAX-XMIN)/10.0
       C   ALEN=10.0
       C   GO TO 50
       C   ALEN=(XMAX-XMIN)/YLEN
       C   ALEN=1E-4
       C   IF (ALEN<1.3E-4) GO TO 50
       C   FLEN=(XMAX-XMIN)/30.0
       C   FLEN=1E-4

```

FUM 5/

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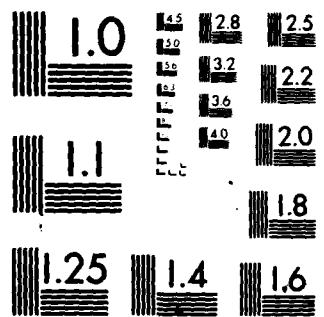
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MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

```

115      C      ALLEN=30.0          P1  115
C      C      SET SCALE PARAMETERS   P1  116
C      C      CCONTINUE             P1  117
120      C      AX(11)=0.0          P1  118
      AX(12)=XLEN                P1  119
      YV(11)=0.0                  P1  120
      YV(12)=YLEN                P1  121
      C      C      CONVERT PLOT ORDINATES TO RELATIVE VALUES   P1  122
C      C      DO 55 I=1,NUMP          P1  123
      U(I)=U(I)-APIN            P1  124
      V(I)=V(I)-YIPN            P1  125
      C      C      55 CONTINUE           P1  126
      C      C      RETURN             P1  127
      END                         P1  128
130      C      CCONTINUE             P1  129
      C      C      130 CONTINUE           P1  130
      C      C      RETURN             P1  131
      END                         P1  132
135      C      C      135 CONTINUE           P1  133
      END

```

## CARD #. SEVERITY DETAILED DIAGNOSIS OF PROBLEM

187

36	I	XH	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
38	I	XH	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
39	I	XH	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
40	I	XH	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
41	I	XH	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
42	I	XH	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
43	I	XH	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
44	I	XH	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
45	I	XH	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
46	I	XH	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
51	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
52	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
53	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
54	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
55	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
56	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
57	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
61	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
62	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
63	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
64	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
65	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
66	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
67	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
68	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
73	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
75	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.



```

CALL LINE (XX,YY+5,1,0,0)          P2 58
RETURN                                P2 59
C   EIGHT NODE ELEMENT (BRICK OR WEDGE)    P2 60
C   25 CONTINUE                            P2 62
DO 30 M=1,4                           P2 63
JNP(M)                                P2 64
  AX(M)S(M)U(M)                      P2 65
  30  YY(M)=M(M)                      P2 66
                                         P2 67
C   DC 35 N=5,0                         P2 68
                                         P2 69
  70  JNP(3,M)                        P2 70
    AX(M)S(M)U(M)                      P2 71
    35  YY(M)=M(M)                      P2 72
                                         P2 73
  75  AX(9)S(9)U(9)                    P2 74
    XX(9)S(9)U(9)                      P2 75
    XX(10)S(10)U(10)                   P2 76
    XX(11)S(11)U(11)                   P2 77
    XX(12)S(12)U(12)                   P2 78
    XX(13)S(13)U(13)                   P2 79
    XX(14)S(14)U(14)                   P2 80
    XX(15)S(15)U(15)                   P2 81
    XX(16)S(16)U(16)                   P2 82
    XX(17)S(17)U(17)                   P2 83
    XX(18)S(18)U(18)                   P2 84
    CALL LINE (XX(9),YY(9),2,1,0,0)      P2 85
    XX(19)S(19)U(19)                   P2 86
    YY(9)=YY(6)                        P2 87
    XX(10)=XX(13)                      P2 88
    YY(10)=YY(3)                        P2 89
    CALL LINE (XX(9),YY(9),2,1,0,0)      P2 90
    XX(9)=XX(12)                        P2 91
    YY(9)=YY(2)                         P2 92
    XX(10)=XX(7)                        P2 93
    YY(10)=YY(7)                        P2 94
    CALL LINE (XX(9),YY(9),2,1,0,0)      P2 95
                                         P2 96
C   RETURN                                P2 97
                                         P2 98
C   SIXTEEN NODE ELEMENT (THICK SHELL)    P2 99
C   *0 CONTINUE                            P2 100
                                         P2 101
C   TOP AND BOTTOM USING SYMBOL FOR MID-NODE(S)
INC=9                                P2 102
DO 50 I=1,2                          P2 103
  IF I=.50+.2) INC=4
  DC 45 M=1,9
  J=I(M)+INC
  JNP(J,U)
  XX(M)=U(J)
50  U(M)=U(J)
  CALL LINE (XX(2),YY(2),9,1,2,0,1)    P2 111
                                         P2 112
                                         P2 113
C   LUGES                                P2 114

```

```

115      C      DO 55 I=1,4          P2    115
      J=NPI(1)           P2    116
      K=NPI(1+4)         P2    117
      X=(9/I)*U(1)       P2    118
      Y(9)=V(1)          P2    119
      X(10)=U(10)        P2    120
      Y(10)=V(10)         P2    121
      55 CALL LINE(X(9),Y(9),X(10),Y(10))   P2    122
      C      MEJURA          P2    123
      C      HEND (PIPE ELEMENT)    P2    124
      C      IF (NSEG>1)TA/RAD2    P2    125
      C      60 NSEG=L1,I1 NSEG=1    P2    126
      J=NPI(12)           P2    127
      X(12)=U(12)         P2    128
      Y(12)=V(12)         P2    129
      130
      IF (NSEG>1)TA/RAD2    P2    130
      J=NPI(12)           P2    131
      X(12)=U(12)         P2    132
      Y(12)=V(12)         P2    133
      132
      X(3)=X(11)          P2    134
      X(4)=X(12)          P2    135
      Y(3)=Y(11)          P2    136
      Y(4)=Y(12)          P2    137
      136
      TA=0                P2    138
      EDC1=EX(1)+DC(1,1)*EX(2)+DC(2,1)*EX(3)+DC(3,1)  P2    139
      EDC12=EX(1)+DC(1,2)*EX(2)+DC(2,2)*EX(3)+DC(3,2)  P2    140
      EDC2=EV(1)+DC(1,1)*EV(2)+DC(2,1)*EV(3)+DC(3,1)  P2    141
      EDC22=EV(1)+DC(1,2)*EV(2)+DC(2,2)*EV(3)+DC(3,2)  P2    142
      CALL LINE(X(2),Y(2),X(1),Y(1))  P2    143
      RTERM=RADIUS          P2    144
      144
      IE(KODE;EV(1),RTERM=RADIUS,TAN(0.5*(ME(1)-  P2    145
      UCDE)*TERM)+(X3P(1)*DC(1,KODE)*TERM)+(X(2)-  P2    146
      IMP)*EX(1)+(X3P(1)-DC(3,KODE)*TERM))-YMIN)  P2    147
      VCOR=(EV(1)*(X3P(1)-DC(1,KODE)*TERM)+EV(2)*(X3P(2)-DC(2,KODE)*TERM))-YMIN  P2    148
      IMP)*EV(3)*(X3P(3)-DC(3,KODE)*TERM))-YMIN  P2    149
      U0=76 I=1,NSEG          P2    150
      X(I)=X(1)           P2    151
      Y(I)=Y(1)           P2    152
      149
      I=1A=1TA*RAU2          P2    153
      X=RADIUS*SIN(1ITA)          P2    154
      X(2)=CUCU1*X*EDC12*UCUR          P2    155
      Y(2)=ECU2*X*EDC12*UCUR          P2    156
      IF (I,L1NSEG) GO TO 65          P2    157
      J=NPI(13)           P2    158
      X(12)=U(12)           P2    159
      Y(12)=V(12)           P2    160
      160
      65 CALL LINE (XX,YY,2,1000)    P2    161
      /* CONTINUE          P2    162
      /* CAJBIAE ((X(2),Y(2),1,1,-1,1))  P2    163
      /* JBPW          P2    164
      165
      C      END          P2    165
      C      P2    166
      C      P2    167
  
```

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138 1 NO. 52ND ST. PROBLEMS - SEVERITY DETAILS - 01-1

139 1 NO. 52ND ST. PROBLEMS - SEVERITY DETAILS - 01-1

SUBROUTINE P3      7474    OPT=1

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```
1      *DECK 'P3'
2      SUBROUTINE P3 (IMED,TH)
3
4      C THIS ROUTINE COMPLETES THE PLOT FRAME
5      C DIMENSION MED(1), TH(1), M(13)
6
7      C COMMON /MESH/ X(12),Y(12),ALEN,YLEN,ALEN,EX(3),EY(3)
8      P3   1
9      P3   2
10     DATA M/1HZ,1HZ,1HZ/
11     IMA69
12     IPOL
13     P3   3
14     C PLOT TITLE AND AXES
15     C CALL SYMBOL (0,0,-3,0,14,ME(1),0,0,0,0)
16     P3   4
17     CALL PLOT (-1.5,1.5,-3)
18     DC S 1#1;3
19     IF (M(1)) .GT. 270 .OR. GO TO 10
20     CALL SYMBOL (.5*EX(1),.5*EY(1),1.0,13,TH(1),0,-1)
21     CALL SYMBOL (EX(1),EY(1),0,1,6,14,11,-1)
22     CALL SYMBOL (1.2*EX(1),-0.75,1.2*EY(1),-0.75,15,TH(1),0,0,1)
23     S_CONTINUE
24     C ADVANCE PAPER TO NEXT FRAME
25     C CALL PLOT (1.5,-1.5,-3)
26     CALL PLOT (ALEN+7.0,0,0,-3)
27     C RETURN
28     P3   5
29     P3   6
30     P3   7
31     END
```

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